

-0007 ± 4.7
0000

-011 ± 3.9
-010

6028 0 59.4 +50 46 6.6 A2m +6.46

584

GL1241 59 23.134 1798.0 +50 45 59.41 1896.5

30
170

59
45 00.00

57 55.99
1 27.002

59 22.992
154

23.746
- 9

137

23.190
- 14
176

23.197
- 2
195

208
169
600

(410.7)

37 55.0
8 5.20

45 00.20
- 42

44 59.78
+ 28

45 00.06
44 59.87

- 28
59.59

59.63
- .37

59.45
- 22
59.23

1925.4

112621 8
15888
5903

1944.82

1946.96

38.7 (42.2)

R.A. : 1.000
DEC. : -31.900
R.A. : 82.000
DEC. : -29.000
DISTANCE : 5.800
MODULUS : 145
VEL. : 25.100

q1 (U) : 0.826
q2 (U) : 0.564
q3 (U) : -0.009
dU : 194.920
U : 27.953

q1 (V) : -0.563
q2 (V) : 0.822
q3 (V) : -0.088
dV : -298.619
V : -45.382

q1 (W) : 0.043
q2 (W) : -0.078
q3 (W) : -0.996
dW : 24.765
W : -21.421

6290 4/2/60

010
70.9

-41 17

13 7

② 14

0.214 1.3 + 10224 ± 113

2152 - 984

$\frac{117}{0.338}$

$\frac{117}{2152}$

70.21

2165

$\frac{117}{307}$

$\frac{117}{2179}$

7036 000

$\frac{117}{-5}$

70306 - 0009 + 404

7034 - 0005

$\frac{117}{8.5}$

14.1

7036 - 0005



3

RAD. VEL. : 4.188
 MODULUS : 201
 DISTANCE : 8.888
 FM. DEC. : -2.888
 FM. R.A. : 28.888
 DEC. : -41.888
 R.A. : 1.888

p1 (U) : 0.828
 p2 (U) : 0.252
 p3 (U) : -0.181
 u : 127.977
 v : 29.727

p1 (V) : -0.288
 p2 (V) : 0.787
 p3 (V) : -0.231
 w : -112.888
 x : -28.888

2

p1 (W) : 0.048
 p2 (W) : -0.248
 p3 (W) : -0.828
 y : 12.827
 z : 2.827

R.A. : 1.000
DEC. : -41.300
PM. R.A. : 48.000
PM. DEC. : -5.000
DISTANCE : 8.500
MODULUS : 501
RAD. VEL. : 4.100

q1 (U) : 0.826
q2 (U) : 0.555
q3 (U) : -0.101
dU : 127.977
U : 63.727

q1 (V) : -0.563
q2 (V) : 0.797
q3 (V) : -0.221
dV : -115.030
V : -58.559

q1 (W) : 0.043
q2 (W) : -0.240
q3 (W) : -0.970
dW : 12.957
W : 2.517

+0010 = 4.6
-056 = 4.4
-066

6211 | 01.1 +52 14 6.3 142 -7.0 1

603

1275 | 5.289 1910.7 +52 14 6.00 1411.3
-039
250

59 39.26
1 27.860
05.120
1 05.164
1289
-275
275

29.4

6 3.3 1427.6
8 4.25
14 7.55
7.44
7.11 1883 12.02
7.28
7.39

28.8

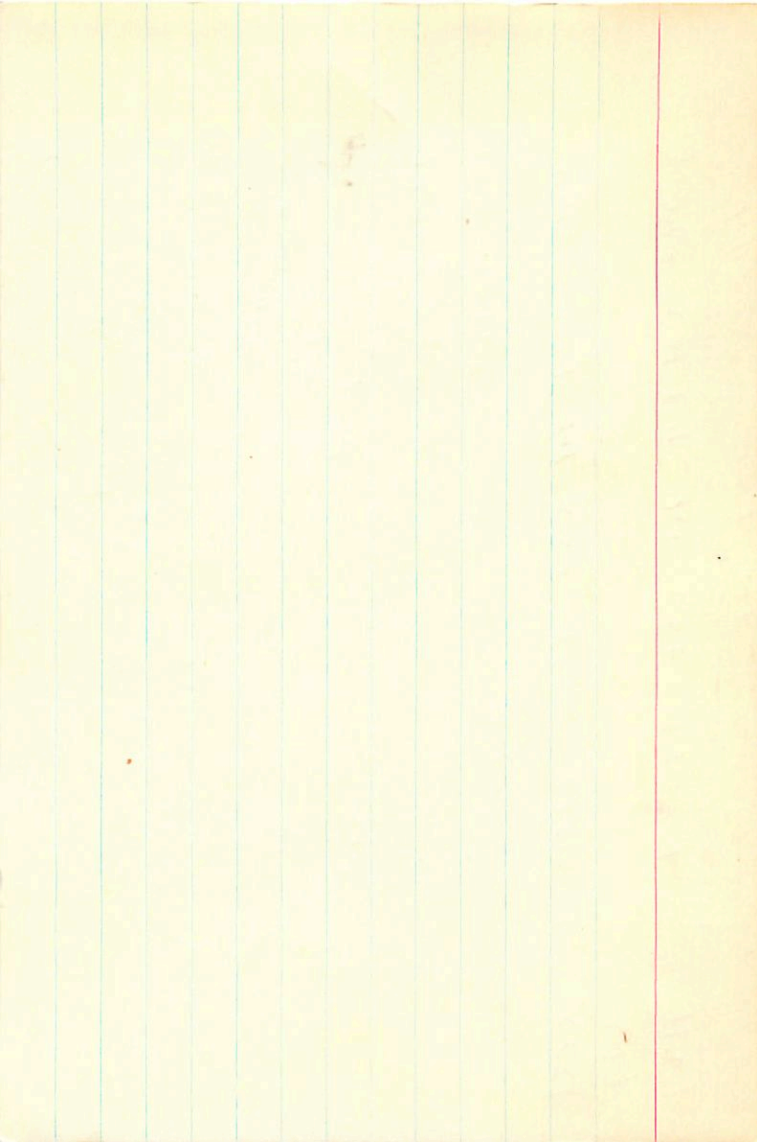
1945.71

5.82
6.28
-24
5.58
6.10
24
5.86

1944.96
1940.1

5.282
274
+031
281

5.283
241



-015956.4 -101448 511 52m=0
-0130 -091

6334 01 01.3

F52 712.0 ± 1.09, 1.5
F52 +130 ± 1.0, 1.5
+12.5 a

12824 11m 100''

1282 16.240 1501.7 -60 21 52.62 1856.6

768
17,008
5.39
47.23

1272

-0145 -096

34

145
72
34
10

16.47 1946.9

-108
+10

51.2

-098 +10

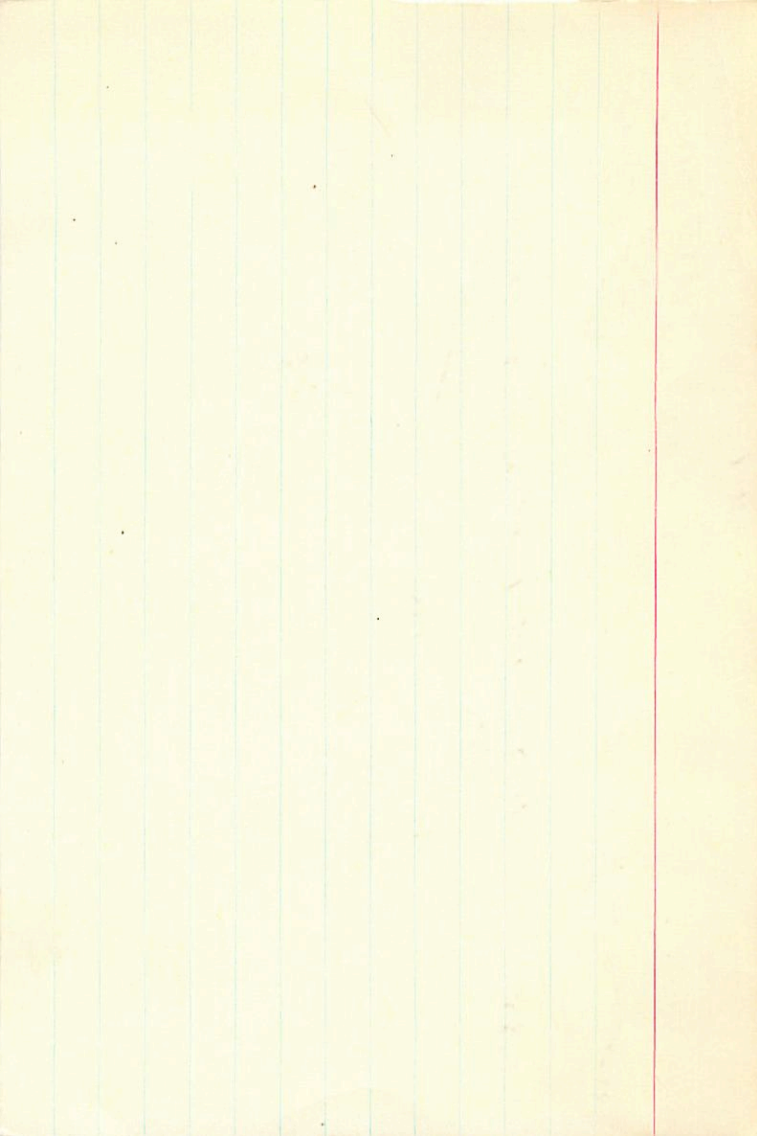
50.3

8
51.7

986
-586

4
54

4
9



301

1 21-2 +1 07

+8.

6288 607 059 1184 -986

6-11 +27

PNS

[+1218 -0418]

13.2 204
1315

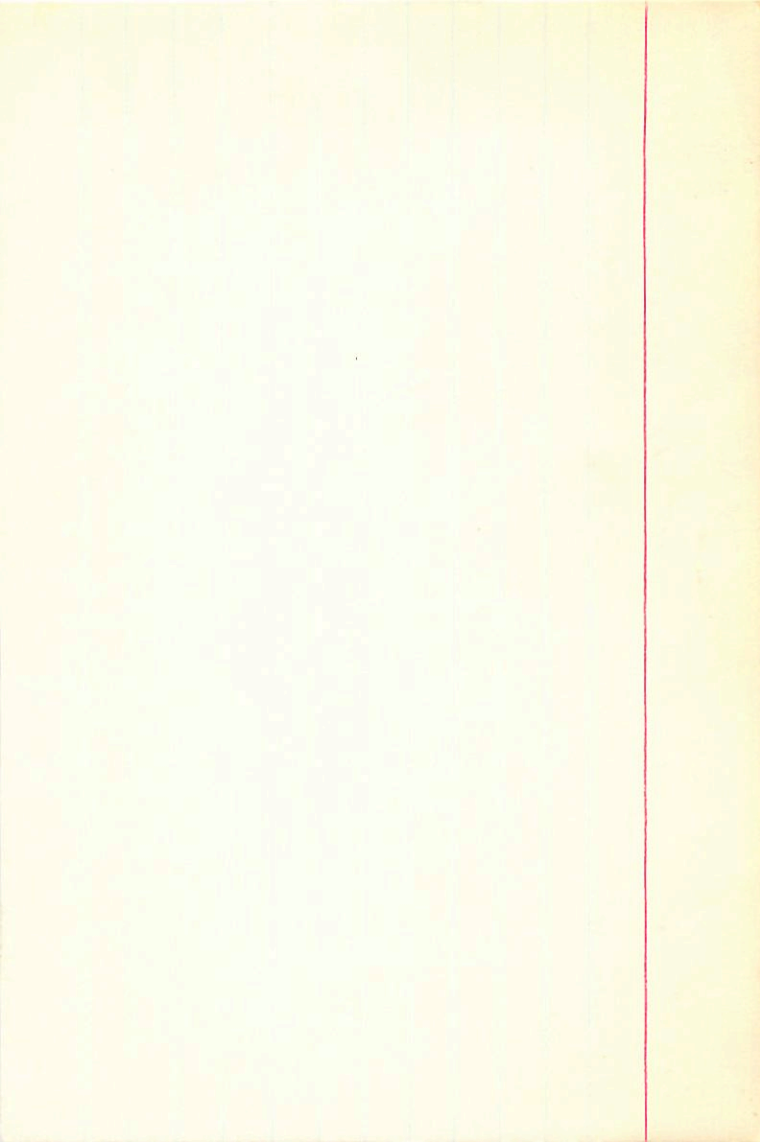
+85

9562 9724

2927 -2312

1282
2.5

607-12
3.37



6340

1 01.6

-34 5-7

8.54 A1E

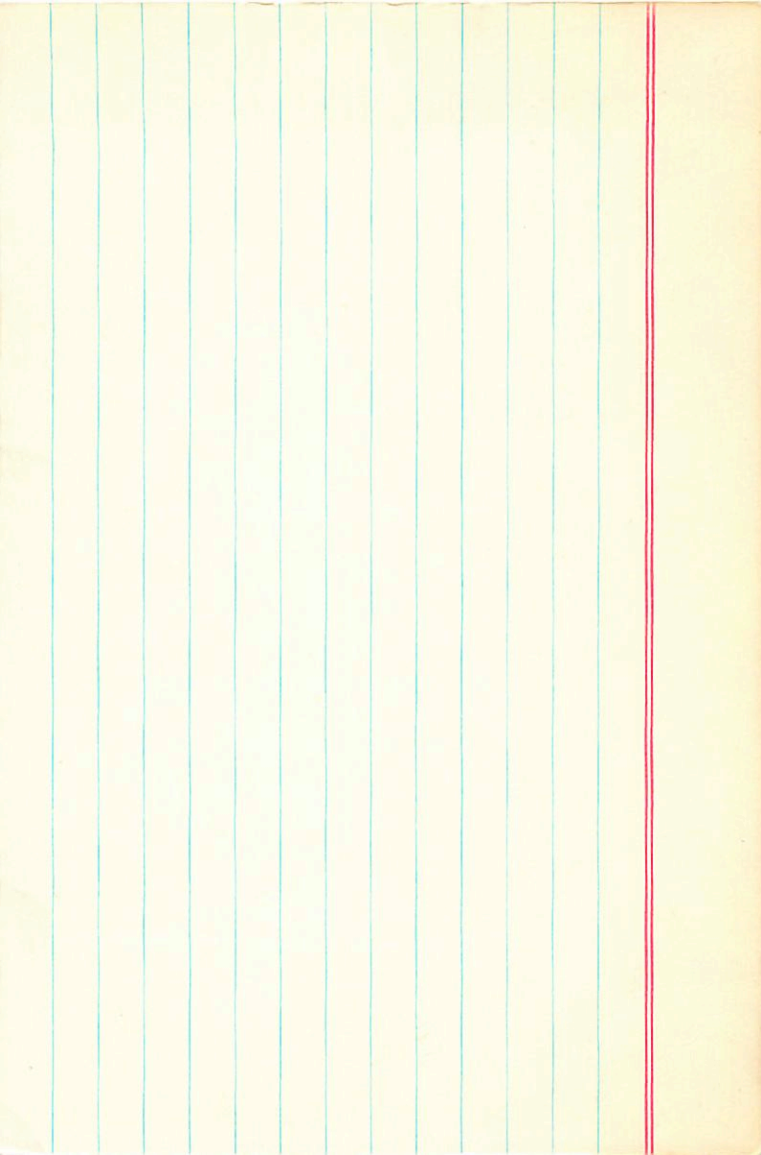
FV816

40.11

(1.56)

A25 -132
A54 -124
A1E -1.8

-40



-30,146 6348 , 01.9 -2 38 G5 -20.3 (4)
-17.1 50.5 1 Surage

G 70-35

9.18 +0.795 +0.36

-129 (3) Var
20.2 (4)
2 Surage

S = 06

2.95 = 38.910.

| | | |
|-------|-------|-----|
| -185 | -117 | 4 |
| -8 | +3 | |
| <hr/> | <hr/> | |
| -193 | -114 | |
| +2 | | |
| <hr/> | <hr/> | |
| -191 | -116 | N30 |

| | | | | | | | | |
|------|------|------|-------|-------|---------|-------|-------|-------|
| +826 | +498 | +265 | -7478 | -2738 | -1.0216 | -39.7 | -4.5 | -44.2 |
| -562 | +762 | +320 | +5088 | -4189 | +0.899 | +3.5 | -5.5 | -2.0 |
| +043 | +413 | -910 | -0389 | -2271 | -2.660 | -10.3 | -15.6 | -25.9 |

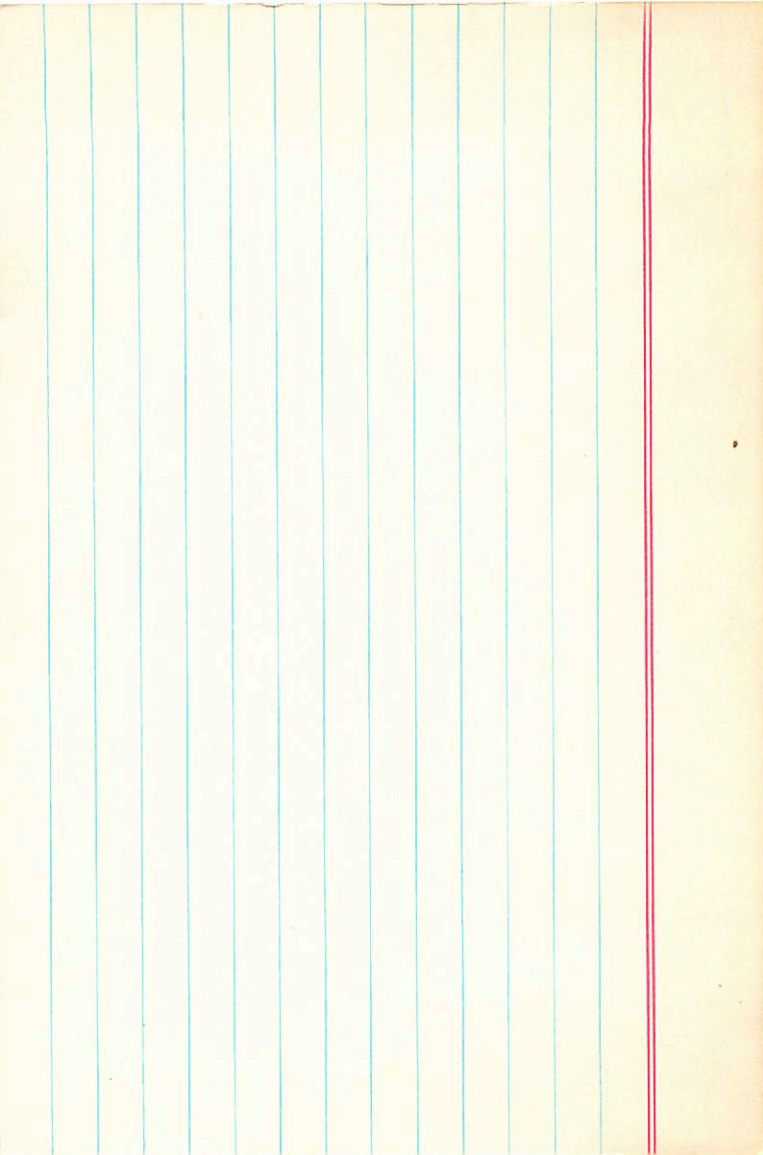
6402

| 02.2 -80 45 F80E-B -0.2 kg

F0637

8.24 +0.52 (1.62)

+0.65 +.024 CP →



6403 24M

1 02.2 - 33 48

+18.85 Ven
6.43 1107-11

661047

+ 30 1/2 + 9

-0048-017 Sky

-00454-0186

-0506
-050-450-
-020

7860-505-0186
1014-4109
5554-00449
4650-0574

0189
3.12

405

7386

$$6386 \quad 1 \quad 02.3 \quad +5 \quad 23$$

$$+0016 \pm 2.2 \quad -010 \pm 2.1$$

$$+0024$$

$$-013$$

$$6.2 \text{ gms} - 15.0 \text{ g}$$

615

1895

$$1301 \quad 1 \quad 2 \quad 16.984 \quad +5$$

$$23 \quad 19.511895.6$$

$$\frac{082}{902}$$

$$\frac{.54}{20.05}$$

$$0 \quad 5-9.326$$

$$1 \quad 17.428$$

$$2 \quad 16.954$$

$$024$$

$$16.978$$

$$16.985$$

$$16.985$$

$$2 \quad 16.988$$

$$\pm 0.09$$

$$\frac{97}{97} \quad +.083$$

$$97$$

$$16.982$$

$$\pm 0.199$$

$$15 \quad 16.48$$

$$8 \quad 3.418$$

$$12 \quad 19.196$$

$$164$$

$$19.40$$

$$5.6$$

$$+ \frac{.30}{.8}$$

$$19.32$$

$$+ 19$$

$$19.51$$

$$19.24$$

$$+ 3$$

$$19.27$$

$$1927.20$$

$$1009$$

$$1939.32$$

$$1934.4$$

$$1933.6$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

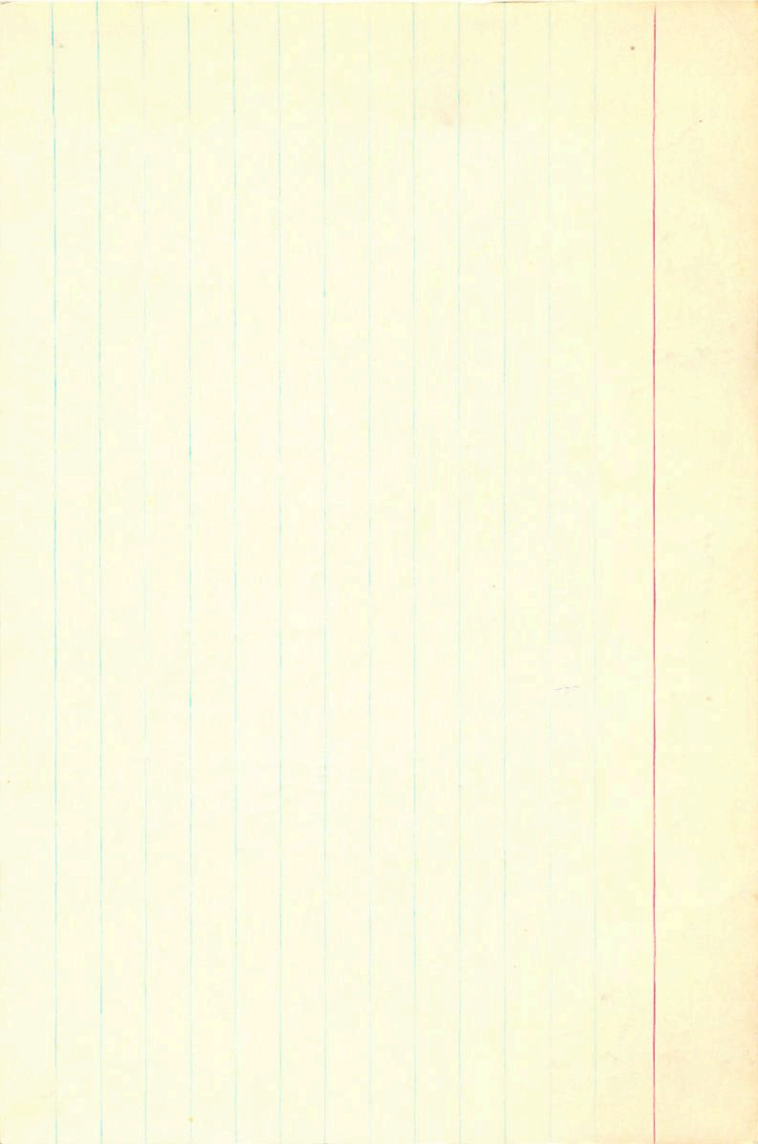
$$- .5$$

$$19.550$$

$$- .5$$

$$19.550$$

$$- .5$$



1302
6030F

+4 var?

1. 02.4 +14 40

1706397

40204

276 149 508 2165
+53

0000 +058 130
0000 +054 60 →
0000 +056

2 12 256

154 0

8220 389 414

1032

+16

-544 629 534

1667

+2.1

052 674 -737

1789

-3.0



-9
+2

66
354
104

+10.9

1406413 1 02.2 -48 13 6.83 +1592.57 112.11

001296

1571

+0053 +012
+ 4.5
- 4.2
+00156.0

+0069 54.0

+0051
19 013

10.223
-336

9.887

+0060
+ 09

+015 +015

3.171

6.935

10.106

10.055

10.048

10.021

140

31.39
-05
31.44

+012
+3

+13

33.72
3.45

30.27

30.35

6.2

30.07

30.69
7.5

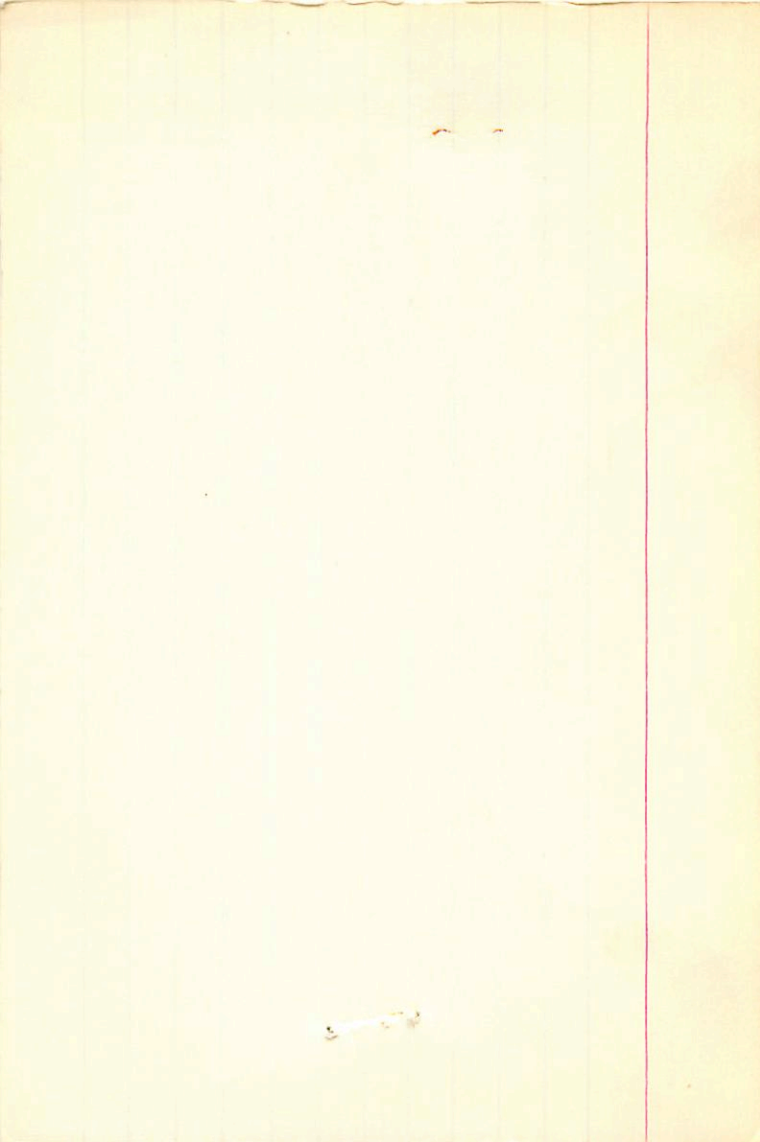
9958 5762

0265 2029

0612
-0004
-10.3

0064

1928.63
6.97



667

M2 III

6413

1 022 -48 13 6.53 +159 +10.9

6.80 +1.61 +1.94 (4)

5.92 +0.82 (3)

-55.4 9.1
10.0 -4 330 M.
4.54

8.20

+0053 +012 8.19 1970
+ 5 + 8.5

1.0058 +0165
1.0058 +012

1 0580
492
2857
7
060012
330M.

6.80 +1.60 +1.90
5.76 +0.80 1.1

35
52.5
10.5
4.20
9.7
7.6

822 544 -159
-566 960 -317
053 -351 -935

+1753 +0310 +2063
-1207 +0132 -0775
+0113 +0200 -0087

+68.0 +663 -1.7
-25.6 -29.1 -2.5
-2.9 -13.1 -10.2

570
485
2677
36

10756 + 012
55
Share
10758

10756 + 012

6413.000*

1.000*

2.200*

-48.000*

-13.000*

0.063*

0.021*

8.200*

436.516

10.900

0.300

-0.162

4

129.170

-0.093

-0.319

4

-44.228

-0.020

-0.934

-18.910

818

1 03.4 -32

10

~~712.8~~

AD6519

(4) C₅-

9.02 + 0.01 f(1.74) 64 IR - II

$$\begin{array}{r} \text{"} \\ -019 \quad -045 \\ +3 \quad -8 \\ \hline -016 \quad -056 \end{array}$$

6517 01 03.4 -26 34 +45.5 4692

FD1115

8.51 +0.64 (1.71) 6442

up 10.9
23.4 116.0

+104 -091
+112

8.92 +0.65 +0.09 (2)

8.83 +0.24 (3)
2.75

+104 -079
+4 -1
+108 -080 →

11.53 +1.03 +0.83 (1)

11.13 +0.41
10.75
10.2

5





2

6517.000*

1.000*

3.400*

-26.000*

-34.000*

0.100*

-0.000*

3.200*

69.15 43.652

45.500

0.205

0.055

417 11.435

-0.603

-0.019

5 -42 -27.178

0.023

-0.998

-44 -44.432

16.14
1324

$$\begin{array}{r}
 1 \quad 03.4 \quad + \quad 70 \quad 40 \quad -004 \\
 +0176 \pm 70 \quad -009 \\
 -001 \pm 3.4
 \end{array}$$

$$\begin{array}{r}
 26890 \quad 96.7 \quad +0163 \quad 52.15 \quad 96.6 \\
 -938 \quad +0149 \\
 \hline
 25952 \quad +0163 -005 \quad 52.20 \\
 +0162 -004
 \end{array}$$

$$\begin{array}{r}
 26689 \quad (46.06) \quad 57.23 \\
 70 \quad \frac{57}{96} \\
 \hline
 26758
 \end{array}$$

$$\begin{array}{r}
 26687 \quad (56.85) \quad 57.94 \\
 20 \quad \frac{57}{96} \\
 \hline
 26707
 \end{array}$$

365

01 03.4 463 41

8.98 + 1.30 + 1.21 ②

+ 0.565 ③

1/2

~~Weyfost~~
Weyfost
Weyfost

+ 1.520 + 0.290 Cui 15

- 1.1

9906 9979
1371 - 0647

1878
—
010
252
048
978

+63°137

00 57.4

+63 10

365

Y 217

60 M(6)

~~99~~

68 Y(5)

44 G(8)

81 S(10)

0.4
3.6 22.0

8.94 + 1.31 + 1.18 NTR R

9.01 + 1.30 + 1.23 JK

9.14 + 0.565 (2)

1525 + 340

1.5

0.15

Ci 18.142 + 1.52 ± 0.29

73 3.72
1029

8.95 MOp + 8.5
± 0.069

+1.520 ± 0.290

+1.546 + 333 MWR

1.507 404 6L

1.513 + 368 L

726

7.02

1.525

6.5

1.51

1.525 + 350

$+598 + 821 - 58 + 568$
 ~~-260~~ $-528 + 16 + 823$
 ~~$+177$~~ $+ 56 + 448 + 19$

13.5 gm.

$6.0280 + 0.899$
 $-4.1709 + 0.248$
 $+ 1.4111 + 1.5314$

| | | | | |
|---------|-------|------|-------|-------|
| 5.9350 | +77.2 | -0.9 | +76.3 | +79.3 |
| -2.8456 | -50.0 | -1.2 | -51.2 | -53.1 |
| +1.9425 | +25.2 | 0 | +25.2 | +26.1 |

→

9

76.000

+36.180

6476

1

03.4

+31

55

6.6

9.12

+27.58

628

1320

3

25.741

1898.4

+31

5.4

52.10

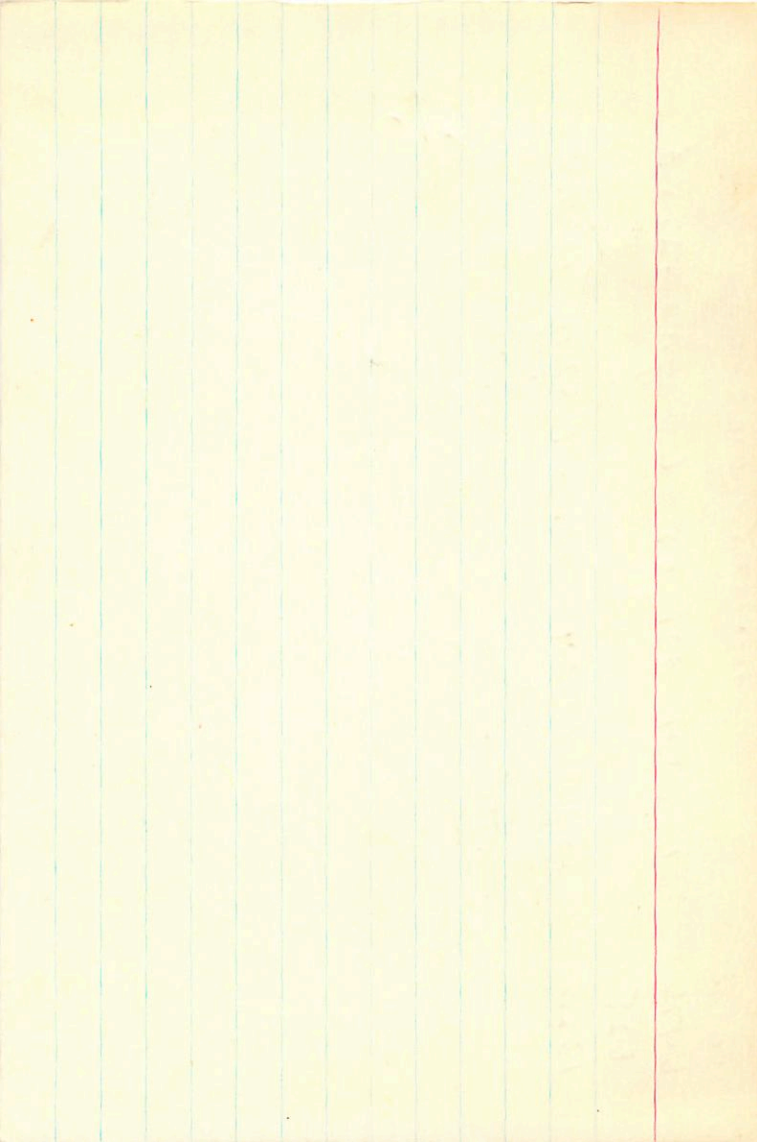
1889.5

$\frac{-036}{.705}$

$\frac{1.21}{53.31}$

+0007 2.5 -020 2.0

+14 ②



6560

1 03.7 -32 07 R3 III

+4.5

FD634

8.10 +1.09 (2.18)

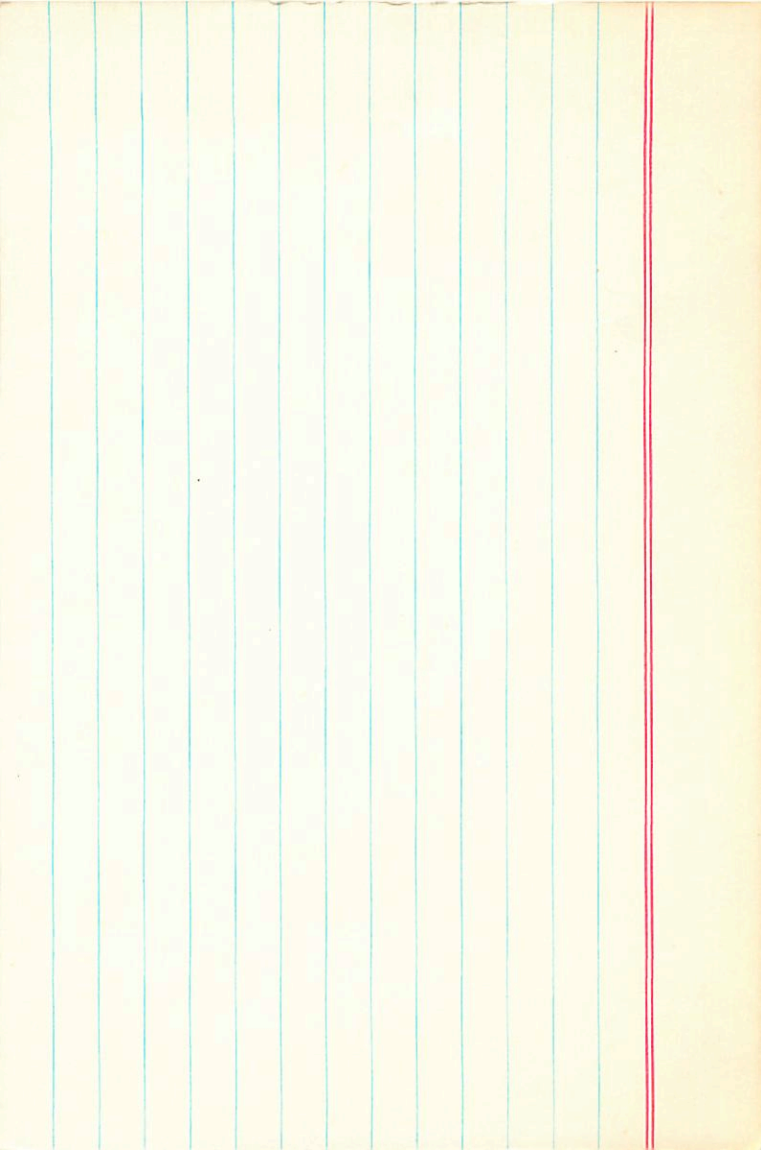
-0.032 -0.038 GP

-⁴

-0.032 -0.042

+ 0.06 +²

-0.026 -0.040 →



6525

1 038

+ 29

24

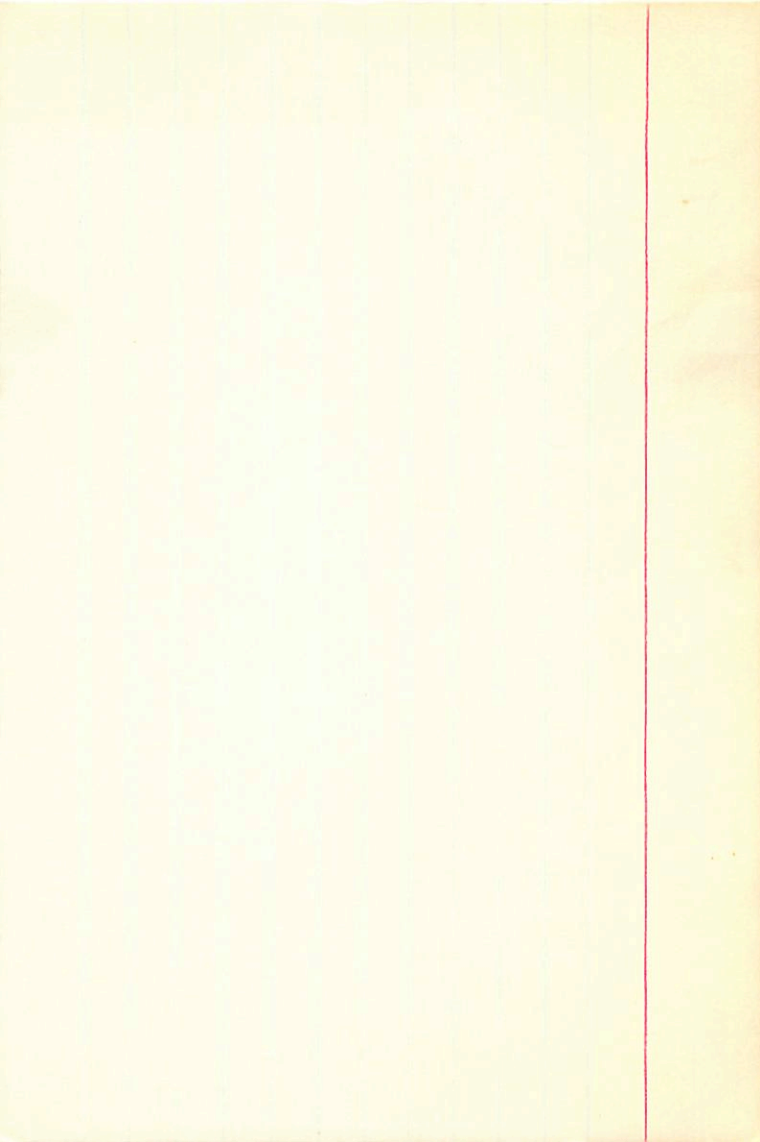
8165

- 2.4

12117

$$\begin{array}{r} +031 -052 \\ -10 \quad -3 \\ 0 \quad +2 \end{array}$$

$$+021 -053$$



6594

1336

01 070 -35 04

-0009 ± 7.5
 -0008
 -0005
 $+004$
 $8.10 + 061$
 -005

$6-37$
 -13.5 ± 0.9
 $9(14)$
 (11.71)

57.801 19090

037
 838

56.815
 9
 806

46.414

40.444

56.836

824
 909

56.815

-20
 79

-35 03 53.95 19066

68.75

53.80
 86

43.9

802
 036

39

53.56
 53.04
 1928.89

2.45

53.59
 37

53.98
 324

53.6

8585

42.9

36.3

53.84
 1956.96

53.76
 53.71
 $+15$

ADD 515

10²² 27¹¹ 6¹¹ + 0023 24.3

+ 002 23.5

46.5 (1)

6540 6540

11²⁰⁰ 04.2

+ 0021 + 53 14

6.5 120 + 6.5 8

637 APR 31

1343 4 10.242 1997.8 + 53 13 52.77 1844.0

$$\begin{array}{r} 120 \\ - 120 \\ \hline 0 \end{array}$$

$$\begin{array}{r} -11 \\ \hline 52.66 \end{array}$$

$$\begin{array}{r} 2 \quad 41.18 \\ 1 \quad 21.838 \\ \hline 10.0183 \end{array}$$

$$\begin{array}{r} 5 \quad 51.2 \\ 8 \quad 2.50 \\ \hline 52.70 \end{array}$$

$$1927.3$$

$$\begin{array}{r} 10.209 \\ - 1.93 \\ \hline 8.279 \end{array}$$

$$\begin{array}{r} 13 \quad 52.45 \\ - 2.55 \\ \hline 49.90 \end{array}$$

$$1199.5$$

$$\begin{array}{r} 10.216 \\ - 2.09 \\ \hline 8.126 \end{array}$$

$$\begin{array}{r} 52.5 \\ - 2.5 \\ \hline 50.0 \end{array}$$

$$399$$

$$\begin{array}{r} 10.216 \\ - 2.09 \\ \hline 8.126 \end{array}$$

42.2

$$\begin{array}{r} 52.65 \\ - 2.65 \\ \hline 50.0 \end{array}$$

$$1945.64$$

$$40.0$$

$$\begin{array}{r} 10.227 \\ - 2.25 \\ \hline 7.977 \end{array}$$

$$\begin{array}{r} 52.40 \\ - 2.40 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} 52.45 \\ - 2.45 \\ \hline 50.0 \end{array}$$

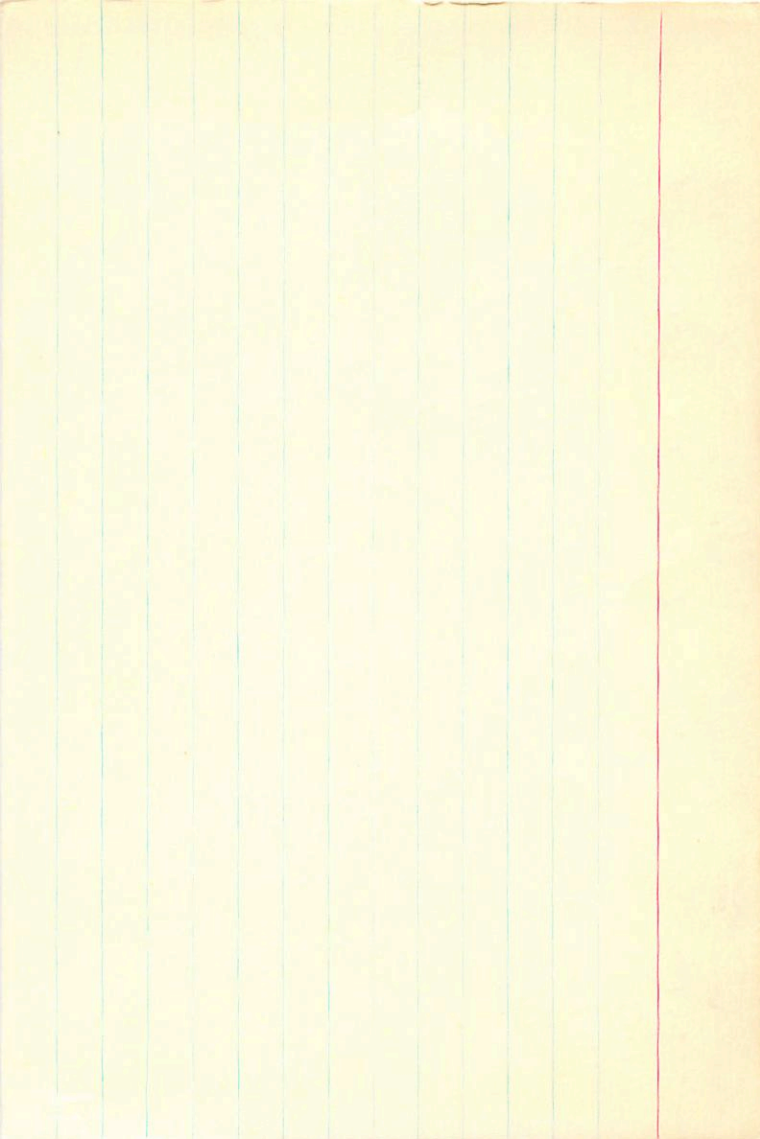
$$\begin{array}{r} 46.0 \\ \hline 46.0 \end{array}$$

$$\begin{array}{r} 52.26 \\ - 2.26 \\ \hline 50.0 \end{array}$$

$6.7 \left. \begin{array}{l} 4'' \text{ gain} \\ 7.5 \end{array} \right\}$ +0044 = 41.0 +00423.1 B 8.3 dF3 -1.0 f
 +0044
 6651 1 04.6 - 2 00 7.5 dF6 -6.3 f
 643 -3.68

1354 4 37.607 1895.8 -1 59 56.440, 891.5
 -235
 .369
 3667 -23

321.005
 116.480
437.533
 437.013
.549
 .512
-
 .536
.536
 +.167
 -2 57 5-8.62- 1933.89
 8 2.10
 -1 59 56.52
 -37
56.89
 56.89
-
 56.87
 -20



+74.29 H18312

6473 1 04.9 +78 45 Ag 66

-25.9 (3)

-2248

G-61358

w(12.5)

-2250(6)

-2250(4)

w644

6.4

-18 -17 -18 .017

-026±3 -028±3 GC

-006

-042 CA2

-024

-030

-0099=30 -033=2.8

288 960 984 178 -024 -035 -27.4 -034 -27 -028

007010 -023 -033 150 -062 -4.9 -5 -1

+6 -5 -29 017

-15 -17 -18

51255 1891.0 +79 44 44.50 1890.0

~~1584~~

~~839~~

1.98

46.48

78PAC
6680
G-C1368
W 651

HR 307
28/1/66

1 05.2 +01 45 DATA 144
6.25 +0.40 -0.01 F51UR
S=0.2

Stoddard

+0156 ²³ -028 ²⁴ M30
+0155 22.6 -032 ^{22.1} Cc → M30

+01519 -0256 PAY Smp

2027
209-030

+1555 -030
PRY 01557 -0285

+56 -31 -11 .015
+43 -21 -10 .02

~~196 2033~~
224 934

+200 -034 G-C
+200 -028 N
+200 -026 F
+200 -029

9769 1.0000 2640
2135 10010 -0302

Hypoderm

-6.4

3.81

250860 526 850 +200 -029 +142 -055 +7 -115
-056 004 192 -014 -199 929 +11.9 +11 +3

+1 +49 +1

020

+43 -20 -5

+3 +40 +2

025

+36 -14 -5

022

+40 -18 -5

23.5

-5 +43 +2

+39 -19 -2

4

355

6680

3.0

1 5.2 +31 '15

FS 14

354
358
362

HR327

6.25 +40 00 (2)

CC1868

78Pnc

.268 .160 .522 (2) SPC 24770^{ct}

[m] 208 +11

Prob Work 272

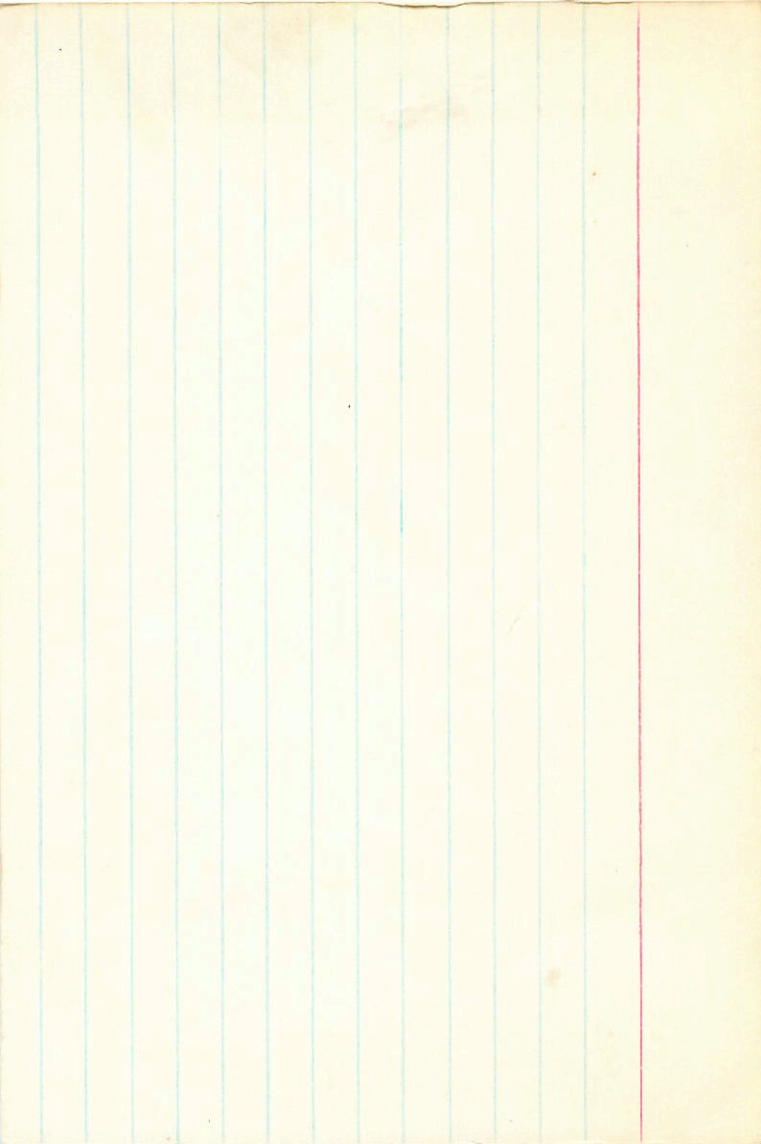
[G₁] 468 40
50

3.22 +41 -168 -11

+0.156
-0.030

(+15.0)

-7 -6 -7 / 11 pm



37²
54

6706

1 05.2

-10 03

df3

HR329

5.87

661369

30604

281 185 504 - 3599

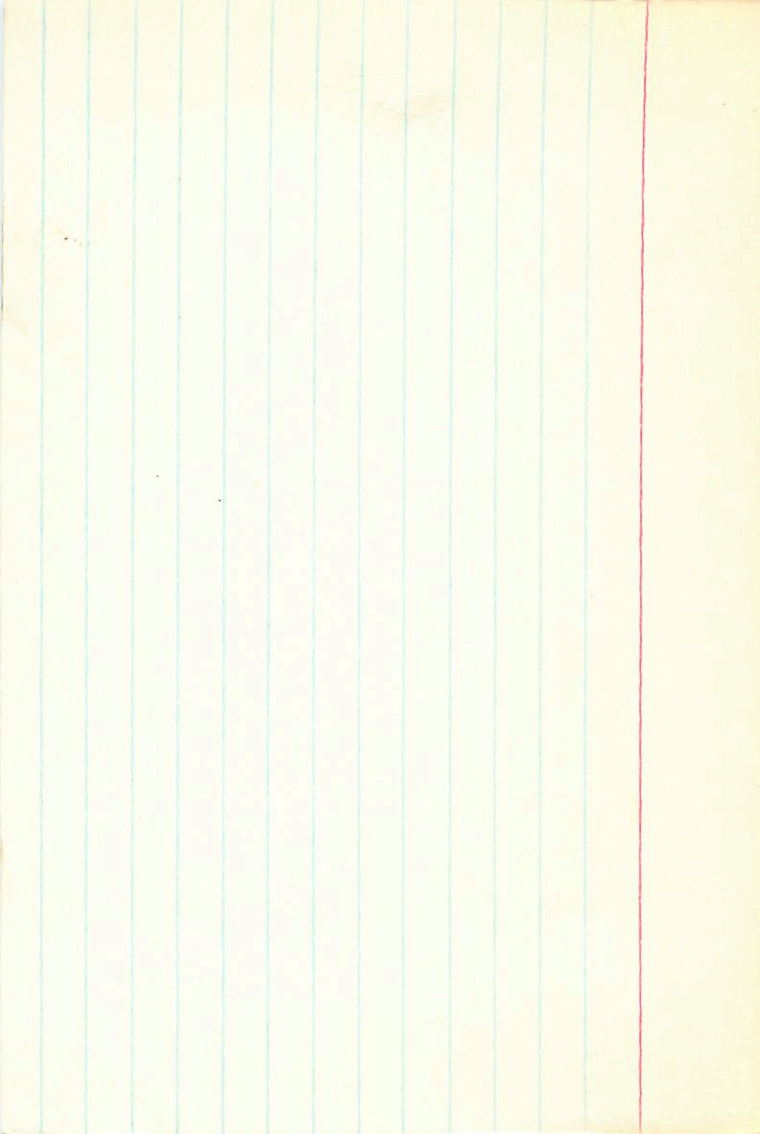
293

261 813

[m] 236 ~~46~~ -15

$\frac{44}{52}$

[5] 414



2270-148 07 05.29 - 8 30 00

4.224

6718

+150 023

8144 65 17 10

9867
1623

9902 9906

1917
-0039
-0.9

(A) Alpha Bank S¹

0202

3.47

MV = 15.51
PV = 40.2 9.47 0.398 0.205 3862.605 (3)

(3)
+348 C

+0218=5.7
+248
+0196

6101 0 59.8 +4 47 8.4 d/26 +19.76

589

661245 59 48.247 1901.0 +4 47 22.33 1898.7

$\frac{1.068}{47.179}$

0.214 2.24 2.24 - 11.54
10.179

47.935
 $\frac{14}{952}$

5.2

20.21 1937.91
20.28

30.6

$\frac{1555}{778}$
 $\frac{1599}{599}$

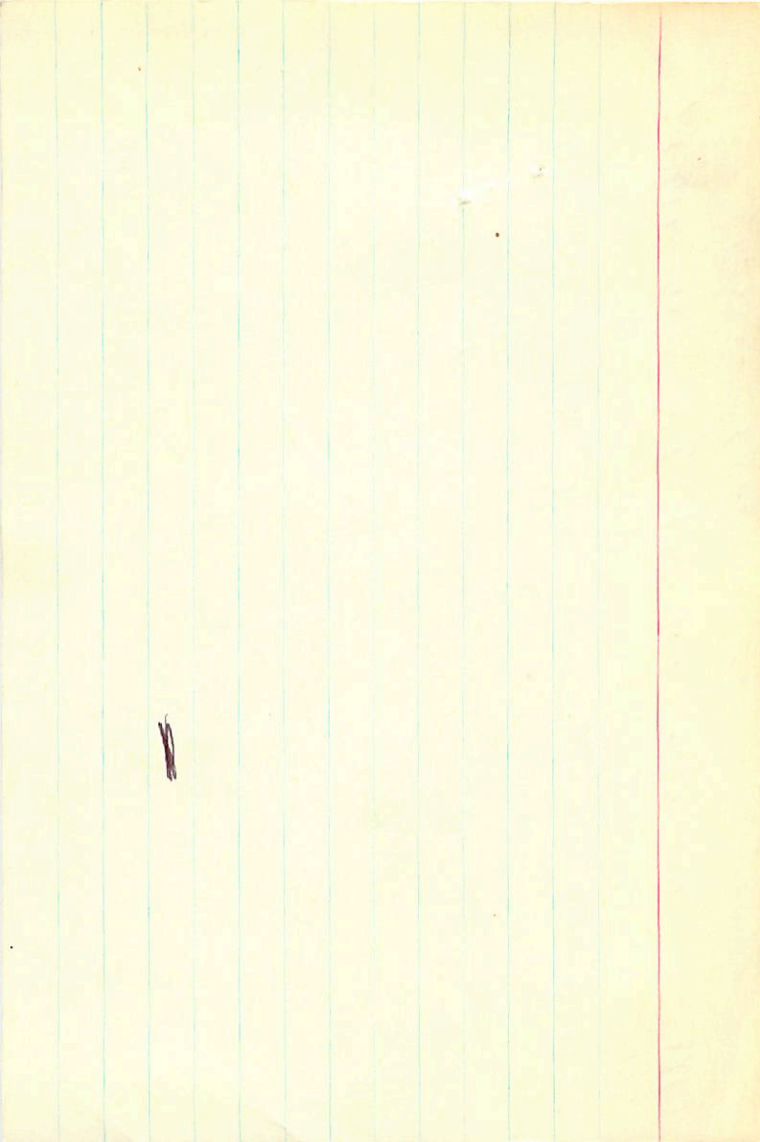
6311
31.6
32.9

30.1688
17.5068
47.6621
6.88
60.3

13.0 1425.2
4.86
17.38
17.50
17.54
17.64
+8.17

328
224
1.5
+19.7

3792
18.96



RED.
MOD.
DISEASE
PLANT

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|-----------|---|---------|
| R.A. | : | -1.000 |
| DEC. | : | 4.800 |
| PM. R.A. | : | 328.000 |
| PM. DEC. | : | 224.000 |
| DISTANCE | : | 1.500 |
| MODULUS | : | 20 |
| RAD. VEL. | : | 19.700 |

| | | |
|--------|---|----------|
| q1 (U) | : | 0.826 |
| q2 (U) | : | 0.458 |
| q3 (U) | : | 0.330 |
| du | : | 1764.989 |
| U | : | 41.718 |

| | | |
|--------|---|----------|
| q1 (V) | : | -0.563 |
| q2 (V) | : | 0.712 |
| q3 (V) | : | 0.420 |
| dv | : | -115.625 |
| V | : | 5.975 |

| | | |
|--------|---|---------|
| q1 (W) | : | 0.043 |
| q2 (W) | : | 0.533 |
| q3 (W) | : | -0.845 |
| dw | : | 631.680 |
| W | : | -4.046 |

6139 00 59.8

-31

53

8.79 +0.51 (1.62)

PPM

6055-029

070-029

052
-029

5.8

+25.1

8.79 5.71 60 IU

60 IU +25.1 +0.51 (1.62)

R.A. : 1.000
DEC. : -31.900
R.A. : 82.000
DEC. : -29.000
DISTANCE : 5.800
MODULUS : 145
VEL. : 25.100

q1 (U) : 0.826
q2 (U) : 0.564
q3 (U) : -0.009
dU : 194.920
U : 27.953

q1 (V) : -0.563
q2 (V) : 0.822
q3 (V) : -0.088
dV : -298.619
V : -45.382

q1 (W) : 0.043
q2 (W) : -0.078
q3 (W) : -0.996
dW : 24.765
W : -21.101

2

667

112 III

6913

1 022 -48 13 6.53 +159 +109

6.80 + 1.61 + 1.94 (4)
5.92 + 0.82 (3)

6.80 + 1.40 + 1.90
5.76 + 0.80 + 1.1

- 554 9.1
100 - 4 330 M.
4.54

5.25
1.05
4.20
93
1.10

8.20

570
485
285
77

+0053 +012 878 1920
+ 5 + 85
+0058 +0165
~~4445~~ +012

10580
492
2857
77
060012
330M.

822 544 -159
566 960 -317
053 -351 -935

+1753 10310
-1207 +0432
+0113 +6200

+2063
-0775
-0097

+68.0 +663 -1.7
-25.6 -25.1 -2.5
-2.9 -13.1 -10.2

+0258 + 012 Sharp
+0585 + 0165

+0064 +032 +1c Fly
+0585 +0165 Sharp → Fly
+0061 +025 Fly

+0610
+063 +021

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