

Part

Q Am Si 5 56.3 +37 12 89.5 Aop

(+21.4)

2095
40312
7557
2.42 -08 -26.35

2.928
159
2.928
2.928

(9)

274
1247

-040 +186 +966 2.769 2
+60435 -0855 ±1.0 604 5.9
+80405 -0833 +74.36

2.928
2.769
(15.9)

E = +0.3

(3.15)

V₀ = 2.53

0-V₀ = -11

11-130 -28

MV-0.95

5197 2247 } 0.812
6115 0745
8544 -9744

+04583
+047-083

11417
18040-058

78



2095.000*

5.000*

56.300*

37.000*

12.000*

0.047*

-0.083*

3.500*

50.119

29.300

0.045

0.988

+31 33.3 31 31.188 +31

-0.450

0.098

-14 -14.5 AT 19.682 -14

0.000

0.117

+3 13.6 3.441

140

5.988

37.208

58.888

-78.888

2.758

35

38.888

-8.844

-8.143

8.989

44.687

31.246

-8.584

8.657

8.182

-412.234

-11.571

8.882

8.494

8.118

-19.981

2.598

70

+100967

+8

Darlin

5 57.6 +10 13

$\sum +0002 +007 T(60)$

-009 +004 Y

+ 1 + 4

-008 +008 (00)

- 2 + 3

-010 +011

- 2 + 010

$\boxed{-006 +010} \rightarrow$

450 m.

-057 324 944

-497 810 -308

865 487 -115

-0016 +0154

-0141 +0384

+0246 +0231

+0138 +6.2 +4.7

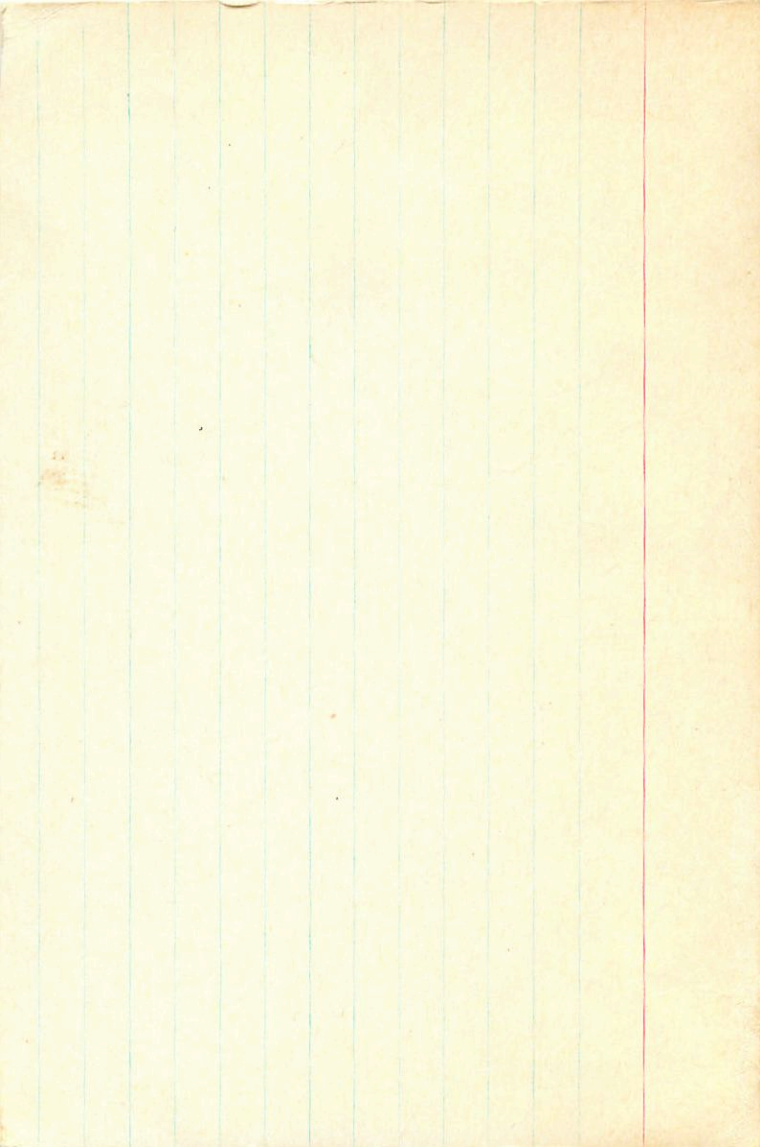
+0243 +10.9 -1.5

+0477 +21.5 -0.6

+11

+9

+21

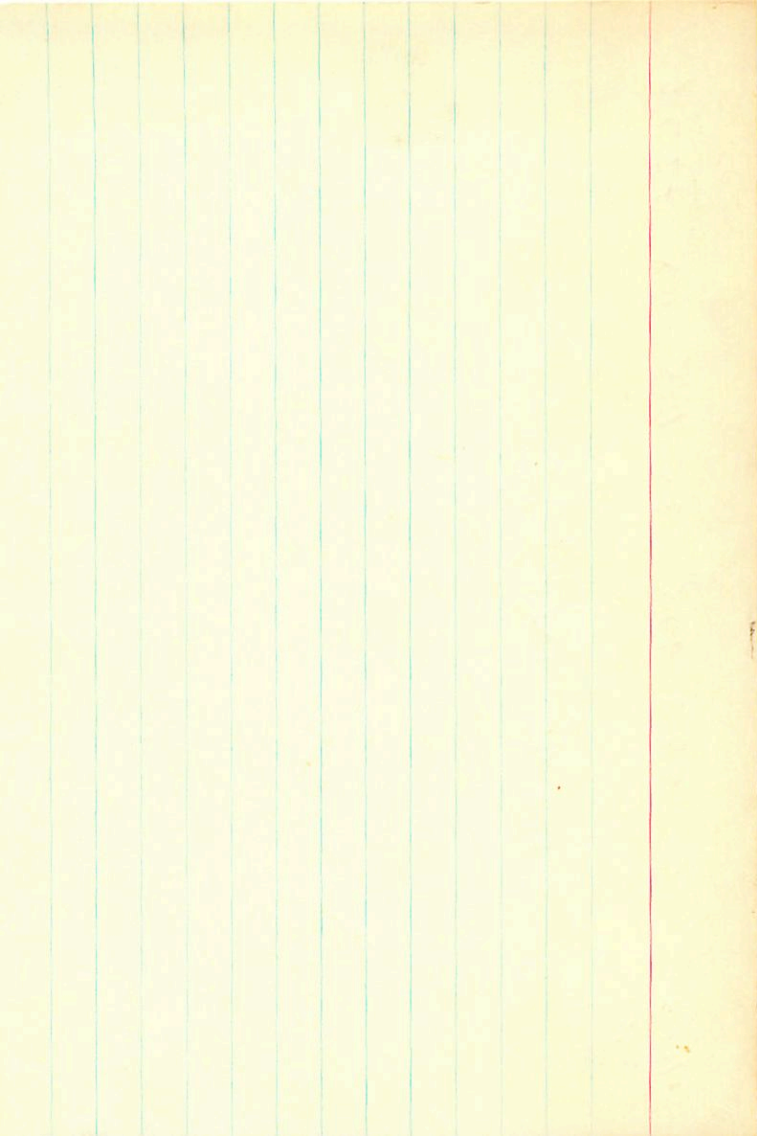


40055 S 583 +75 356.5 N5 +3.76

3761

7606

29
+0044 -003N30



38847 S 58.9 +85 00 dg2 -702 w(4)

GC7617 8.86 +0.58 +0.12 G05 R

W3766 $\delta = .01$

Y1331

+840112

-81 -39 +2 .015
-70 -41 -6 .020

+091 +152 GC
+087 +164 FAZ

+090 +156

96(12)
292(12)
15±6

AD40887 S 58.5 -31 02

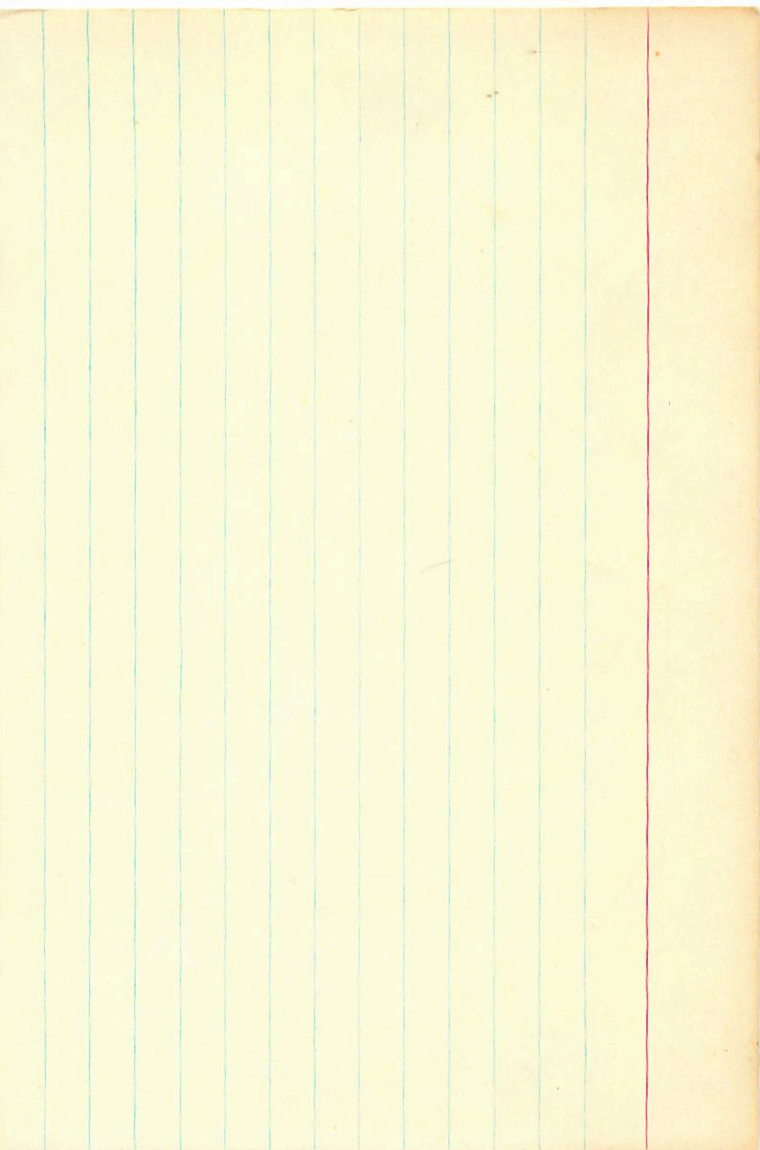
P = 103.4

Triple Sigma

-0.398 +0.400

-0.060 -0.460 0.865 500 +1.132 +8.678 -1.6318
0.864 0.404 0.293 -766 +1.6381 +7754 1.5552
0.500 -0.766 -0.404 -1104 1.7513 1.6932 -1.0966

+51.7 -79.2 -41.8



HR2131

5 59.5 -38.55

5.54 1.58

GL 7630

WB 769

27.519
-081

488

1505.3

+0007 ±3.6 -021 ±3.1

34.49 1502.7

+75

33.74

+0004 -016

+0004 -016

150 No. 27.481

-6

27.475

013

27.481

-069 889 483

-493 366-790

868 276-414

-0013 -0674 -0884

-0094 -0277 -0371

+0165 -0209 -0044

39.649

+22

39.477

1988.62

-10.2 +8.6

-5.5 -150

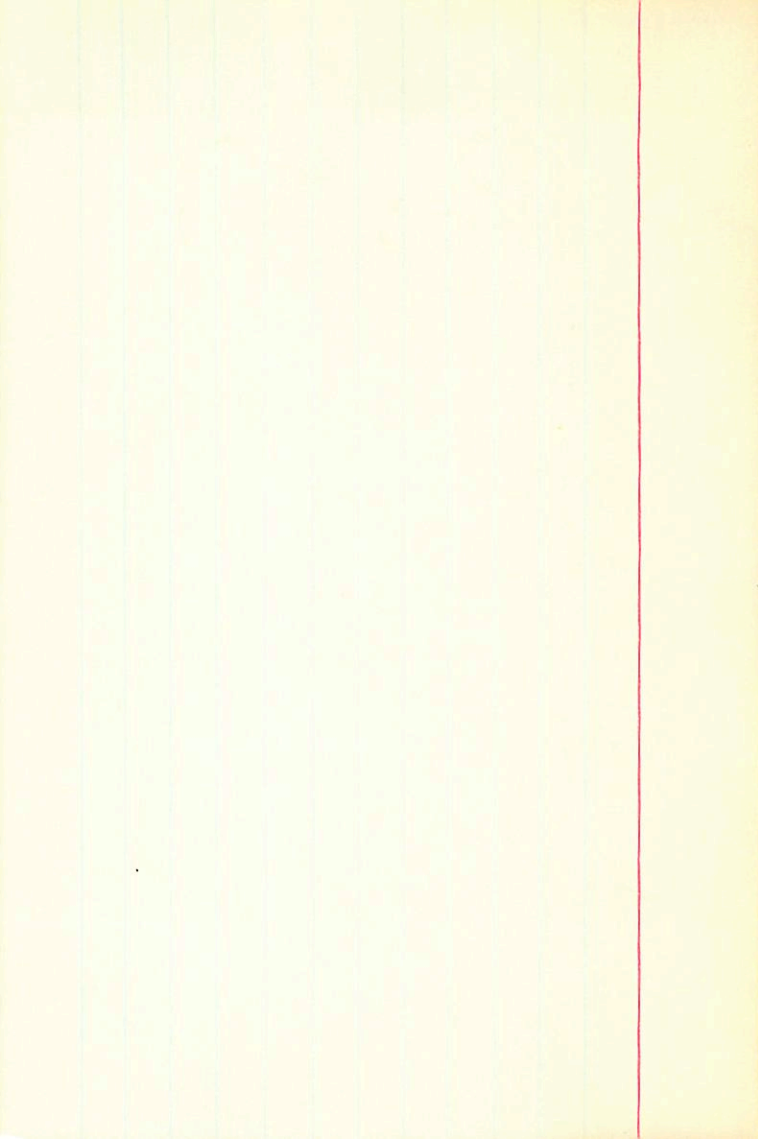
-3.0 -7.9

39.93

-2

-20

+16d 1d
W52



u di

HR2124

5 59.6 409 39

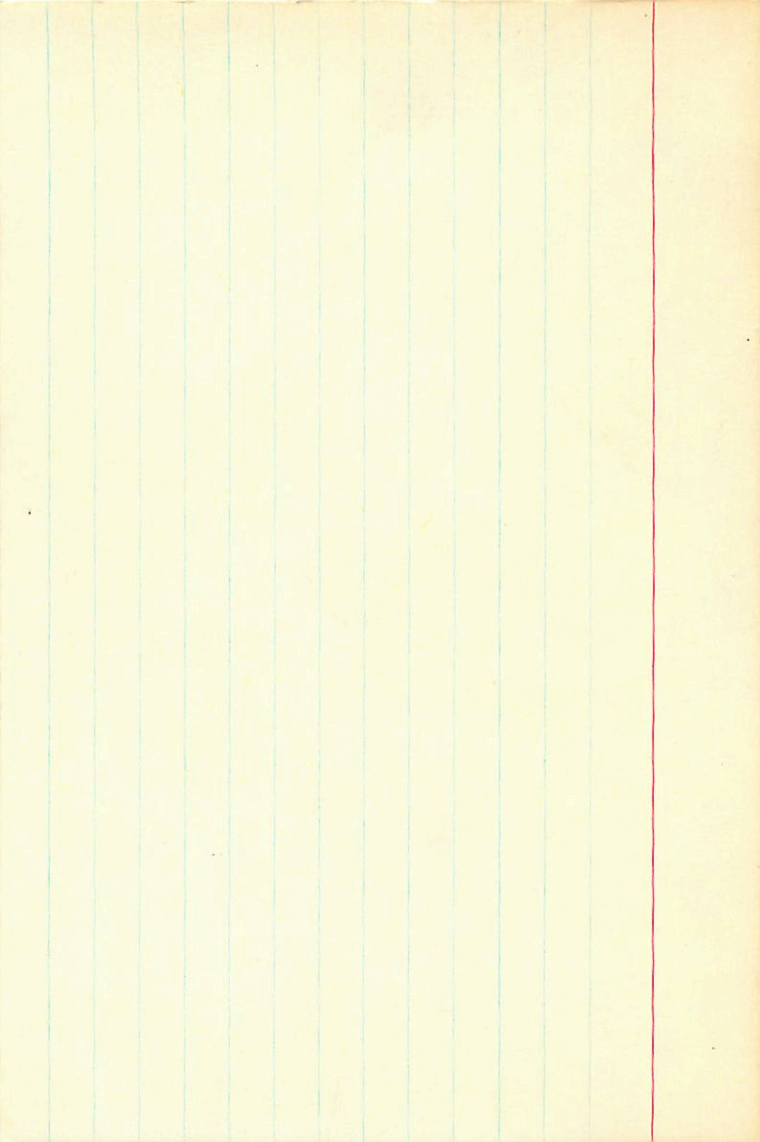
44552

Am

+016 -02962

+013 -030N30

42.0
Order



40932 5 58.6 432 35 d. 155 434.18

HR2122

6.23

290 158 487 7650

1082 - 2126
1086 - 2056

40832
7634
76313

1082 - 212
1080 - 212

40 ps.

-067	-060	996	-0308	+0602	+0244	+1.1	+34.0
-493	470	020	-2264	-8742	11006	-440	+0.7
816	489	086	3972	-4914	942	-3.8	+3.0

+35.1
-43.3
-0.8

1 0 535 842 +1096 -205 134.1 -110 +15 -820

-096 119 00 -389 570 +25.7 0 +29

-455 531

-10 +43 -3

04

-8 +40 +1

05

+34 -20 +1

4054617 5 53.6 +9 39 +45e

.0256

4.12 10.155 10.05 +016 -027 H1

+0.13 -026

20.5
+40.5
+1.5

20.5
+42.3
-14.4
-5.0

1.0
-2.7
-0.2

-0.483
-13.76
-0.109

-0.67 +333 +940
-493 +808 -321
+868 +485 -110

-0041 -0442
-0304 -1072
40535 -0644

1 000 165 556 016-027 445 -005 +8 -125[✓]
016-005 0 0 076-024 445 0 445 0256

+3 444 +3
440-17-5

mlw

5 59.6

+9 39

1984981

+0011 -024 ±18

378996.2

+0010 -031

AcireliA

-048

+0005 -038

4080h

37869

+0008 -034

+14

+0008 -033

3883

+00063 -0318

5115

+00593

0252

9116 9255
9438 -3688

37865

5608

6660

+19
884

-9
3559

6660

37876
858
+258
004

557 6912
-18
2527

2919

Perseus

5657 5.9

125
886

57.77 88.53
+6
5683

Corvus

41340

5 54.8 -62 00 F2 +5.4 256.

8.8 +0.52

-046 -120 CP

-048 -126 → 00

+ 6 + 3

-042 -123 →

6.000
-62.000
-90.000
-123.000
5.500
126
5.400

-0.067
0.998
-0.017
-568.210
-71.626

-0.493
-0.048
-0.869
126.704
11.259

0.868
0.050
-0.495
-202.748
-28.196

71

41172

6 00.1

-0021±9.5
-1007
-27 25

-106±8.3
-086

-5.4±0.8 C, (5)

7.11 +44 FSTU-D

7654

7.352 1899.6 -27.25 29.32 18975

$$\begin{array}{r} 100 \\ \hline 7.458 \end{array}$$

$$\begin{array}{r} 5.56 \\ \hline 23.76 \end{array}$$

$$\begin{array}{r} 7.928 \\ 59.485 \\ \hline 7.413 \end{array}$$

34.5

$$\begin{array}{r} 27.94 \\ 1.90 \\ \hline 26.06 \end{array}$$

1934.59 811
34.1

$$\begin{array}{r} 420 \\ 19 \\ \hline 439 \end{array}$$

$$\begin{array}{r} 437 \\ \hline .02! \end{array}$$

$$\begin{array}{r} 26.06 \\ -1.09 \\ \hline 27.15 \\ +2.25 \\ \hline 26.90 \end{array}$$

26.90 36.6

$$\begin{array}{r} 7.420 \\ 15 \\ \hline 435 \end{array}$$

$$\begin{array}{r} 27.15 \\ +2.25 \\ \hline 26.90 \end{array}$$

27.14 1933.52
26.89
-3.14

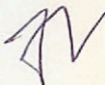
2

6.000
- 27.400
- 6.000
- 96.000
4.500
79
- 5.400

- 0.067
0.831
0.552
- 376.419
- 32.883

- 0.493
0.454
- 0.742
- 194.061
- 11.405

0.868
0.322
- 0.379
- 168.375
- 11.328



+8P201
39861

6 00.2 +81 31 8.9 d65 -27.08

7655
3784

-0368 -372 →
-0256 -381 → +30

-310 -376

-0004 ± 16.0

~~+0371 ± 19.0~~ C.C.

-0378 ± 6.4 -372 ± 5.4 C.C.

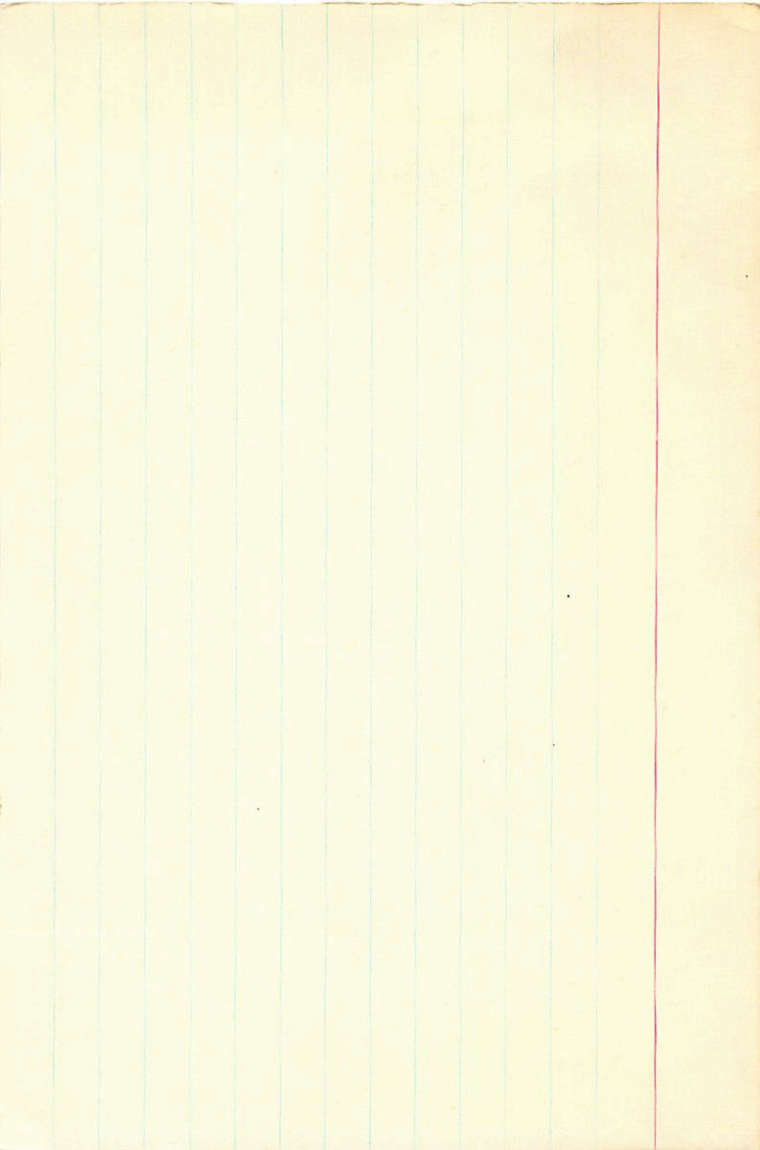
-0266 -059 -381 Q.P.

-073 -327 G

-067 -792 +607
-493 +855 +670
+868 +254 +427

100P

+0219	+1.4115	+1.4333	+143.3	+16.4	+1269
+1609	9891	-8283	-82.8	18.1	-100.9
-2831	-4527	-7358	-73.6	-11.5	-85.1



40859 7657 6 003 +27 39965-2.58 w(3)

8.5 -120 (A) w(+2.4)

w3786

+20963

opt. q. nos 4629

+1315 (B)

17.917 1902.7 +27 38 425-2 18943

$\frac{-24}{893}$

GL 7657

128.04

+006±5 -040±4 cu

43.17 -4
43.13

17.834

$\frac{4}{410}$

+0005 ± 6-4 -040 ± 3.8

1 0 464 856 +006-040-2.8-019-1-164 ✓

-026 019 0 0-025 098 -2.5 0 -2

-6+16-34

005

$\boxed{-3-36-14}$

000 124

+0013 ±7.5 -051 ±4.9
+0010 -055

±0.4 (4)

40827

6

00.7 +59 24

68

+31.478

7667

636

6.24

2.1

+010 -051

3793

41.604 1905.9 +59 23 5065 19018-002 -048

-057

700115 -003

2.46

7004

-050

(2121)

700080 -0521

53.11

208

28.25
133.07
41.556

30.9

50.5

1928.3

100-20

55.4
58.2

577

3788

73.5
36.8

Surf

40.30

51.42

51.42

51.20

35.0

41.540

70061

51.7

1945.21

7597 1299

41.533

7009-052

50.83

6004 -9915

0527

41.542

1447.01

50.6

1447.01

0027

41.566

100-50.50

50.94

1447.01

0069

1 0 861 509 +004-050 +31.4-043+27 -11 $\sqrt{5}$

-004043 00 -019 20 $\sqrt{2}$ +16.0 (B) +14

-1 +36 +14 0-1

-3 +45 -+10

007

+45 -14 0

2005 1200 0.1

2005 1200 0.1

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2005 1200 0.1

2005 1200 0.1

$+470$ 410
 40708 L 00.8 +67 39 8.8 265 +486 4W
 7671
 3796

$+0055 \pm 7.8$ -308 ± 10.6 SB(26)
 $+0065$ -303

50.953 1906.1 +67 38 55.19 1909.1
 $\frac{-241}{.712}$ $\frac{12.60}{7.79}$

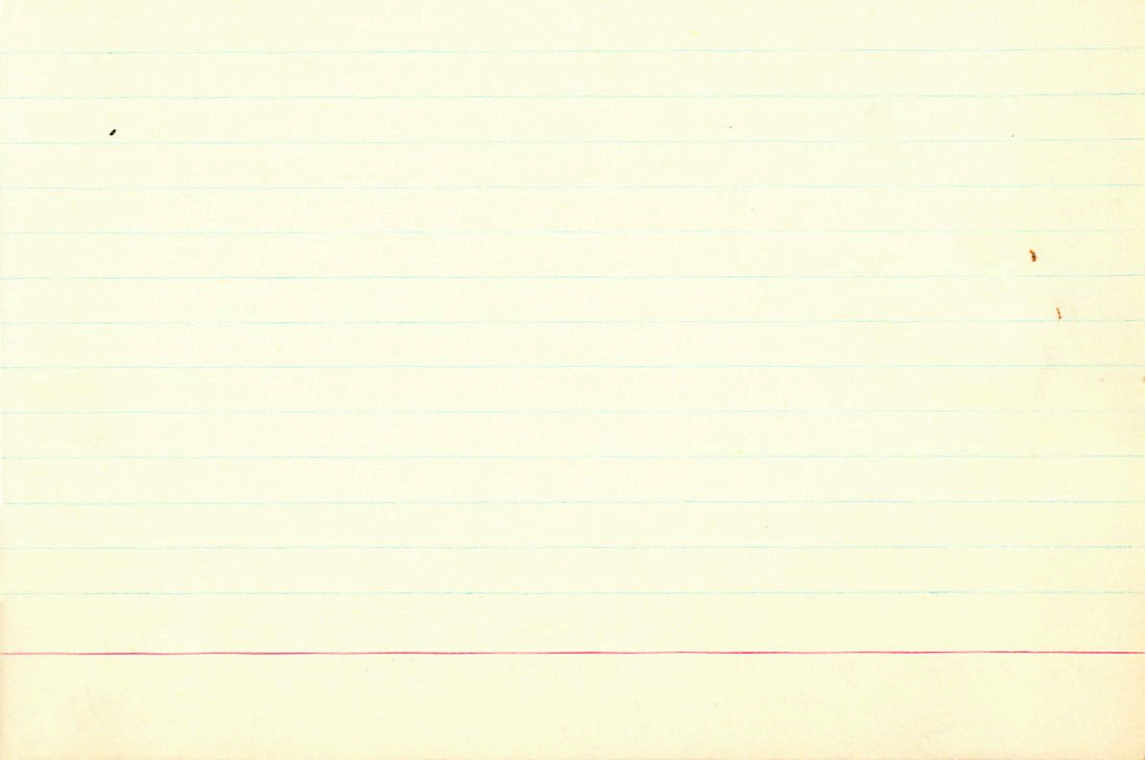
26^L-8

50.81
 $\frac{57}{.867}$

1.5 1930.1
 $\frac{-8}{1.42}$

M
G

$+0068$ +039 -335 GP
 $+0055 \pm 8$ -308 ± 10.6 GL
 $+0065$ -303 RW



11/24/79

6 010 444 14 + 821 188

4-25 FS

40788-153 *Sanchez*

4095-153

182

-153

225

1821

3

H1304

G-07698

W0814

Y1400

T140136

6 024

6.6

12.5
117.9

+24	-56	+1	.020
+19	-72	0	.015
+21	-64	0	.0175

3.40	+232	-54.0	-5.0
	-251	-428	-59

50000 +365
-184

758 A(16)

+106 -11

$$\frac{6.900}{361}$$

$$7.161 \quad 1500.5 -$$

$$249 \quad 569$$

$$+0073 \quad 59.5 -$$

$$-175 \quad 78.7$$

$$+14 \quad 23 \quad 43.91$$

$$1898.0$$

$$+9.10$$

$$53.01$$

$$46.22 \quad 19338$$

$$46.36$$

$$44.87 \quad 1940.08$$

$$+10$$

$$44.97$$

$$3.98$$

$$133$$

$$36.9$$

$$45.66$$

$$38.9$$

$$-7.35$$

$$(36.4)$$

$$7.002 \quad 7908$$

$$+ .204$$

$$6.987 \quad 29$$

$$7.016$$

$$6.964$$

$$7.002 \quad 33$$

DISTANCE
MODULUS
VEL.

28
32.100

-0.065

16:

96

45

42

1.49

0.84

0.19

35.52

-17.2

0.8

0.5

0.

54.

7.

41452

6 02.2 -35 07 12.10

C₄₄
+13.98

9.81 + 1.14 (2.20)C

889 + 1.12 + 1.12 (1)

9.36 + 0.40 (2)

4+6 795
514 7.7
(8.4)

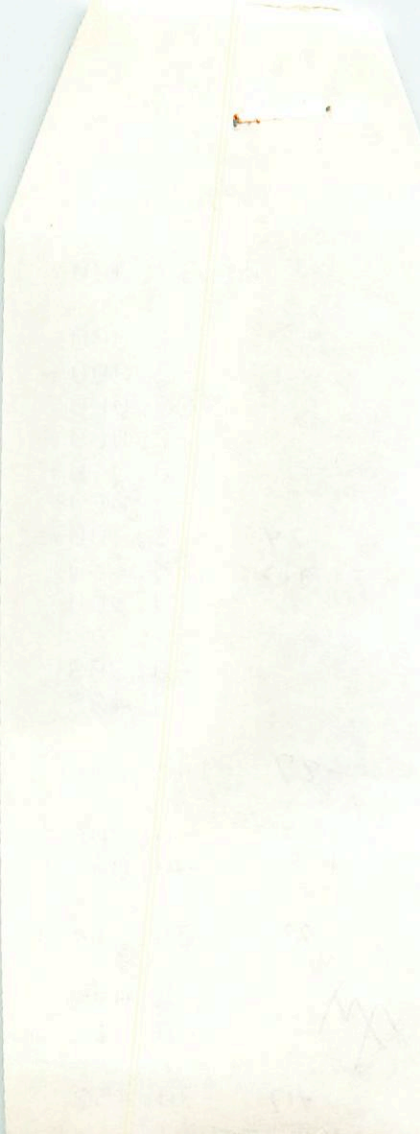
+0024 -064

+0356

4640-064



7/1



41492.000*

6.000*

2.200*

-35.000*

-7.000*

0.040*

-0.069*

7.4 0.400*

802 478.630

13.900

-0.308

0.435

-87 -141.236

-0.206

W0 -0.801

-73 -109.814

0.076

-0.412

417 30.452

HR2149

6 02.5 +32 10

+105.1 8 (15)

5.64 -0.20 020

-017 +1296

1 0 -533 846 -017 +129 +105 -069 -056 -56
017 069 00 081 327 +89.8 0 +89 516 516
256

+40 +253 +202 002

+120 +160 +55

+8 122 -4 01

+106 -54 -29

+4 +95 -30 02

+70 -64 -32

41534

41839

667708

W3819

6 02.5 -32 10

5.64 -0.20 B2R

(1.21)

-0015" +124" N30

-0013 ± 5.0 +128 ± 5.3

HR2149

+152-23 -12 .005

2865

+105.1 H.P. C, (5)

+92.8 L(10)

+98.6 W(3)

+99.08

+70.356 var

-017 +129 66

-019 +124 N30

-018 +126

John ...

John ...

2442

1 0 -533 846 -018 +126 +94.0 -067 -53.502 ✓

+018 067 0 0 0 85 317 +93.5 0 +84

+17 +147 +47

005

+152 -23 -17

+28 +190 +114

+222 +15 -2

003

+8 +116 -3

01

+104 -45 -30

4/19/0
+0°1270

664140

48.184 001
659
249

-0013263
+0001
+0001

-010263
-008 441 714
-003 83
524

6 028
+00 87 0

48.230
124
659

70.00

467
0

48.227
124
N/S

6308

745
0

+260 1067 6 02.8 +26 34 d.K6 - 91.56w(3)

W3824

41404 (39847)

CC366

9.42 10.88 10.66

1125R

S = -06

9711

98226

(19)

983

-186 -371
+ 24
-175 -367

-19 -37
-174 -366 Y

-90 -43 -75 .0225 -0.131

-0.130

-183 V(R)

10M(7)
15Yk(7)
21V(14)

-190 -370 (M-V)
-16

-196 -376
+3 -1

1746

FL -193 -377

126
36
11

448834

49112

6 030 ~7 48

247 (099) (226) -233
✓ 099 107 208 2644
999 (352)

41547

3827

7721

NO. 134

0.35
1.252

5440

10.758
5.248

254

5.279
1.1
2.97

5.291

1511.4

276
+0.20

259

-10 14

16.17

-1.10
17.27

11.07

4.18

15.25
-1.29

76.52
-1.29

16.52

+33

16.19

14.36

+0.91

1504.0

1933.8

1440.72

254

37.3

33.3

+0.0972.7 +0.2472.3

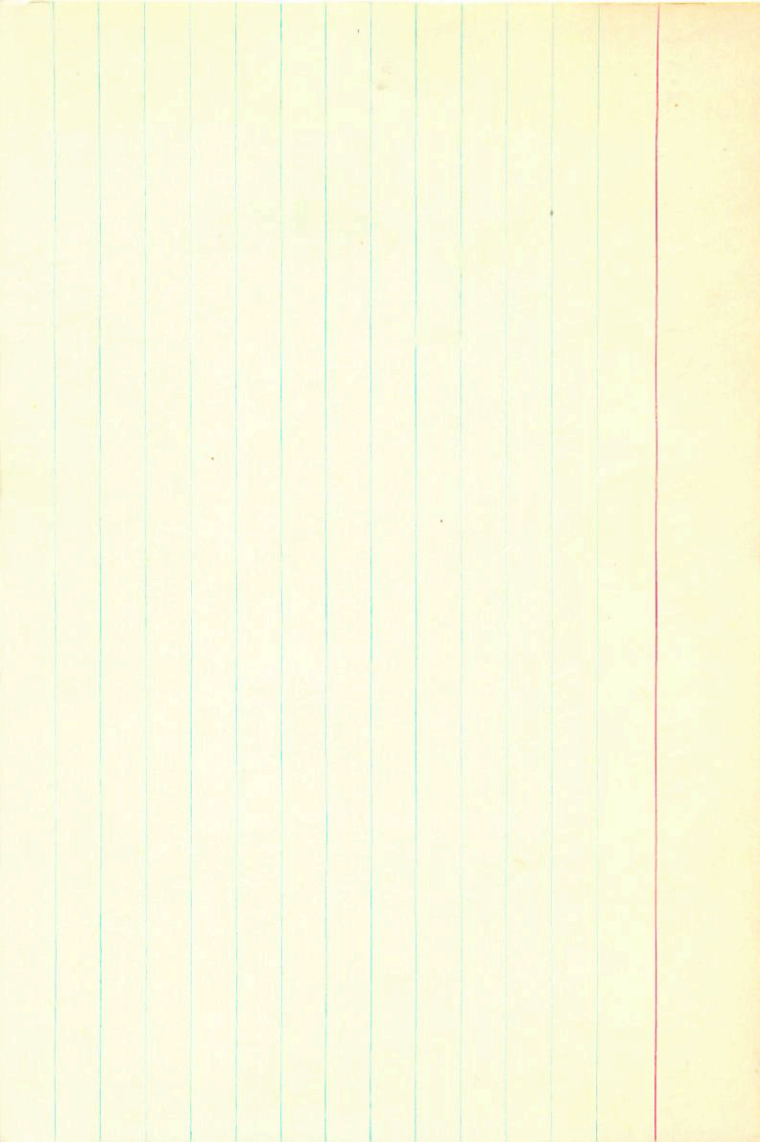
+0.005

+0.27

-10 14

0.3.1

dfy +32.158



+009² 0.15⁶ → BL

+120

6 03.7 -24 12

-0002
+0018±5.0
-03
-020±7.1

+0005 -015

41.894
-96
598
23.40 18937
+1.13
21.87

+007-05563
+1
+006 -015

198408 400m
-16
-34
0

39.953
27.815
41.762
41.770
20
790
-008
500m.
-294
-320
+60

15.70
5.82
21.52
1.12
22.64
+26
38

250
250
22.5
250
250

+7.4
-8.5
-4.1

S day

607737

-003 -0559
-0282 -0360
+0371 -0252

2366 250f
-0592 -148
-0642 -16.0
+0119 +3.0

-076 +786 +613
-488 +507 -710
+870 +354 -344

-0040 -0470 -0710
-0254 -0432 -0486
+0453 -0302 +0151

+009⁶ - 015⁻⁶ BL

+12C
400M.

292

364

-076	+786	H.13	+0032	-0559	-0596	-23.4	+7.3	-16.3
-488	+507	-710	+0208	-0360	-0568	-23.7	-8.5	-31.2
+870	+854	-344	+0375	-0252	+0123	+2.4	-4.1	-1.7

E = +05

m - M = 8.15

410M.

-18

-33

W24630

21

L.15

47 +176
43 228

2.07

APR 15

+9 -15

S Sep

6 03.7 24 11

7.1 - 8.9

907

way/630gr

2-14

8.15

410ms.

-18 -33 -1

+18
+16

+3
+009 -015

+12.0

+0.009 } LB
-0.015 }
984

Egg (adding gunk)

+012 -015

E3
+03

6.5 4.1
+170 +1.6 8.2

+114.1 1000

S Sep 7.05 +1.18 +1.30 -5.35 -18 -33 -1 +9 +120 E6
4.5 +1.75 8.15 -6 -4 +1 -15 -20

Step 200.5 - 20.4

41534 238.4 - 23.4 5.64 - 0.22 - 0.82 0.3 + 0.3 7.55

75



1880
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1880-1899

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 1900

~~05-18~~

225

44 1.8

4.02

23

1.7

7.9 - 5.2

-6.2

8.000*

6.000*

3.700*

-24.000*

-11.000*

0.012*

-0.015*

8.300*

7.9

38 0.42

457.0883449

12.000

-0.061

0.597

-14 -20.883 -14.0

-0.063

-0.723

Handwritten signature

-37.271 -30.2

0.025

-0.348

7.140 *MB*

1900
1901
1902
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2000

R.A. : 6.00
DEC. : 44.25
PM. R.A. : 132.00
PM. DEC. : -153.00
DISTANCE : 2.25
MODULUS : 28
RAD. VEL. : 32.10

q1 (U) : -0.06
q2 (U) : -0.26
q3 (U) : 0.96
dU : 160.45
U : 35.42

q1 (V) : -0.49
q2 (V) : 0.84
q3 (V) : 0.10
dV : -835.50
V : -17.2

q1 (W) : 0.8
q2 (W) : 0.4
q3 (W) : 0.
dW : 54.
W : 7.



41304 6 02.1 114 24 dFG 436.5 80(3)

G-7698

6.6

W8814

Y1400

F1401136

+22	-25	+0060	+36.5
-56	-93	-184	
-5	-6		

52.5
47.9
4

+106 -05 Rc

+24	-56	+1	.020
+19	-72	0	.015
+21	-64	0	.0175

3.40	+232	-54.0	-5.0
	-251	-438	-54

Σ
+0000 +36.5
-184

758 A(16)

+0073 54.5
+0057
-175 58.7
-189

~~249 569~~

7.161 1500.5 - +14 23 43.91 1898.0

$\frac{361}{6.900}$

$\frac{+9.10}{53.01}$

6.969

46.22 19338

$\frac{7.00}{33} 2$

$\frac{7408}{+209}$

$\frac{46.36}{14}$

6.987

$\frac{7.00}{29}$

44.87 1950.06

36.4

$\frac{4497}{+10}$

3.88

7.016

$\frac{433}{133}$

$\frac{36.9}{38.9}$

$\frac{45.66}{7.35}$

38.9

$\frac{45.66}{7.35}$