

43880

6 15.3 -34 43 N3 III +46.9 8C

F0877

3488

Cycle

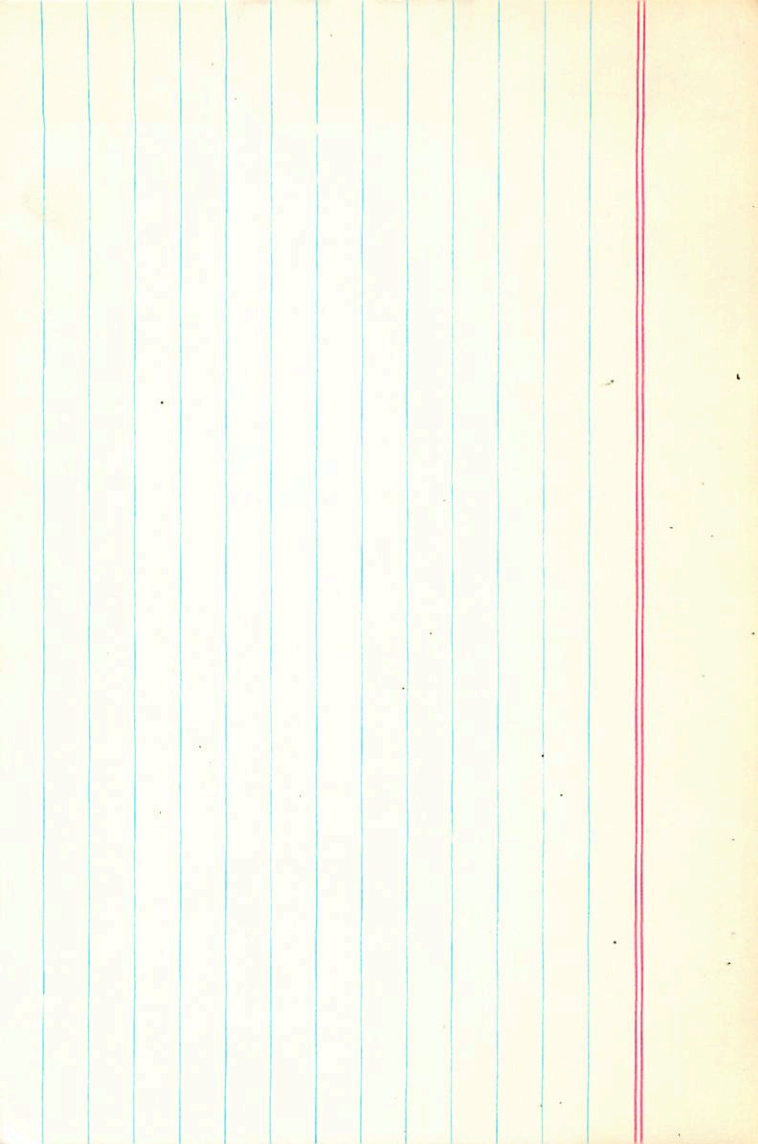
-0.21 +0.45

Yale

-0.006 -0.060

9.07 +1.26 (2.29)

X



43646

6

15.4

+29

48

+10.7

8075

+0002 ± 8007

-050 ± 7.5

25.827 2.7

10.22 2.0

37

+12

-00059

-0415 20

-00022

-0403

-00049

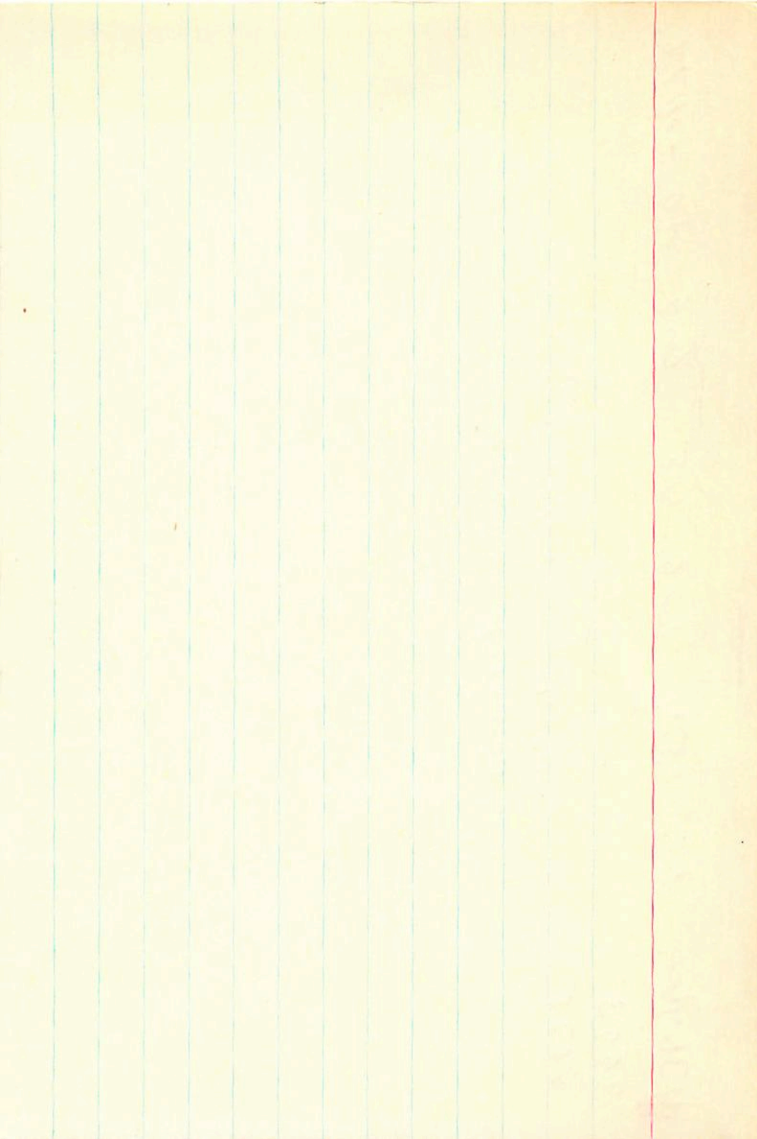
43646 6 15.4 +29 48 6.9 A0 +11.78

3993

8078

-0004<sup>8</sup> -059 N30

0000±9.7 -050±7.8



+650523  
 43297 6  
 8074  
 +0028±83  
 2  
 15.4  
 +65  
 31  
 8.6  
 d63 -16.38  
 342  
 -1247

3992 24695-  
 117  
 378  
 1908.1  
 +65  
 31  
 23.03  
 1910.5  
 11.22  
 34.25

24524  
 54  
 50  
 29.0  
 1929.9  
 6  
 28.94

+019 -259 GP

10 Mem

6 15.9

+0002 ± 2.8 -012 ± 2.2  
-0007 -016

+23 27 563 441.58

43740

6.5

1898.5 +003 -012 Q  
+002 -014 V

43740

3997

51.601 1902.9 +23 37 27.93 -010 -015 Z

8092

-009  
51.592

62  
2855 -010 -015

51.554  
24  
535

51.571  
26  
597

26.8

28.01  
24  
1928.04 28.25 1933.4

29.7  
31.2

20.122 572  
31.410  
51.531  
531  
535

27.84  
2  
27.86

60.84  
-31.32  
29.52  
-166  
27.86  
28.07

1927.61

28.06  
-149

?

1480

995-070 400 916-010-015 +Y1.5 -006 +17 -D66

D10 006 0010 047 053 +38.0 -3 +35

01

+2 +Y1 +11

$\boxed{+Y1 -9 -Y}$

008

+3 +Y2 +9

$\boxed{+Y1 -10 -5}$

005

+6 +Y5 +6

$\boxed{+Y2 -13 -10}$



-0007 ± 8.3 -0.15 ± 8.10  
 -0004 -0.25 ± 0.5

43947 6 16.8 +16 0.2 6.0 +42.5 - 8

4010

8117 47.398 1905.7 +16 2 8.28 1905.7  

$$\begin{array}{r} 030 \\ 429 \\ \hline \end{array}$$

47.404 6.7 1.7  

$$\begin{array}{r} 2.9 \\ 433 \\ \hline \end{array}$$

276

20.977 117  

$$\begin{array}{r} 26.408 \\ 47.385 \\ \hline 40 \\ \hline \end{array}$$

8.08 1933.4  

$$\begin{array}{r} 8.28 \\ \hline \end{array}$$

42.80 1930.40  

$$\begin{array}{r} -33.52 \\ \hline 9.28 \\ -1.57 \\ \hline 7.71 \\ +2.2 \\ \hline 7.92 \end{array}$$

830  

$$\begin{array}{r} 96 \\ \hline -0. \\ \hline \end{array}$$

1920.49  

$$\begin{array}{r} 4387 \\ 3352 \\ \hline 10.258 \\ 8.19 \\ \hline 8.93/8.51 \end{array}$$

47.370  

$$\begin{array}{r} 20.978 \\ 26.408 \\ \hline 47.386 \\ \hline 40 \\ \hline \end{array}$$

333  

$$\begin{array}{r} 276 \\ \hline \end{array}$$

43497 6 16.8 114 02 60 442.58

w4010 6.5

|          |     |             |
|----------|-----|-------------|
|          | 001 |             |
| -        | 014 | -016 27     |
| -        | 010 | -016 66+    |
| <u>-</u> | 012 | <u>-016</u> |
|          |     | -016        |

957-074 276 961 -012-016 +42.5 -004 +12-071

+012 004 001 000 055 024 +40.8 -3 +41

+3 +43 +5

01

+39-14-7

+1+43+7

015

4.15 397  
70

2269 4 17.2 +14 40 gmo +333  $\frac{1}{2}$

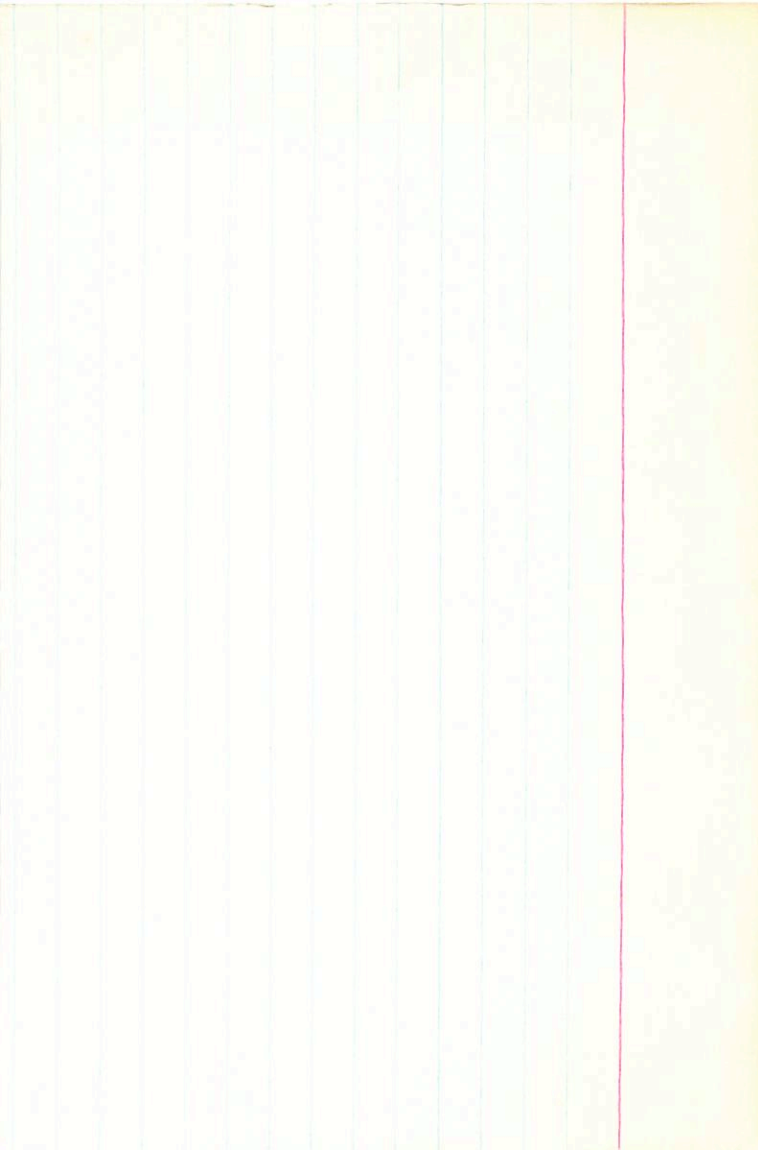
44033

5.66 +157 +1.55 (3)

4.70 +0.735 (3)

4.76 +0.74 (3)

6.2 ± 3.0  
0000 -018



-0009 = 5.1 + 004 = 3.9  
0000 + 002

44131 6 17.5 - 2 55 5.2 g m 1 + 42.0 g

4017

8137 29.299 1908.8 - 2 55 18.05 1909.4  
37  
336

14.205  
15.125  
29.330  
333  
340

41.71 1935.06  
- 35.48  
17.19  
18.28  
- 1.36  
18.55  
18.34  
- 1.21  
19.31

29.309  
17  
326

1941.55

19.21 1938.31

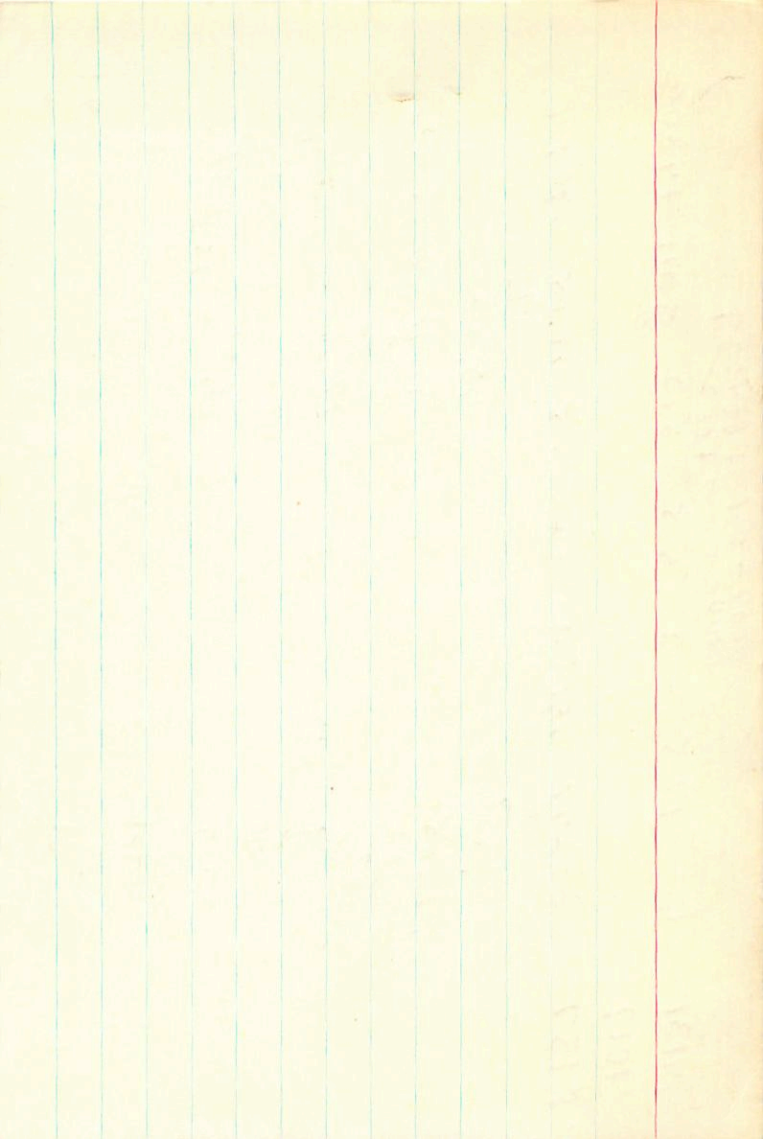
19.57  
+ 29.8  
18.2

38.4

59.289  
30.05  
29.239 / 6.34

3.32  
14.84  
18.16 / 6.34

29.0



+10.5  
-35 F5T4

43905 6 17.7 +53 29

HP2264 5.32 +45 +09 1549

6.5 dump  
sp 13 1.83  
1.83

GC8151  
45 Ann

1.284 .171 432 (15) SPC 2.689

③ ct  
Get  
±2.0

[m<sub>1</sub>] 222 0  
[C<sub>1</sub>] 575 174  
615 174

-30 24  
+00325 -0575  
+00245 -0549  
147  
472  
-25

3.40 +2.6-21.2 -3.0  
+170-440 -61

+0264  
-0.8

+024-094

+1.85  
345

X 1000-2000



8



2254.000\*

5.000\*

17.700\*

53.000\*

23.000\*

3.024\*

-3.094\*

3.450\*

43.978

-3.800

3.166

3.903

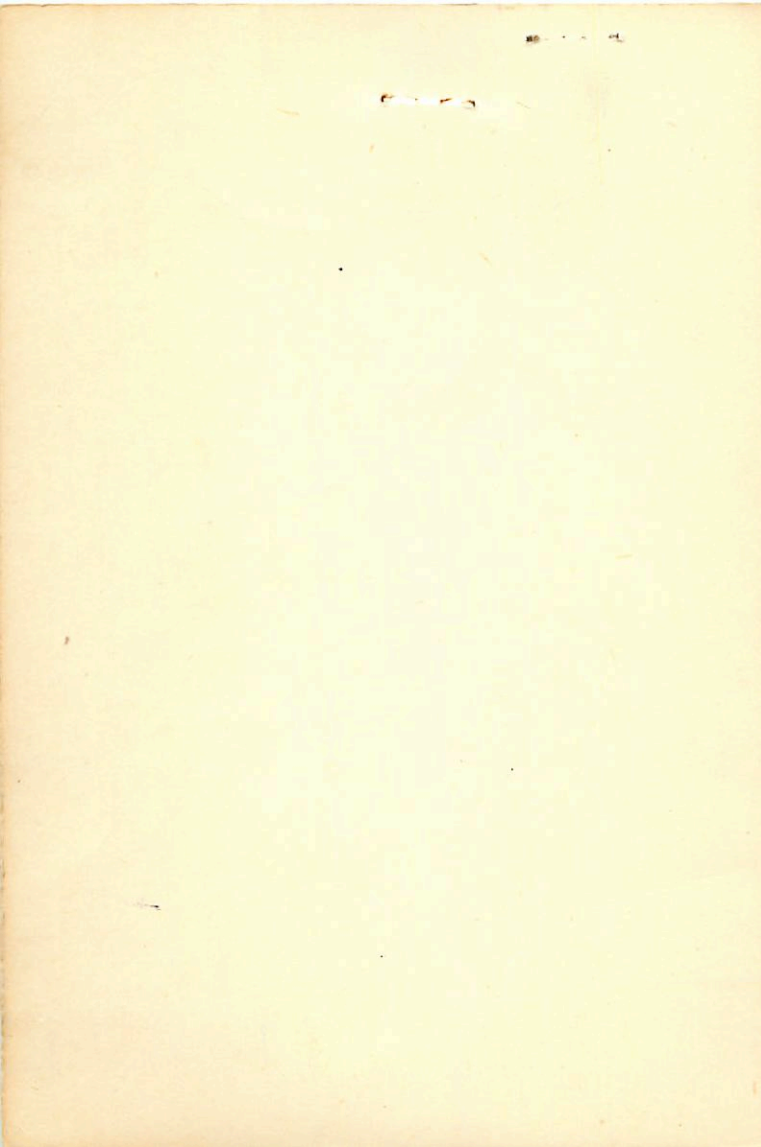
7.422

-3.424

3.309

-21.001

3.065









8-1-1

1-1-1

P



2285, 000\*

6, 000\*

19, 900\*

22, 000\*

32, 000\*

0, 052\*

-0, 113\*

4, 050\*

64, 565

54, 800

-0, 097

0, 983

47, 604

-0, 581

-0, 169

-46, 721

9

-0, 034

0, 073

1, 79

45 Am  
1+R 2264

Sy.D. P =

+0036 ± 2.5 -096 ± 1.8  
+0029 -099  
+0024 -095

6 17.7 +53 29 dFY -0.5 a

W 4021 43905  
4021  
8151

5.36 +0.43 +0.12

+032 -096 GC  
F500 +020 -095 F

43905 42.510 1799.9 +58 28 38.27 1898.6 +028 -095 (u/2)

4021

4.93  
+028 -095

8151

40.58  
1.842

39.5

43.20

76.7

1925.7

0265 -097

02619 -094

0234

021-094

39.15

-4.05

39.4  
40.8

1945.52

38.68 1947.61  
-22  
38.46

38.75

-27

38.48

42.422  
18

404

20

424

42.444

16

460

42.434

13  
447

443

113

443

113

42413

22

490

3200

24

86

68737

3200

24

86

6 0 804 545 +025 -095 -0.5 -076 -0.4 -270  
-025 076 00 -133 360 -0.3 0 -0.3

-13.3 +36.0 -27.4 0 10

017

W4035 6 18.8 +02 18 6.2 A5 -26 d

AD 44333

5V

-026 -021 4

-28.00

GC 181

024 021 -0011 ± 3.4 -026 ± 3.4

HR 49.476 1912.2

35.78 1909.4

042  
518

1.04  
36.84

49.435

35.52 1937.05

34

24

469  
-049

35.78  
1.06

-143 +453 +980  
-452 +761 -465  
+881 +464 -094

F0135 -0494  
+0428 -0829  
-0835 -0506

-0359 -3.6  
-0401 -40  
-13.41 -13.41  
33

0020 -023  
-0.020

76mm

-2.7 -22.8  
-3.0 +12.1  
-9.9 +2.4

ADS 4490

9.87  
10.75

→ 122" from

M3 III

U Mem

6

19.9

+22

32

5M3

+54.5a

HR 2296

44478  
4046  
8208

97  
2.09

+1.67

WB-13

106

+0042 -113 N30  
+0041 ± 0.7 -113 ± 0.6  
GL → N30

+056 -112 FR3

+060 -114 GC

+060 -113 N30

+059 -113

059

059 -110

+50 -33 +5

024

+43 -51 +2

016

~~44~~-354 454891 +059-113 +54.8 -051 +25 -453

-051 047 -023 020 -351 114 +48.8 -19 +45 16

-39 +52 -5

+41 -43 +23

26

-33 +49 +6

+40 -33 +24

-38 16.6 -4.2

-21.3 -23.7 -6.8

38.3 -96 -4.2

-44 +53 -9

+38.8 -51.8 -25.5

014

BVL46 ✓ 6 20 18 -54 32 10.2 A2

$\mu = -0.035 + 0.049$

✓

10.12 d  
9-10 0.795 A2

①

-5401026

9.66 + 0.37 + 0.11 2654767

6 20 00 -54 25.5 9.9 F2

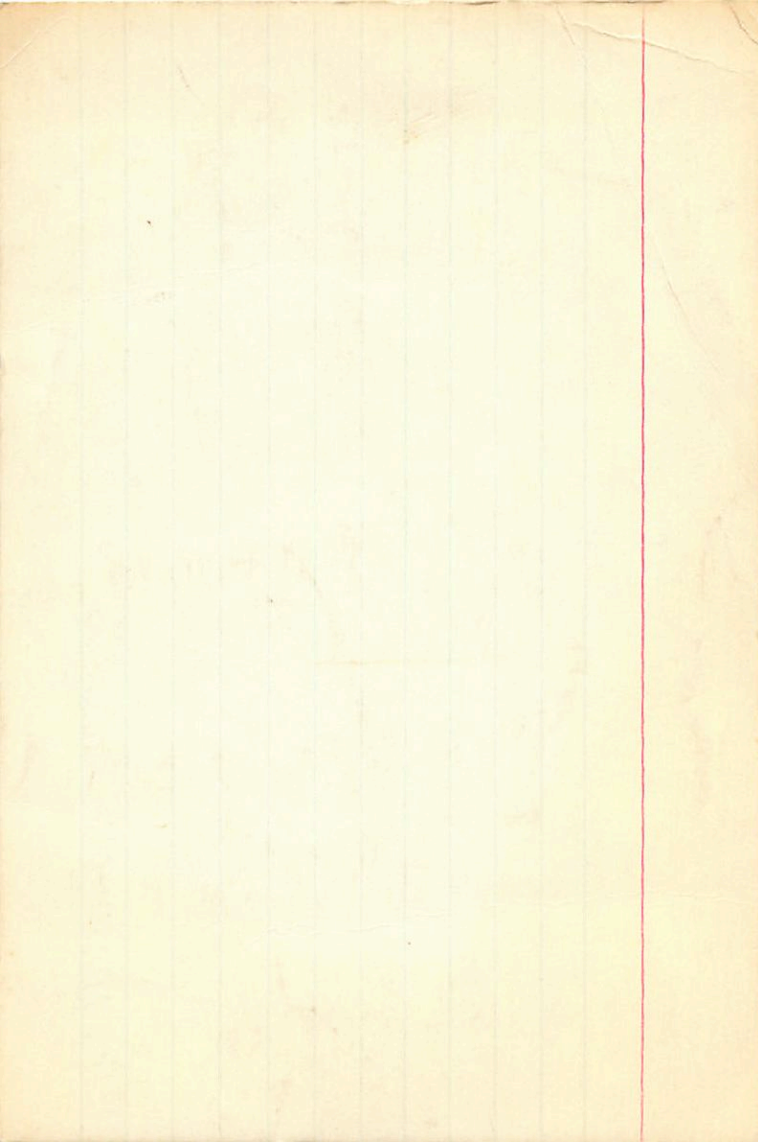
$\mu = -0.24 + 0.33$

✓

①

-5401021

9.79 + 0.40 - 0.10 2654767





$-0007 \pm 5.9$   
 $+0002$   
 $-034 \pm 5.5$   
 $-031$   
 $+33.5-8$   
 45018 6 21.9 -25 33 5.79 MS

4073

8267 53.952 1911.0 -25 32 57.30 1905.5  
 $\frac{027}{979}$   
 $\frac{+1.38}{55.92}$

$\frac{53.022}{1925}$   
 $\frac{53.945}{957}$   
 $\frac{11}{970}$

$\frac{983}{+004}$

(4.6)

$\frac{9.61}{45.40}$   
 $\frac{54.27}{1.10}$   
 $\frac{56.31}{+24}$   
 $\frac{58.07}{1938.82}$

$\frac{35.68}{26.11}$

$\frac{53.973}{980}$

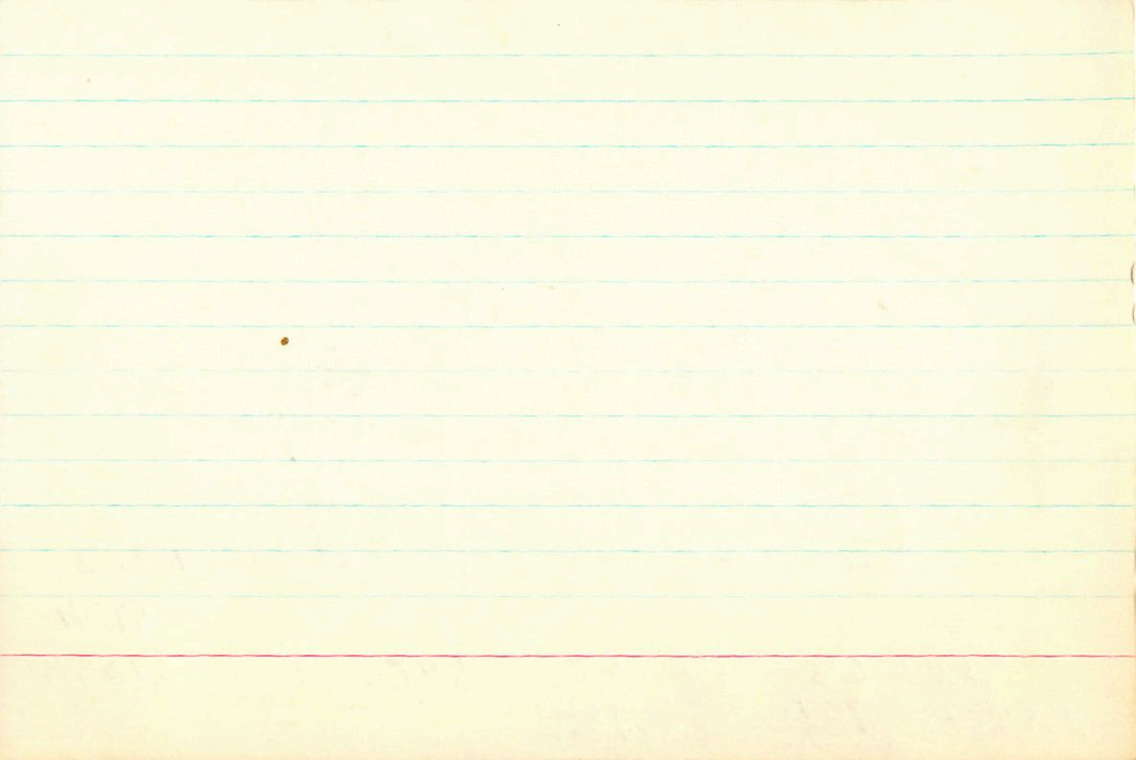
$\frac{57.28}{25}$

$\frac{1433.15}{57.03}$

$\frac{56.72}{-0.80}$

$\frac{53.983}{1.698}$

$\frac{57.30}{+24}$   
 $\frac{57.06}{}$



HR2320

6 22.0 -56 2/

Am +6.78

45229

5.60 +0.25

-040 -028 GC

4075

10

-037 -028 N30

-038 -025

8274

-0044 -028 N30

020

-0041 -026 ± 3.6 GC → N30

±4.1

~~020~~

195 -097  
~~832~~ ~~554~~ -832 554 -832 -024 +6.7 023 -6 -026  
038 -023 004 -002 190 -090 0 +3 0 20

+19 -1 -10  
-5 -9 -14  
5 4 13

70 55 22 10

$Z = -49$

↑ Mon 6 22.5 +7 07 +32.5

+0002 = 0.012

1090 ~~pts~~

|      |      |      |       |                 |       |       |     |       |
|------|------|------|-------|-----------------|-------|-------|-----|-------|
| -152 | +373 | +915 | -0021 | <del>0212</del> | -0233 | -25.4 | +4  | +29.7 |
| -446 | +800 | -400 | -0063 | <del>0455</del> | -0518 | -56.4 | -69 | -13.0 |
| +982 | +459 | -045 | +0124 | -0261           | -0137 | -14.9 | -16 | -1.5  |



5-30pm  
44708  
4087  
8287

A055036

10<sup>m</sup> 31''

8,5<sup>m</sup> 96''

107#

6 22.5 +58 27 5.5 9.5 -2.86

28

-0005 -002 N30

-0004 ± 2.4 -010 ± 1.7

M.28

+6.7 ①  
5.13

No

+13.06

BL Du

6 22.6

+14 45 8.5-9.2 1

HR2308

243  
 8420 5.59+2.30 - 465 +0.98  
 460 6.17+2.34 - 4.71 +0.96  
 470 6.28+2.33 - 4.83 +0.91

May

R = 460

R = +0.96

4.4 88  
 4.12  
 11.57  
 2.67  
 33.7  
 6.2

9

79

n=11 9.00

26

+5 -27 +1

243  
 9092 6.06+2.40 -  
 095 6.09+2.38 -  
 096 6.14+2.35 -  
 118 6.16+2.35 -  
 125 6.19+2.35 -

486 +1.09

481 +1.09

483 +1.07

484 +1.14

154  
 165 6.27+2.34 -  
 177 6.28+2.36 -  
 499

214

230 6.26 +2.36 -



+0005 -009 Lavin +13.06

$\frac{+0003}{+004} + 2$   
-007

+004

2.000

638m



-152 244 958  
-446 847 -286  
851 471 020

-0029 -0081  
-0084 -0281  
+0167 -0156

-0110  
-0365  
+0011

+5.4 +12.4  
-27.0 -3.7  
+1.0 +0.3

HP2313

6 227 20 55

45067

255 120 354 2605

-0.1257

305 360 145 400

(11)

(400)

355 145

555 360 150 419

Go 324 22.50

14 Jan  
 44974      4      22.7      +21      40      6.4      966      -23.66

4088

8296      42.665      1903.0      +21      40      28.27      1998.9

$$\begin{array}{r} 0.19 \\ \hline 684 \end{array}$$

$$\begin{array}{r} 42.665 \\ \hline 677 \end{array}$$

$$\begin{array}{r} 12.585 \\ 30.050 \\ \hline 42.635 \end{array}$$

$$\begin{array}{r} 639 \\ \hline 348 \end{array}$$

$$\begin{array}{r} 42.634 \\ \hline 673 \end{array}$$

$$\begin{array}{r} 72 \\ \hline 2909 \end{array}$$

$$\begin{array}{r} 28.24 \\ \hline 28.48 \end{array}$$

$$\begin{array}{r} 76.43 \\ \hline 46.30 \end{array}$$

$$\begin{array}{r} 30.13 \\ \hline 1.63 \end{array}$$

$$\begin{array}{r} 281.51 \\ \hline 28.71 \end{array}$$

$$\begin{array}{r} 28.24 \\ \hline 1939.02 \end{array}$$

$$\begin{array}{r} 2 \\ \hline 28.21 \end{array}$$

1935.1

1927.74

$$\begin{array}{r} 28.47 \\ \hline -0.62 \end{array}$$



+15,70  
5.55 4.5 / 2L

17R 2352 6 23.1 -69 57

6-6 8310

W 41094

6.659

$\frac{-170}{329}$

SAC

6.728  
-41

-152 974-160

-446 -211 850

852 061-468

+0037 ± 3.7  
+0046  
1904.1

+0041 +023

+0051 +022

+026 +022

-0186 +1016 830

-0550 -0220 -0770

+1087 -10064 +1150

+025 ± 3.4  
+022

24.42 1855.7

$\frac{-1.26}{25.68}$

24.69 1938.4  
-12

24.81 +13.1 -2.5  
87 -12.1

+12.4 -2.5 +10  
-11.5 -10.6 -2.5  
-7.2 -9.4 +10

45194

028327

13. P20

+037-1064

6 238

+13 08

-6 e SD

+1017 575 -103 57.5

+0009

-099

59.49

19023

+0013

-101

4.91

+0011 -100

04.46

04.46

49.927

1.10

15834

~~23~~

+20

950

1.30 - 3.10

49.550

962

+ 78

029

578

+

5.1

1540.1

3675

+016 -150

6.0

|      |     |      |       |       |       |      |
|------|-----|------|-------|-------|-------|------|
| -162 | 078 | 947  | -0120 | -1317 | -1437 | -57  |
| -441 | 938 | -321 | -0326 | -3972 | -4298 | +1.9 |
| 883  | 469 | 013  | +0652 | -2223 | -1571 | 0    |

H2 P2

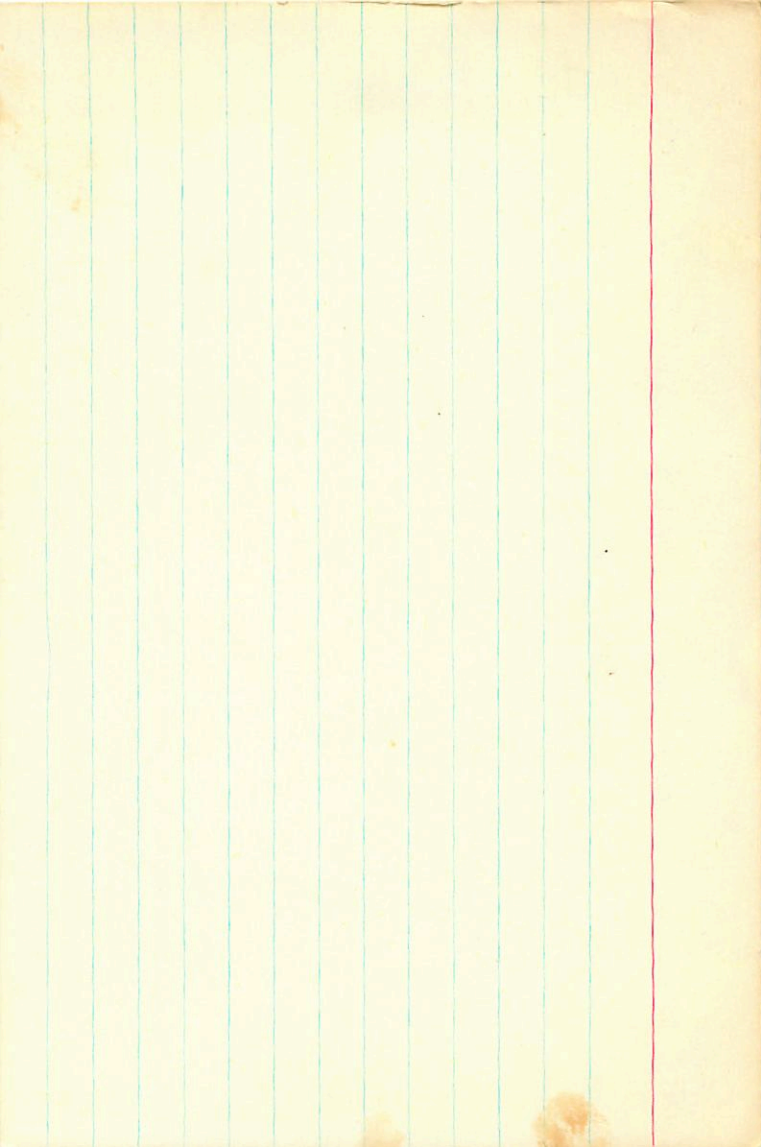
A G Am 6 23.8 +47 04

+1958 (16)

11.0 in mud.

+076 -051 Peep.

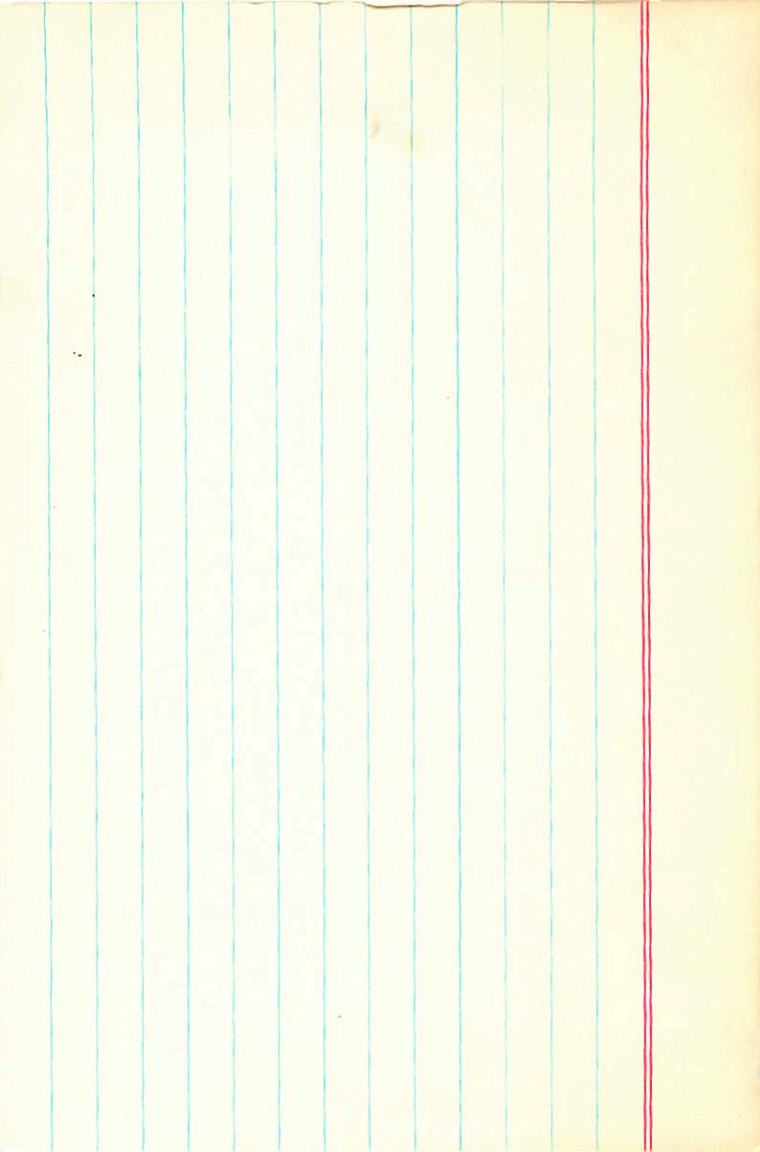




45320 . 6 24.1 -1 29 A7IIp +10 5-sta var

58.6 +08 +08

-0001 -030 N30  
-0002 -030 06 →  
-0001 -033



45192  
8342

+0002 ± 0.5  
+0007  
6 24.3 +32 36 6.4 NO +57.2-6

4105

19.341 1904.3 +32 35 43.40 19033

20.19

-009  
332 +00045 -062 2.90  
+00018 -060 46.30

41.26  
35088  
19.369  
359

23.5

36.0 1925.7

49.52  
46.48

559  
27.8  
21.2

4364 000  
9180 8900 -1.000

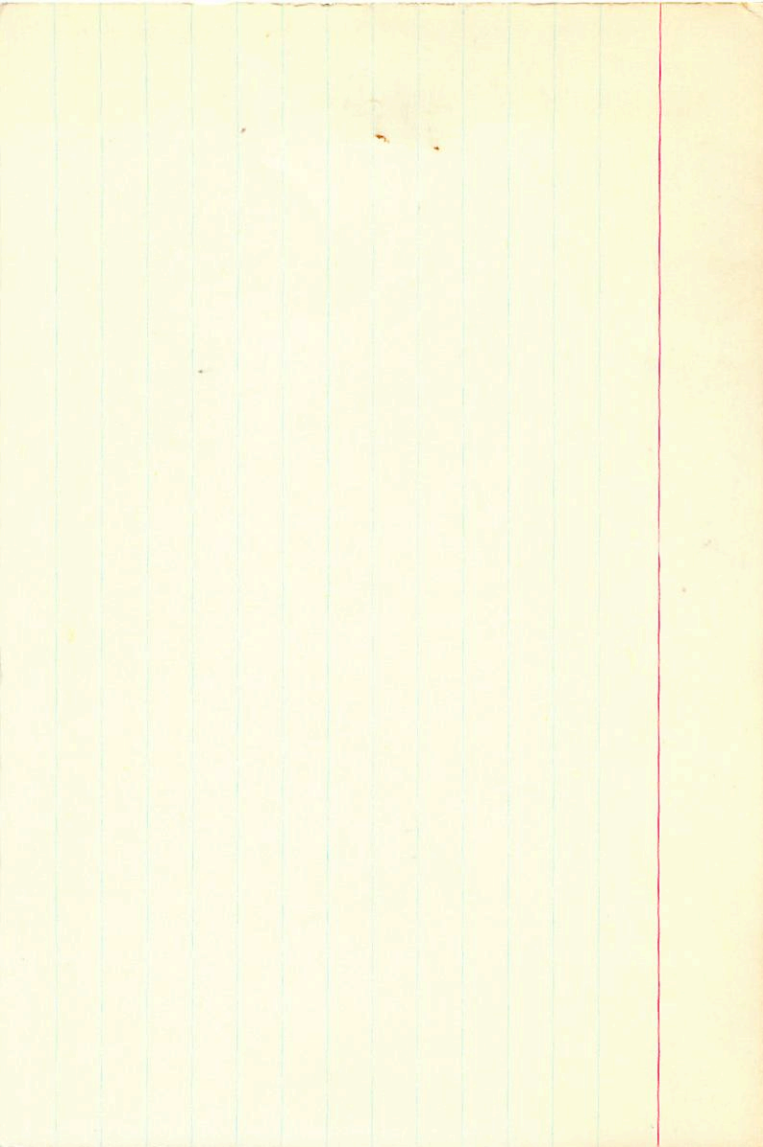
349 0023  
3017 000-060

44.75  
88  
44.78  
1.52

6143 19.30  
29  
529

44.7 1930.0  
44.71  
44.69

Key



SW Mon

6 24.4

+5

24

+39.2

7.4 1.47  
2.02  
5.12 10.47  
5.35

-0001 +005  
-0004 +0055  
-006

~~-0003 +004~~  
~~1~~  
~~-006~~

7.04

-162 399 903  
-441 789 -427  
883 467 -048

+0046 +0076 +0122  
+0125 +0150 +0275  
-0251 +0088 -0103

-004+006

10.47

+35.2  
-16.6  
-0.6

E=+18:

SW Mon 9.05 +1.86 +1.92 -3.85 +4.5 +5 -13 -6: +39.0 112.4  
- 7.25 +1.43 9.6 +1 +3 -2 +7: +47.0 -3.0

SW 205.5 -3.0

|        |            |      |     |     |       |     |      |
|--------|------------|------|-----|-----|-------|-----|------|
| 43526  | 202.7-4.4  | 6.56 | -14 | -50 | 88    | +03 | 7.15 |
| 44448  | 202.0 -3.6 | 883  | -08 | -59 | 82.58 | +12 | 9.65 |
| 44700  | 206.4 -4.5 | 6.70 | -16 | -62 | 838   | +03 | 7.40 |
| 44753  | 201.9 -2.0 | 6.25 | -08 | -30 | 40    | +04 | 6.08 |
| 256577 | 202.4 -2.2 | 9.48 | +13 | -75 | 828   |     |      |
| 45187  | 208.0 -4.6 | 6.50 | -03 | -06 | 89    | 00  | 5.6  |
| 46106  | 206.2 -2.1 | 7.92 | +14 | -74 | 818   | +40 | 9.70 |
| 289135 | 206.4 -2.1 | 6.57 | +18 | -70 |       |     |      |

9







0.000\*

15 Gen  
-0024 ± 1.9  
-045  
-021

48352 6 24.8 +20 49 6.4 q 12 -3

4115

8359 47.737 1892.5 +20 49 18.66 15

$\frac{138}{975}$

AD55080

$\frac{312}{21.78}$

from 28th deposit  
47.753  
26  
 $\frac{779}{2366}$

19.24 1934.7 100  
 $\frac{24}{19.48}$

47.744  
 $\frac{34}{778}$  - .086  
 $\frac{789}{886}$

19.60 1940.22

$\frac{41.8}{}$

47.780  
 $\frac{24}{809}$

$\frac{19.60}{19.62}$   
19.90 1928.04 96  
 $\frac{102}{34.3}$   
 $\frac{19.67}{-2.11}$   
 $\frac{46.8}{}$

11



2480

47220 32 75 49 6

25.0 26048

1825 0606 -716  
1114 2017  
6-17 18.00

2.1345

668642

500309-0601 Supp

6.6  
+277  
-41

(VU)

037304910

-0463  
-045-059

5590  
-7.4

3.532  
+18  
550

(46.13)

57.63  
-258  
57.3

6987 -5508 0601  
6705 -5350 0004  
7154

V<sub>1</sub>=60  
0073

-30  
-49  
517

-128  
02  
k.e

6.18 644 487 449

(40) (650) (35)

725  
2640

0740  
0057  
-0.85  
6279

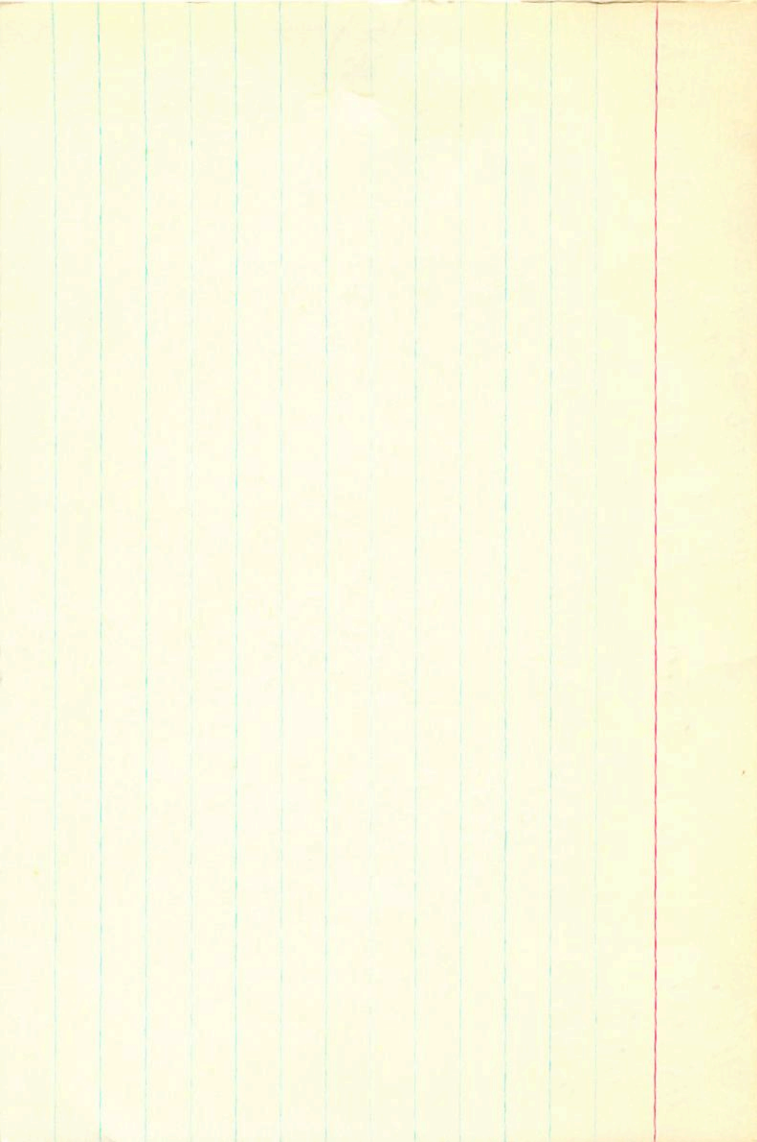
-085  
0014  
0017

1.212 914 190 MF

2.77

12







45427 6 25.4 +27 40 . -51322 D(5)

+270117 2.8 K111

+014 -037 Y

994 -110 465 885 +014-037 -513-017-24-156  
-014 017-001 002 -056 056 -45.4 +5-45  
-6-34-46 007

3

6.400  
27.700  
16.000  
-37.000  
7.500  
316  
-51.300

-0.158  
0.028  
0.987  
-15.493  
-55.536

-0.443  
0.891  
-0.896  
-186.075  
-53.916

0.883  
0.452  
0.128  
-20.079  
-12.933

13

6 25-4 -37 5R 6-18 ESD

2353

4580

668877

-0012 +038 5try

-0017 +0389

-0136

[010 +039]

0993

7148

- 0372

0393

0088

642

0059

6-16

61.2408

 $Z = +70 \mu$ 

RT Am

u 25.4

+80

32

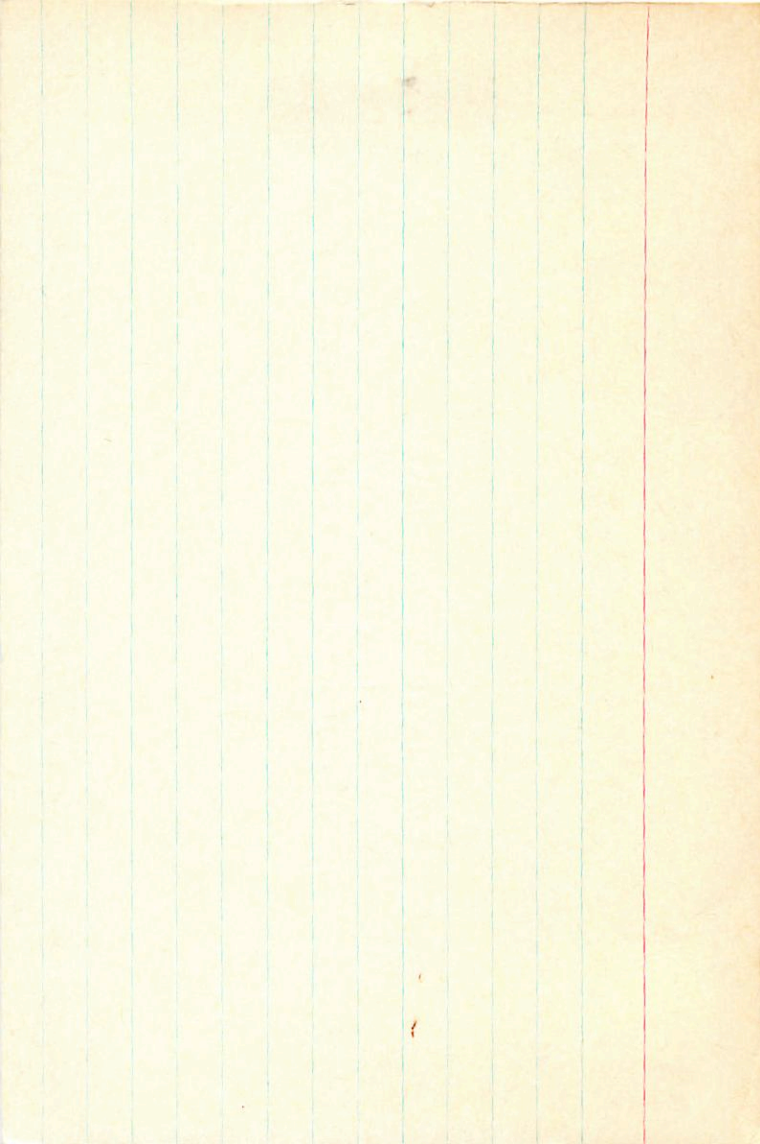
+210

+0003 -011

FR

450  $\mu$ 

|      |      |      |       |       |       |       |     |       |
|------|------|------|-------|-------|-------|-------|-----|-------|
| -163 | -020 | +986 | -0030 | +0010 | -0020 | -0.9  | +20 | +20.7 |
| -440 | +896 | -054 | -0081 | -0467 | -0548 | -24.7 | -26 | -1.1  |
| +883 | +443 | +155 | +0162 | -0231 | -0069 | -3.1  | 0   | +3.2  |



$$234 \checkmark \quad 06 \quad 28.5 \quad +10 \quad 20 \quad -20.3$$

$$45512 \quad +0019 \pm 6.0 \quad -0.40 - 0.40$$

$$580 \quad 32.437 \quad 8.0 + 0002 \quad 13.57 \quad 94.7$$

$$\begin{array}{r} -84 \\ 84 \\ \hline \end{array} \quad +0003 \quad \begin{array}{r} 2.19 \\ \hline 15.70 \end{array}$$

70.15

$$32.433 \quad 12.71$$

$$\begin{array}{r} 28 \\ \hline 461 \end{array}$$

+0015  
+001-040

$$32.440 \quad 62.0 \quad 12.48 \quad 6.4 \quad +10.33$$

$$\begin{array}{r} 88 \\ \hline 965 \end{array} \quad \begin{array}{r} 10 \\ \hline 12.48 \end{array}$$

1.228 1.005 0.290 MF

$$+2 \quad -40 \quad 5.45 \quad -20.3$$

127



HR2339 6 25.5 125 00 6.5 -6.88

YKRDY 345 104 393 2609

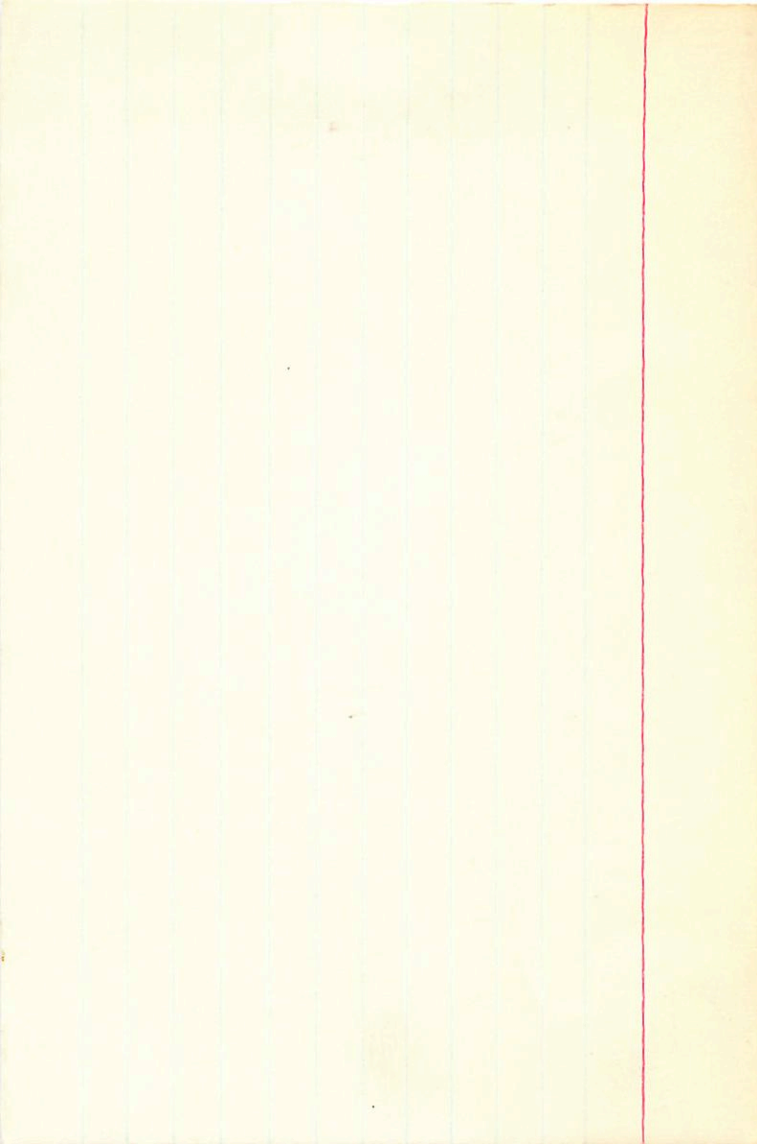
+121 -065  
+119 -067 →

-10.5  
-18.6  
-12.0

36.3pa.

|      |     |      |       |       |       |       |      |
|------|-----|------|-------|-------|-------|-------|------|
| -162 | 040 | 956  | -0914 | -0127 | -1041 | -3.8  | -6.7 |
| -441 | 891 | -109 | -2488 | -2830 | -5318 | 19.3  | +0.7 |
| 883  | 452 | 120  | +4981 | -1435 | +3546 | +12.9 | -0.9 |

100  
R0 260 43.84  
16



45541

6

26.2 + 29

31

A27 + 4371

8.0

-004 -027

~~45~~

949-1117 452 876 -004-027 +43.7 -013 +22 -109  
004 013 001 002 -009 066 +35 -6 +35

$$-5 + 48 + 11$$

01

$$+45 -14 +2$$

02.

$$-6 + 41 + 17$$

$$-5 + 51 \textcircled{B}$$

005

$$+45 -24 -4$$

0075

$$+45 -19 -1$$

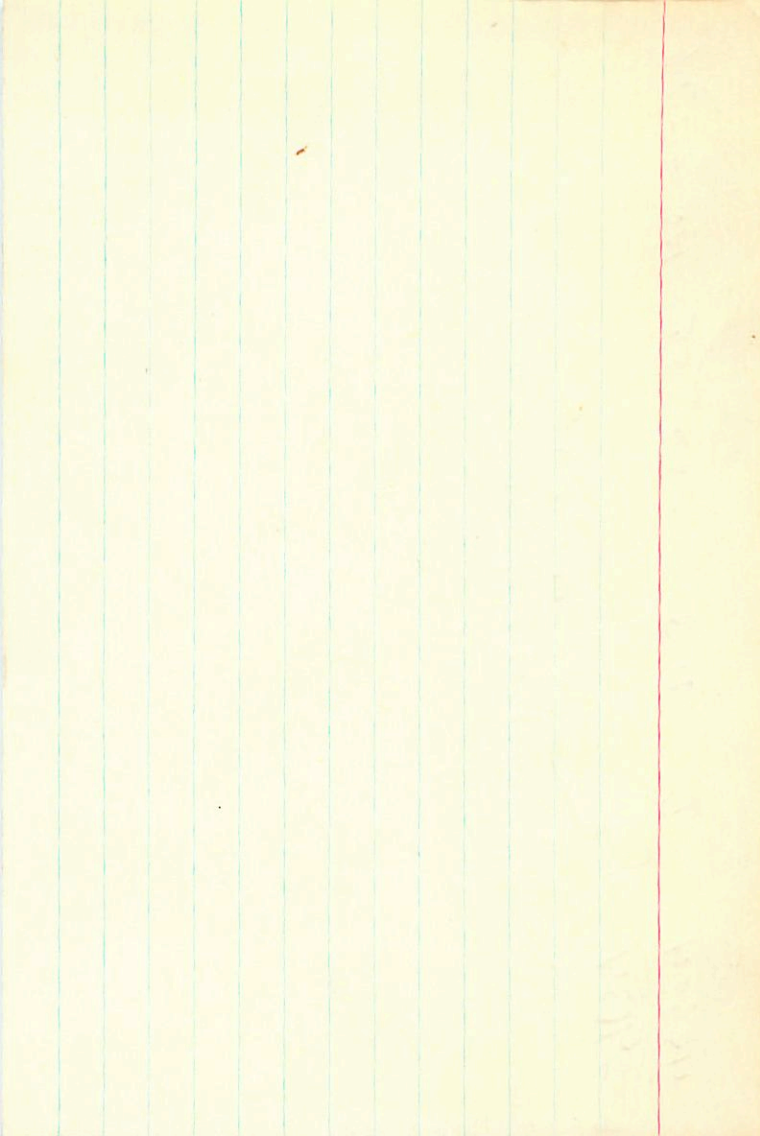
45984 6 26.3 -57 58 10 +12.78

4134

8408

-0005<sup>10</sup> -014 1130

-0019±3.9 -017±3.6 CC → N30



H246407

63  
378  
6

28.1 - 11 06

-11.3 km (near white Barnacles)

-009 000 GC →

0256  
007.68

006 474  
04266  
014743

6.28 + 1.10 (2.09) hake

1.54

3.7

|      |      |      |        |      |      |      |
|------|------|------|--------|------|------|------|
| -180 | +638 | +748 | +00.77 | +0.8 | 8.4  | -7.6 |
| -430 | +633 | -644 | +0183  | +1.8 | +7.2 | +9.0 |
| +885 | +438 | -160 | -0378  | -3.8 | +5.0 | +1.2 |

100

Caribby

-0009 + 003<sup>27</sup><sub>3</sub>

013 + 003

15



AD. VEL. : -11.300  
 MODULUS : 158  
 DISTANCE : 3.000  
 PM. DEC. : 3.000  
 PM. P.A. : -13.000  
 DEC. : -11.100  
 R.A. : 2.450

U : -2.400  
 UB : 19.324  
 P3 (U) : 0.750  
 P2 (U) : 0.840  
 P1 (U) : -0.100

U : 12.031  
 UB : 37.324  
 P3 (U) : -0.430  
 P2 (U) : 0.330  
 P1 (U) : -0.430

U : 10.214  
 UB : -47.240  
 P3 (M) : -0.172  
 P2 (M) : 0.430  
 P1 (M) : 0.384

10

R.A. : 6.450  
 DEC. : -11.100  
 PM. R.A. : -13.000  
 PM. DEC. : 3.000  
 DISTANCE : 6.000  
 MODULUS : 158  
 AD. VEL. : -11.300

q1 (U) : -0.169  
 q2 (U) : 0.640  
 q3 (U) : 0.750  
 dU : 19.324  
 U : -5.409

q1 (V) : -0.436  
 q2 (V) : 0.633  
 q3 (V) : -0.639  
 dV : 35.394  
 V : 12.831

q1 (W) : 0.884  
 q2 (W) : 0.435  
 q3 (W) : -0.172  
 dW : -47.248  
 W : -5.544

15

46114      6   27.5   -17   53      264 +1.38w(3)

628456

BFY

w4161      7.70 +0.80 +0.42      Egg (2) 18"      043

Y1516       $\delta = .01$

-17° 515      7.72 +0.82 +1.84      2 Bay  
<sub>u-Bc</sub>

10<sup>249</sup>

224

7.76 <sup>301</sup> 094 765 245      (1)      -167      -217      cc

-35 -25      -56 .02

242

-175 ± 4      -207 ± 10      y

-36 -28      -77 .015

+5.13  
37

~~-171~~      ~~-212~~

7209

<sup>S</sup>  
-0109 -209

+13

-3 ± 12 c(7)

-0117515.0  
-0105  
-2175113  
-203

27.205 15044 -17 53 0.63 1500.6

26.23  
534  
8

1.344

26.453  
849  
+1  
27.1

890

27.894  
215  
191

1785  
892  
346

330

49.91  
10.72

3379  
1541.8

2445  
824  
-14

11

58.32  
56.35  
-10  
5645

1922.07

1497  
57.38  
7.47

36.6

71.75  
37.4

SB (50)

14A2384      6 28.6      -50      12      2

45.7m      " -0.057 -0.001 → Sings  
~~-0.058~~      -0.058      +2

4  
.7  
"

|      |     |      |       |       |       |       |      |     |
|------|-----|------|-------|-------|-------|-------|------|-----|
| -180 | 967 | 150  | +0469 | -2658 | -2189 | -10.0 | -1.4 | -1A |
| -480 | 057 | -900 | +1121 | -0239 | +0882 | +4.0  | -2   | +2  |
| 885  | 240 | -400 | -2307 | -0660 | -2967 | -13.5 |      | -15 |



-0057 -061 stay

6 28.8 -50 12

-055

72 50

613 810 3.07

$\sigma = 504 \mu m$  Egg -

AG 5.38 +0.355 +0.005 ⑤

913 568 (245)

CO 8.38 +0.765 +0.35 ⑤

913

+5.88 340  $\mu m$  0.21

$\times 10^6$

$a^2/b^2$

6 a L

I 96.96 1901.48 0.25 +230 -424 +406 +195 0.500 27.3 13.22

II 102.24 1902.52 0.27 +223 -395 +380 +262 +0.480 16.1 10.60

III 91.28 1895.68 0.27 +150 -455 +454 +048 0.516 36.6 16.49

207 (87)

n v w

$\mu_1 + \mu_2 = 16.2$   
 $\mu_1 = \mu_2 = 0.81$   
1.30 0.65

$\sigma^2 =$   
2.07 1.00

(-11 +2 -15)

|         |       |      |   |      |      |       |      |       |       |       |
|---------|-------|------|---|------|------|-------|------|-------|-------|-------|
| 189440  | 255   | 0.30 | 1 | QL   | +2.5 | -0.06 | +0.3 | -0.07 | +5.9  | -0.02 |
| 1903.22 | 258   | 0.40 | 2 | I    | -6.7 | +0.03 | -8.5 | +0.05 | -12.1 | +0.02 |
| 1922.19 | 39    | 0.46 | 3 | Dans | -1.4 | +0.62 | -4.8 | +0.01 | 0.0   | +0.02 |
| 1923.00 | 43    | 0.46 | 3 | Dans | -0.6 | +0.01 | -3.8 | 0.00  | +0.8  | +0.01 |
| 1926.22 | 53    | 0.48 | 2 | B    | -2.7 | 0.00  | -4.4 | 0.00  | -1.7  | +0.01 |
| 1929.30 | 60    | 0.53 | 7 | V    | 0.0  | +0.03 | -1.5 | +0.03 | +0.5  | +0.04 |
| 1933.03 | 76.5  | 0.54 | 8 | B    | -0.7 | 0.00  | -1.4 | +0.01 | -0.8  | +0.02 |
| 1936.09 | 87.5  | 0.56 | 8 | B    | +2.1 | 0.00  | +1.8 | +0.01 | +1.5  | +0.01 |
| 1938.14 | 91.0  | 0.54 | 4 | B    | +0.3 | -0.03 | 0.0  | -0.02 | -0.6  | -0.02 |
| 1942.88 | 102.0 | 0.56 | 4 | B    | +0.4 | -0.04 | +0.5 | -0.03 | -0.8  | -0.04 |
| 1949.06 | 115.0 | 0.62 | 4 | B    | 0.0  | 0.00  | +0.4 | +0.02 | -1.3  | 0.00  |
| 1960.11 | 136.0 | 0.61 | 3 | B    | +0.2 | 0.00  | +1.0 | +0.01 | -1.1  | 0.00  |
| 1964.96 | 146.0 | 0.57 | 4 | B    | -2.4 | -0.01 | -1.1 | -0.02 | -4.0  | 0.00  |



19 Mem

46031

4168

4462

$$\begin{array}{r} -0008 \pm 2.5 \\ -0003 \\ \hline \end{array}$$

$$\begin{array}{r} 28.7 \\ +15 \\ \hline 56.4 \end{array} \quad \begin{array}{r} 6.4 \\ +20.96 \\ \hline \end{array}$$

$$\begin{array}{r} 44.830 \\ +15 \\ \hline 54 \end{array} \quad \begin{array}{r} 24.60 \\ +20.96 \\ \hline 45.56 \\ \hline 895.2 \end{array}$$

$$\begin{array}{r} 0.10 \\ \hline 870 \end{array}$$

$$\begin{array}{r} 10 \\ \hline 25.70 \end{array}$$

44.826

$$\begin{array}{r} 29 \\ \hline 855 \end{array}$$

2478 19344

$$\begin{array}{r} 20 \\ \hline 24.98 \end{array}$$

$$\begin{array}{r} 44.828 \\ 24 \\ \hline 859 \\ \hline 852 \\ -011 \\ \hline \end{array}$$

$$\begin{array}{r} 24.96 \\ +6 \\ \hline 25.02 \end{array}$$

$$\begin{array}{r} 1938.60 \\ \hline 34.3 \end{array}$$

$$\begin{array}{r} 11279 \\ \hline 34.3 \end{array}$$

$$\begin{array}{r} 39.1 \end{array}$$

$$\begin{array}{r} 1940.07 \end{array}$$

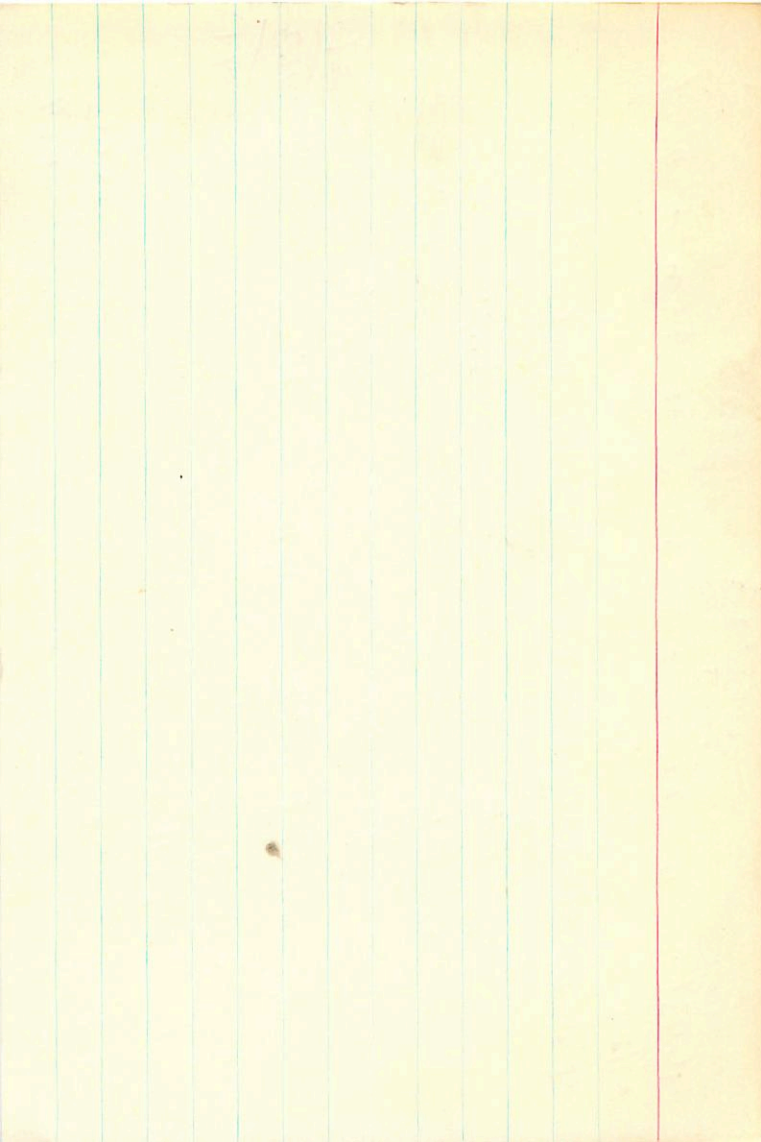
44.841

$$\begin{array}{r} 30 \\ \hline 871 \end{array}$$

24.84

$$\begin{array}{r} 16 \\ \hline 25.02 \end{array}$$

$$\begin{array}{r} 25.01 \\ \hline -0.09 \end{array}$$



30 35.  
-0017 62.5 -021 42.4  
-0017 -025

WW Ann 6 29.2 + 32 30 - 9.4 a

(+R 2372 46057 24 19.2 0017 -023  
9424  
4178

-022 -021 6c  
-024 -024 6a(2)  
-025 -023  
1901.8

11.469 1504.1 + 32 29 32.67  
1.01 1901.8  
33.68

33.546  
37958  
174911  
487  
494  
494  
-0.06  
449  
28.0

817 4.5  
260 426  
32.1  
30.3

35.1 1524.7  
-10  
35.0  
1.77  
33.16  
33.41  
33.54 1939.56

501  
32.92  
- .76

11.459  
43  
50

32.54  
-11  
43  
32.

942-126 537 843-623-023-9.4-012-5.0-090

01

410.8-0.8-14.0

6.5-4.8-15.8

46122

6

6 20 +6 51  
29.1 +6 49

-8

+61276

-032 -042 AC123

~~-053 -028~~

-056 -031Y

-058 -030

-4P

-36

-045 -036

43

-8.0

Amey  
A

-13.4

-7.6

16

|         |       |
|---------|-------|
| 01 (U)  | 0.18  |
| 02 (U)  | 0.33  |
| 03 (U)  | 0.50  |
| 04 (U)  | 0.67  |
| 05 (U)  | 0.83  |
| 06 (U)  | 1.00  |
| 07 (U)  | 1.17  |
| 08 (U)  | 1.33  |
| 09 (U)  | 1.50  |
| 10 (U)  | 1.67  |
| 11 (U)  | 1.83  |
| 12 (U)  | 2.00  |
| 13 (U)  | 2.17  |
| 14 (U)  | 2.33  |
| 15 (U)  | 2.50  |
| 16 (U)  | 2.67  |
| 17 (U)  | 2.83  |
| 18 (U)  | 3.00  |
| 19 (U)  | 3.17  |
| 20 (U)  | 3.33  |
| 21 (U)  | 3.50  |
| 22 (U)  | 3.67  |
| 23 (U)  | 3.83  |
| 24 (U)  | 4.00  |
| 25 (U)  | 4.17  |
| 26 (U)  | 4.33  |
| 27 (U)  | 4.50  |
| 28 (U)  | 4.67  |
| 29 (U)  | 4.83  |
| 30 (U)  | 5.00  |
| 31 (U)  | 5.17  |
| 32 (U)  | 5.33  |
| 33 (U)  | 5.50  |
| 34 (U)  | 5.67  |
| 35 (U)  | 5.83  |
| 36 (U)  | 6.00  |
| 37 (U)  | 6.17  |
| 38 (U)  | 6.33  |
| 39 (U)  | 6.50  |
| 40 (U)  | 6.67  |
| 41 (U)  | 6.83  |
| 42 (U)  | 7.00  |
| 43 (U)  | 7.17  |
| 44 (U)  | 7.33  |
| 45 (U)  | 7.50  |
| 46 (U)  | 7.67  |
| 47 (U)  | 7.83  |
| 48 (U)  | 8.00  |
| 49 (U)  | 8.17  |
| 50 (U)  | 8.33  |
| 51 (U)  | 8.50  |
| 52 (U)  | 8.67  |
| 53 (U)  | 8.83  |
| 54 (U)  | 9.00  |
| 55 (U)  | 9.17  |
| 56 (U)  | 9.33  |
| 57 (U)  | 9.50  |
| 58 (U)  | 9.67  |
| 59 (U)  | 9.83  |
| 60 (U)  | 10.00 |
| 61 (U)  | 10.17 |
| 62 (U)  | 10.33 |
| 63 (U)  | 10.50 |
| 64 (U)  | 10.67 |
| 65 (U)  | 10.83 |
| 66 (U)  | 11.00 |
| 67 (U)  | 11.17 |
| 68 (U)  | 11.33 |
| 69 (U)  | 11.50 |
| 70 (U)  | 11.67 |
| 71 (U)  | 11.83 |
| 72 (U)  | 12.00 |
| 73 (U)  | 12.17 |
| 74 (U)  | 12.33 |
| 75 (U)  | 12.50 |
| 76 (U)  | 12.67 |
| 77 (U)  | 12.83 |
| 78 (U)  | 13.00 |
| 79 (U)  | 13.17 |
| 80 (U)  | 13.33 |
| 81 (U)  | 13.50 |
| 82 (U)  | 13.67 |
| 83 (U)  | 13.83 |
| 84 (U)  | 14.00 |
| 85 (U)  | 14.17 |
| 86 (U)  | 14.33 |
| 87 (U)  | 14.50 |
| 88 (U)  | 14.67 |
| 89 (U)  | 14.83 |
| 90 (U)  | 15.00 |
| 91 (U)  | 15.17 |
| 92 (U)  | 15.33 |
| 93 (U)  | 15.50 |
| 94 (U)  | 15.67 |
| 95 (U)  | 15.83 |
| 96 (U)  | 16.00 |
| 97 (U)  | 16.17 |
| 98 (U)  | 16.33 |
| 99 (U)  | 16.50 |
| 100 (U) | 16.67 |

|             |         |
|-------------|---------|
| R.A. :      | 6.500   |
| DEC. :      | 6.800   |
| PM. R.A. :  | -45.000 |
| PM. DEC. :  | -36.000 |
| DISTANCE :  | 4.300   |
| MODULUS :   | 72      |
| RAD. VEL. : | -8.00   |

|          |       |
|----------|-------|
| q1 (U) : | -0.18 |
| q2 (U) : | 0.37  |
|          | 0.90  |



AD55166

+0027 ± 2.0 +029 ± 1.8

-0.3  
+77

+0027

+023

46136

6

29.4

+17

49

7.2 dFC +0.41

4185

357 165 443 2626  
271 160 559 2677

20" ( 8.1 dFC (+2c)

8482

23.447

1906.0

+17

49 +17.00

1901.3

20

119  
1328

23382

29  
477

+0027 +0255

136  
15.64

1214 +02255 +0271

16.34  
20

1935.1

+0364

405

+037 +026

16.54  
18.50  
-92

1927.65

10.185  
34.0

32.7

55.946  
27.490  
27.336  
-4  
332  
39  
371

47.717  
3893  
22.710

+077

28.0

24.89  
-25.12

17.58  
+58  
16.00  
21

114

16.38  
+0.74

23.403

29  
432

39

26

16.31 1939.10

+17  
16.39

B

GC8481

+003273.6  
+0031

+03153.4  
+022

22.749

1899.2

+17 48

59.87

1895.6

$$\begin{array}{r} 162 \\ \hline .587 \end{array}$$

$$\begin{array}{r} 1.64 \\ \hline 59.18 \end{array}$$

55.144

22.440

22.634

230  
329  
669

359

$$\begin{array}{r} 1.18 \\ -92 \\ \hline 60.26 \\ -1.58 \\ \hline 58.68 \\ 21 \\ \hline 58.89 \end{array}$$

1928.80

35.1

$$\begin{array}{r} 59.06 \\ \hline +0.88 \end{array}$$

35.5

22.667

296

.696

47.719  
34.443  
22.710  
409

1938.14

58.94

1939.10

$$\begin{array}{r} 64.34 \\ 25.12 \\ \hline 59.22 \\ 59.09 \\ \hline 59.03 \\ 20 \\ \hline 59.23 \end{array}$$

4

22.696

29

.525

59.0

59.23

1939.00

6.500

17.000

45.000

26.000

4.000

63

0.400

- 0.100

0.199

0.963

- 12.155

- 0.382

- 0.430

0.065

- 0.259

19.340

1.117

0.005

0.461

0.071

236.456

14.940

17