

2 Nov

41543 6 03.8 +23 39 6.9 9M4 -15.36

3835

6.72 10.57 R3 IV 2

7739

30
0000 -004

123.1142

-0001 ± 2.3 -005 ± 2.0

-13.2 ①

-17.5 ①

-17.6 ①

19 Sep

HR2155

6 03.9 -14 56

+32.06

4.65 +0.06

AV

-014 +015 GC

-023 +010 N

-018 +014

-0016	+010
-0011	+017
-0014	+019
-0202	

37 pp.

-086	+653	+716 ²⁺	+0083	+0460	+0543	+2.0	+22.9
-483	+600	-658	+0465	+0398	+0863	+3.2	-20.4
+872	+401	-283	-0839	+0266	-0573	-2.1	-9.1

+24.9

-17.2

-11.2

1 0 -257 966 -018 10.4 +32. -004 5 066

018 004

-0010 ± 2.0 +018 ± 1.2

532491 3.3 -0010 45.46 3.1

0.47
3.3
46.30

53459 46.26 35.76

+5
46.3
45.54

5585

4575 (2005)

+24
46.3
45.75

4 25.2

2155 6 3.9 -14 56 AIE

41695

7722

467 +04 04 6

31

0231571076(3)

2884(3)65

(16) +53, +61, +22, +1, +2, +3, +4, +5, +6, +7, +8

314

222 1590

141

177

D107, 1 +15, +24, +13

322

a = 0.37 ✓

-0016

1 = 0.56 ✓

~~0016~~ +0.1000

1.071

1.393

-023

+0.85

9224

2870

9714

-2323

+32

3.98



1



2155.000*

6.000*

3.900*

-14.000*

-56.000*

-0.023*

0.010*

3.850*

58.884

32.000

0.042

0.717

25.415

0.081

-0.635

15.530

ADS4704

41841

6

04.4 -23 06

5.5

A2 -14.66

3846

7763

26.891

1905.4

-23 6

13.37

19008

10^{mm} 44'

$\frac{067}{958}$

24.336

2.520

26.904

$\frac{912}{912}$.931

26.904

$\frac{912}{912}$

909

- 049

26.400

$\frac{1}{915}$

13.70

13.50

12.35

-1.14

$\frac{1349}{1349}$

+19

15.30

57.445

-1.144

$\frac{58589}{58589}$

13.79

+39

13.40

44.90

-2.45

$\frac{4245}{4245}$

1434.87

1940.92

7579

37.9

37.1

~~23.17~~

14/10/2078

6 05.1 -42 17

-0034 0 +003 6L

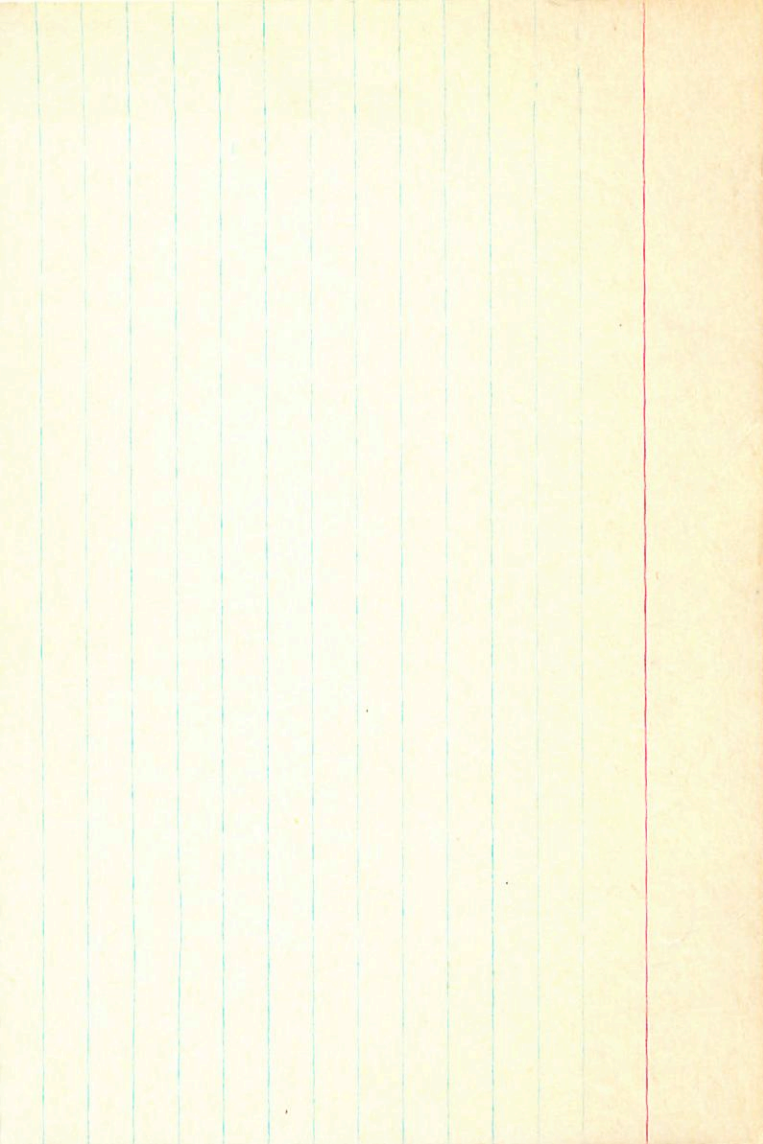
-0041 -013 M30

-086	942	324	0166	+0313	+0474
-483	245	-841	0932	+0081	+1013
872	224	-434	-1682	+0076	-1006

-0.7

+1.7

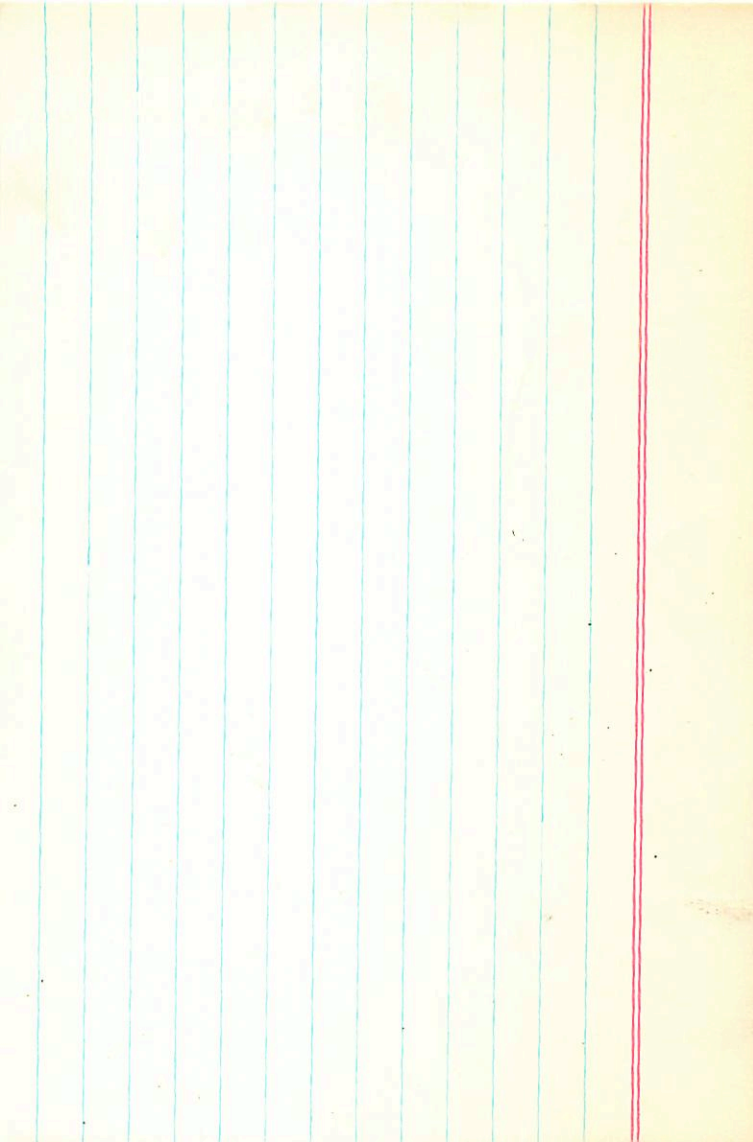
+0.9



42078 6 05.1 -42 17 Am +4.9 C4
I-D 1146 -2 Sta Ven
+1.5

6.17 +0.25 (1.59)

-0041 -013 N30
-0035 +003 GC
-0035 -005



17042443 6 05.6 -22 45

Ret 342

$$\begin{array}{r} +18 \\ 120 \\ -1 \\ +5 \\ \hline +2 \end{array}$$

b-y m1 r1 β

$$0.296 + 0.154 + 0.478 = 0.928$$

533
50
510
510
280

$$P^2 = 3.31 \times 10^2$$

$$Q^3 = 8.33 \times 10^{-3}$$

$$Q^3/P^2 = 2.55 \times 10^{-4}$$

$$P = 18.2 \quad \frac{P^2}{Q^3} = \frac{41 \times 10^4}{2.55 \times 10^{-4}}$$

$$0.275 \rightarrow \frac{2.08 \times 10^{-6}}{0.001 + 0.002} = 1.22$$

$\Delta[C_1]$

$$\frac{0.53}{0.20} = 2.65$$

479

$$\frac{5110}{1009} \times 479 = 2345$$

$$\Delta[M_1] = 2345$$

$$M_1 = 2345 = 9(M_1 - 0.20)$$

$$5.70 + 1.13 = 6.83$$

$$[M-B] = [C_1] + 2[M_1]$$

$$5.70 + 0.43 = 6.13$$

G102-49

6 057

11 28

T26-5

T111037

9800.850.58

000 - 294

7675 3017
7518 815A
7518 815A

7.95 1st - -

37412 5. 36.0 - 31.22 - 19.2 1st.

Serial 20091 (1.91) days

-051-332 CP

376mm
41597

3858

7796

0.948
3442
453

0.16
192

0.948
3442
453
+0023 25
+0030 ± 2.2
+022 ± 1.9 OC →
+0026 +0.8
+020

6 05.6 +58 57 5.4 g. G. 8 +31.1a

-086 -458 863

-483 779 401

872 382 307

-0082 -0422

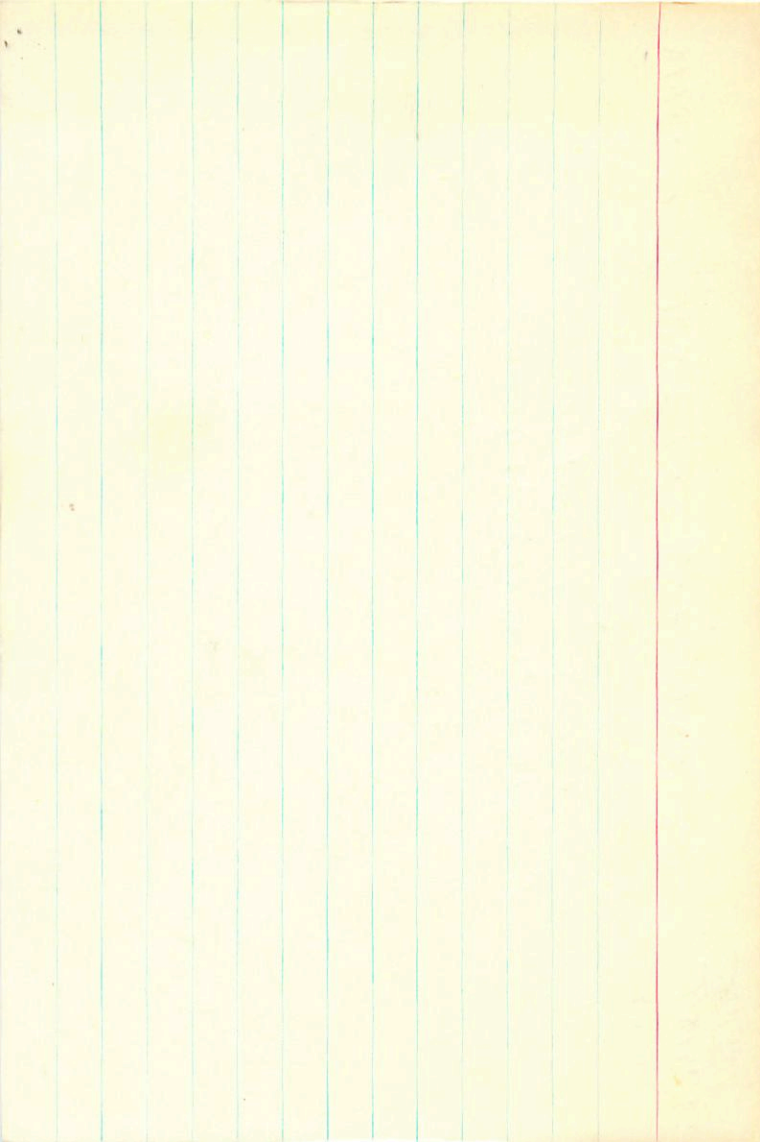
-0408 +0660

+0828 +0325

-0504 -5.0 +27.0

+0252 +2.5 +12.5

+1153 +11.5 +9.6



2169

6 O.S.G

+14 00

Tangles
Simpson

6 Slam

$\rho = +16$

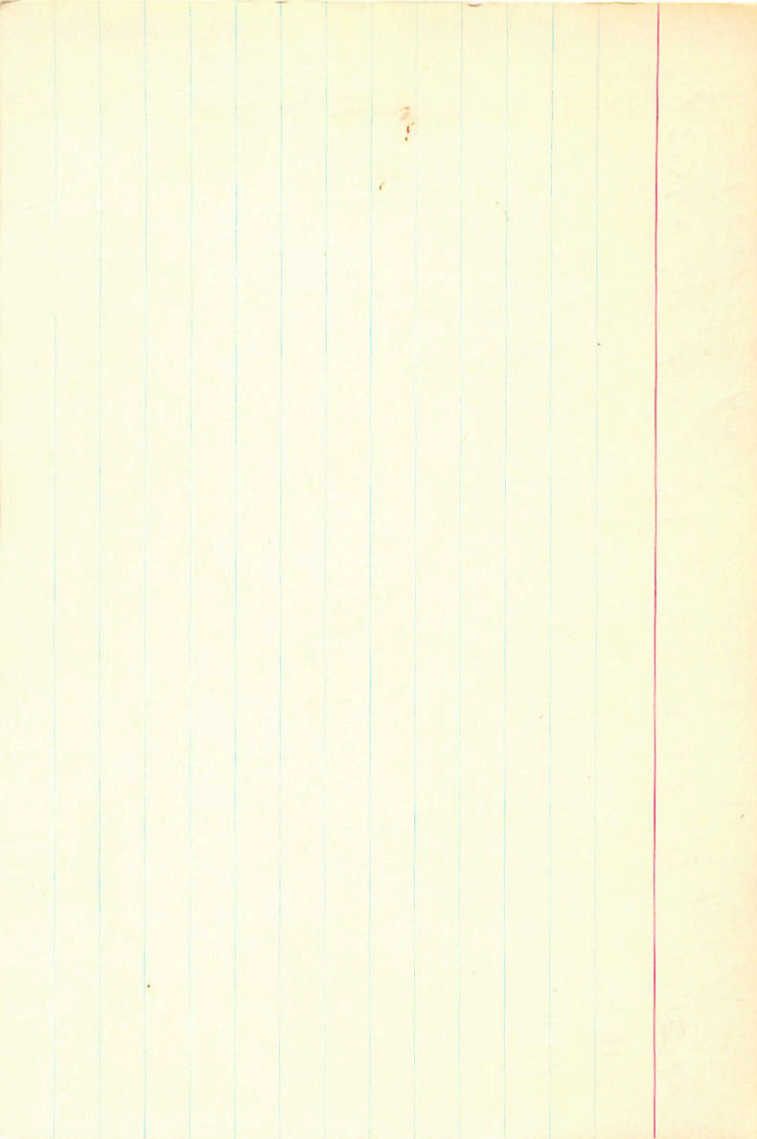
-067 $+241$ $+468$
 -143 $+836$ -243
 -1864 $+493$ -063

$+004$ -016 5 Slam
 -2 $+2$ GC + Yale Zone

 $+002$ -014 $\rightarrow N80$

1000 No.

-01600	-16	+15.4	0
-05548	-55	-4	-60
-0327	-33	0	



6-102-51

6 024 +10 76

256 137

Ⓢ 176 Ⓢ

+171145

4544

844 067 12

6.1

Ⓢ

+176

+17.9

212

-216

+202-216

3.3

+17.6

+0142-231 PPM

+203-231

213

-221

3.11

47.6

2952

R.A. : 6.100
DEC. : 17.950
PM. R.A. : 213.000
PM. DEC. : -231.000
DISTANCE : 3.100
MODULUS : 42
RAD. VEL. : 17.600

q1 (U) : -0.090
q2 (U) : 0.192
q3 (U) : 0.977
dU : -296.123
U : 4.857

q1 (V) : -0.481
q2 (V) : 0.851
q3 (V) : -0.211
dV : %-1393.636
V : -61.811

2
q1 (W) : 0.872
q2 (W) : 0.489
q3 (W) : -0.016
dW : 302.514
W : 12.334

42272

6 07.8

426 03

7.4-8.3

+48 km/hr

+ 21 km

+0006 ±0.1

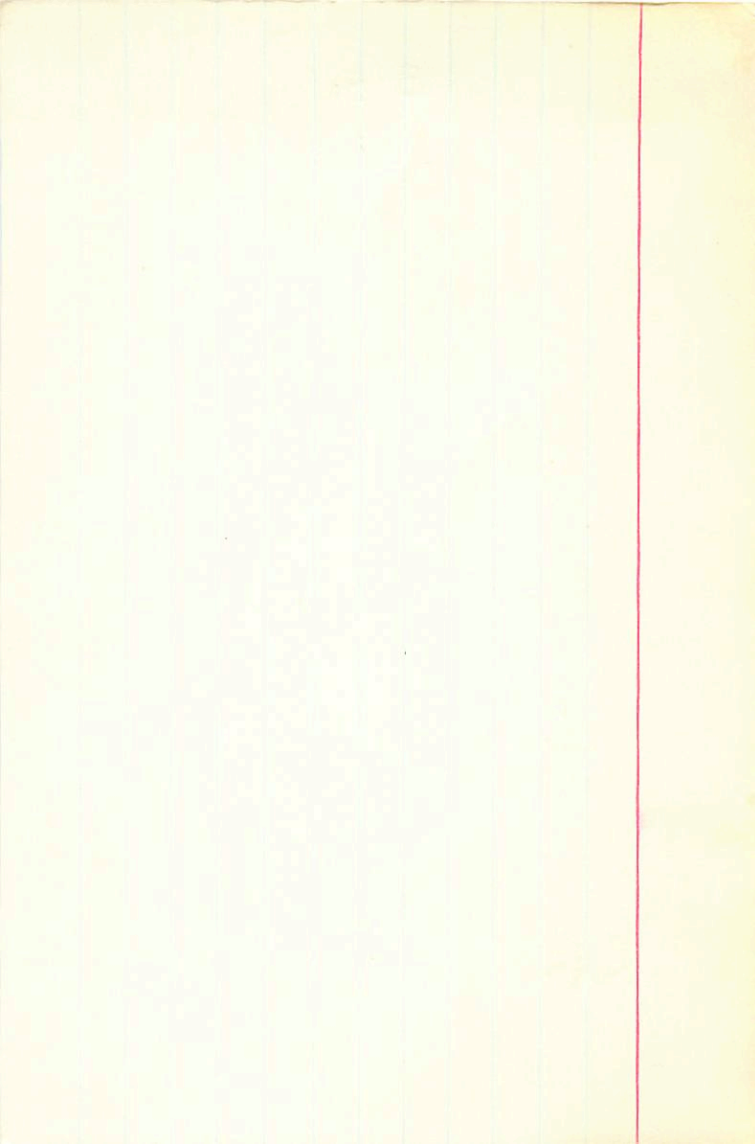
-0007 ±3.2

42601117

46.835 1904.5

37.66 1902.2

Healy



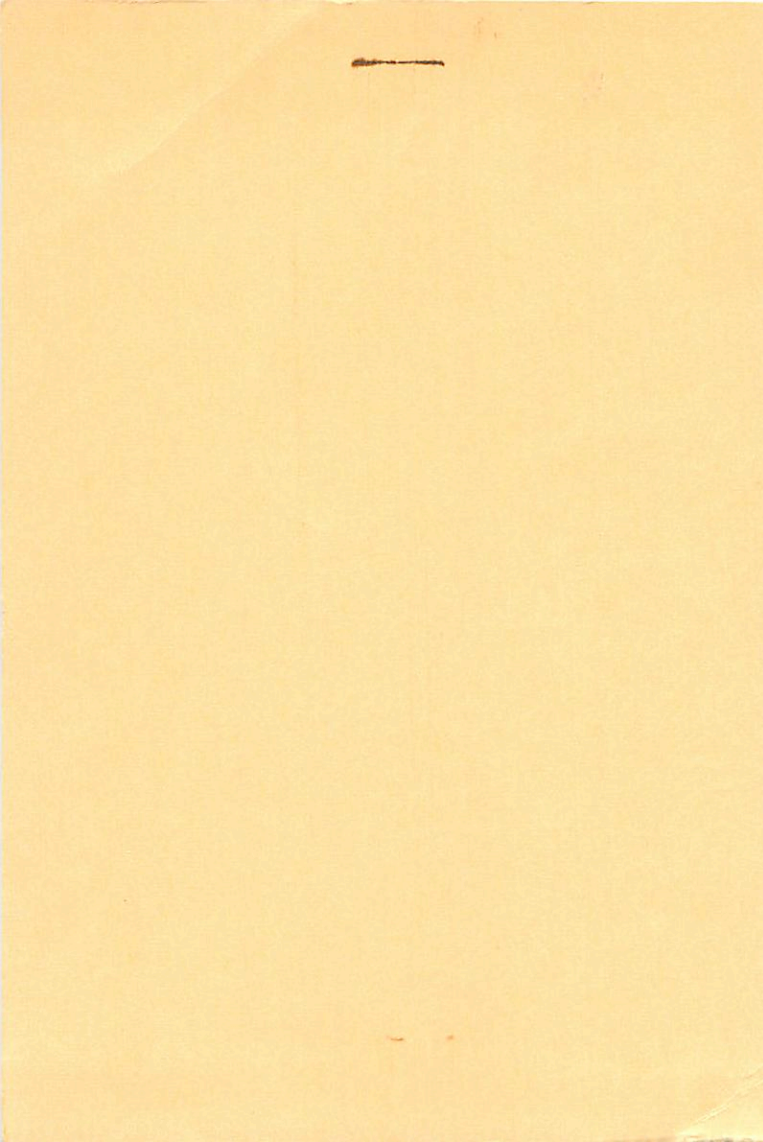
6 082 +10 24

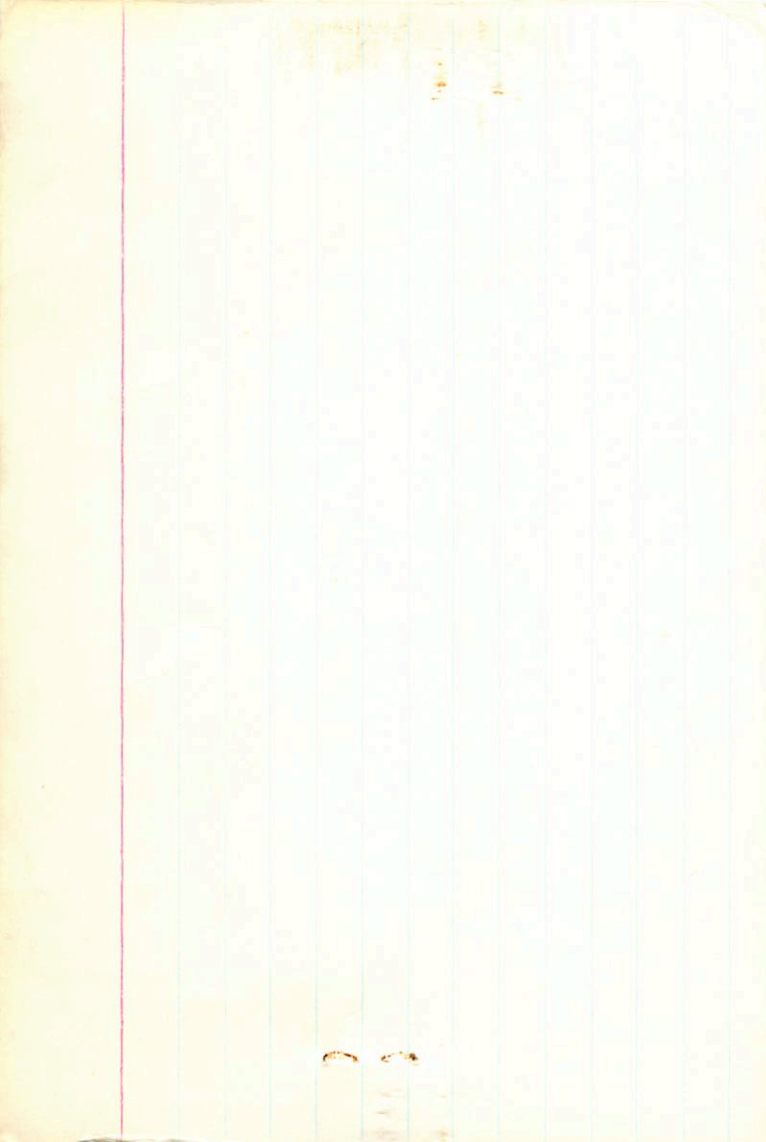
710.1032

274

071-967

5703 3124 }
7035 -9443 }





X Aw 4 08.3 750 15

-182

2

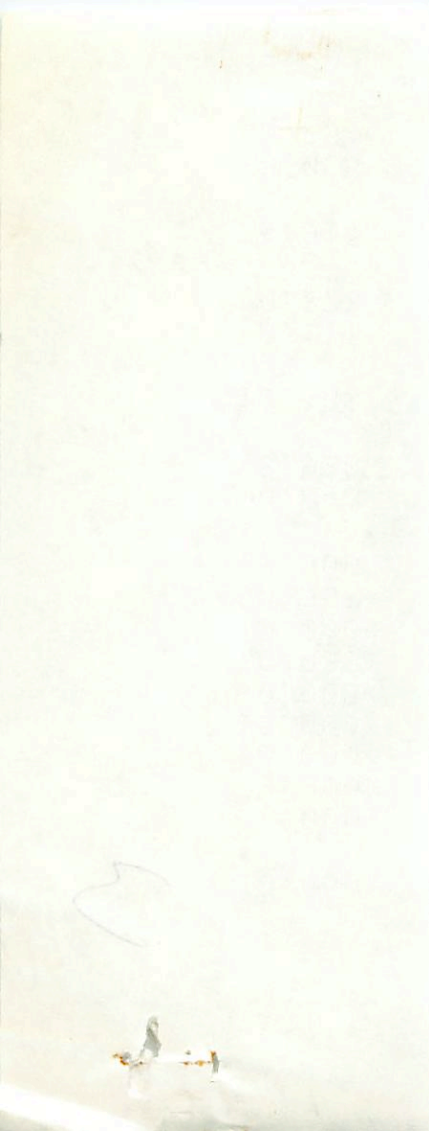
~~$$\begin{array}{r} +0034 \\ - \quad 3 \\ \hline +3 \\ 0 \end{array}$$~~

~~$$\begin{array}{r} +0007 \\ - 24 \\ \hline 41 \\ -28 \end{array}$$~~

~~but.~~

X Aw 825

70 71.02 Barro



-39, 304

0, 254
-0, 055

-74, 914

0, 273
-0, 111

13, 403

0, 929
0, 048

-13, 000
630, 957

9, 000*
-0, 028*
0, 000*
15, 000*
50, 000*
8, 300*
6, 000*
0, 000*

3



-0096 ± 3.9 +022 ± 3.8
0099 +017

5.2 B9 +17.58
B87 +1.5①

43107 6 09.1 -68 50

3908

7880

V Dor
L Dor

3.551 1903.4 49 58.14 1902.2
447
3.998

68 49
90 119
081128 897 2816
1140

3.684
-477
637
58.41 1940.37
-8
58.49

45.0

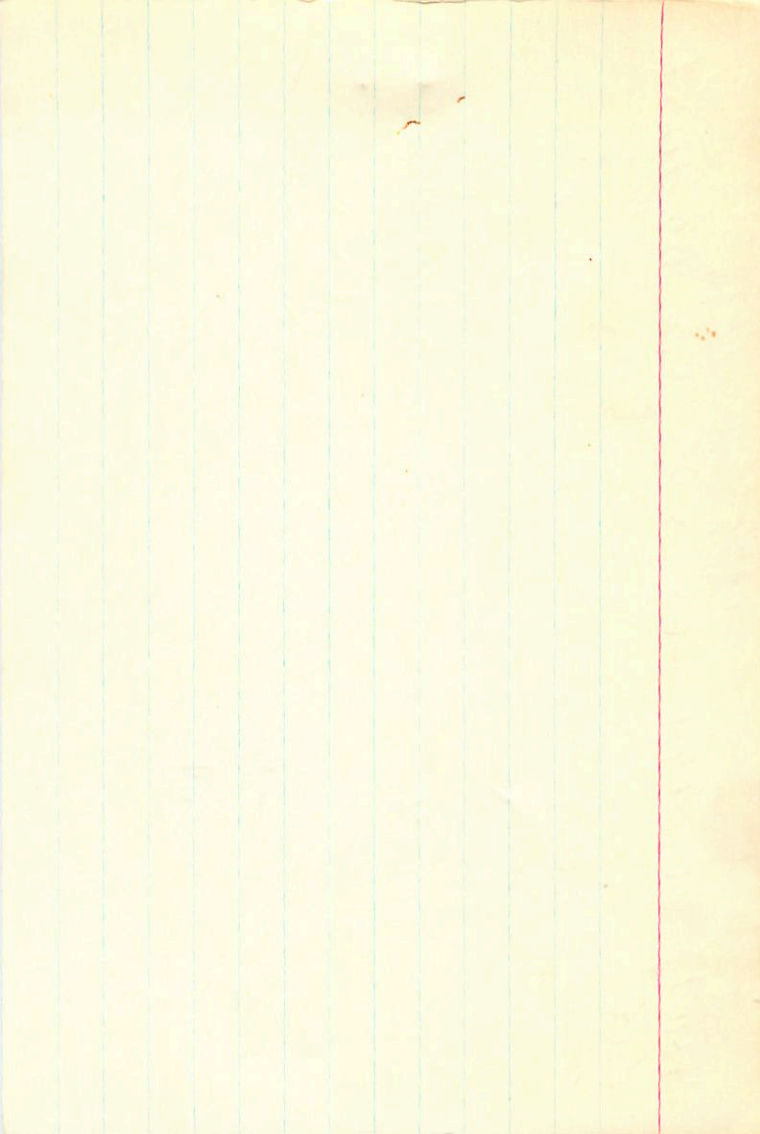
1085
542
-446

94.77
48.4

46.2

3.422
26
448

58.50 195645
+14
5836



-12.5 (3)

6 09.6 +15 22 65

42637

+150/107

8.45-10.91+0615 (2)

8.20-10.325 (3)

7⁸⁶
7⁴

-12.5 Hopki

+015 -037706

+019 -034 GC

+017 -0325 FRY

+017-032 +600

9

102

2

6

0*

0*

0*

0*

0*

17*

32*

00*

95

00

044

066

403

166

256

.915

.003

.025

.578

2188.000*

6.000*

9.800*

51.000*

11.000*

-0.004*

-0.069*

5.500*

125.893

10.800

0.124

0.922

25.603

-0.264

0.285

-30.121

-0.149

0.264

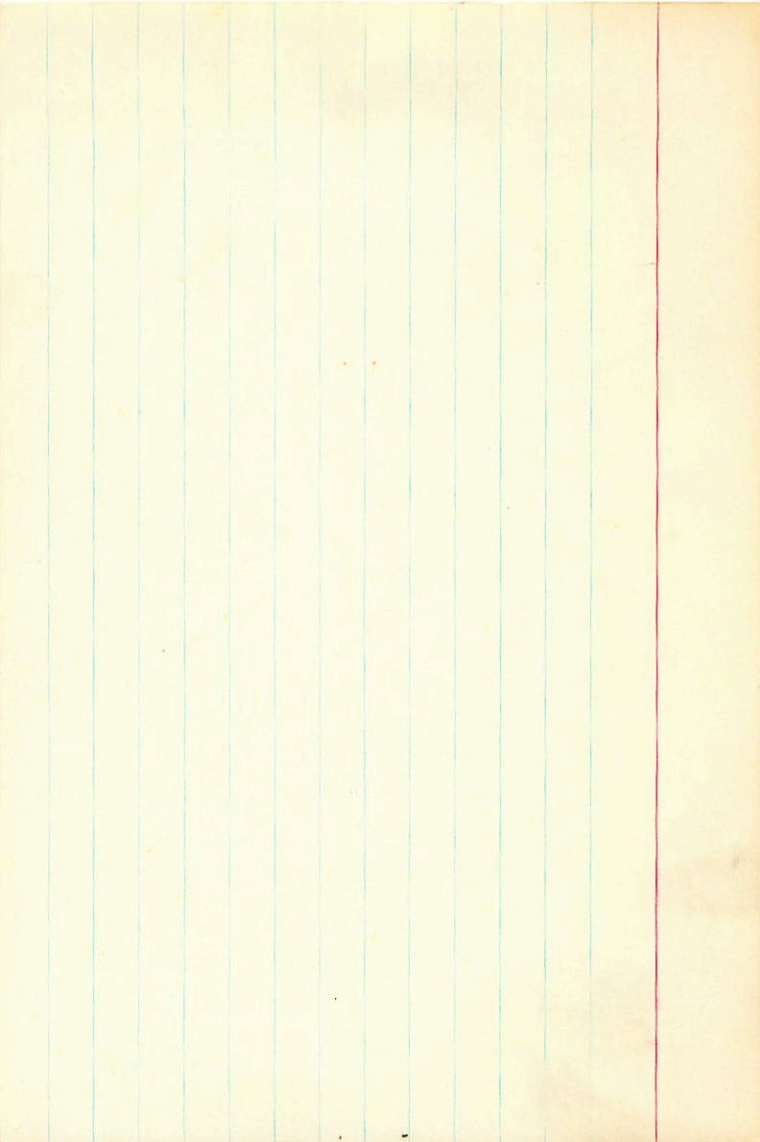
-15.964

5

H042616 G 10.2 +41 43 Aop +0.8 a

7913 6.90 +0.05 +0.03 .0065

+001	-004	Gm2
+003	-003	
<hr/>	<hr/>	
+002	-004	



788 ①

7² Dec 6 11.1 -65- 35 MY +34.5e

43455

3930

7946

5.00 +1.59 Gene

-029 T1116c

-019 T122630

9 +12.2

-6030 +3.2 +113 E3.5

-6038

788

311

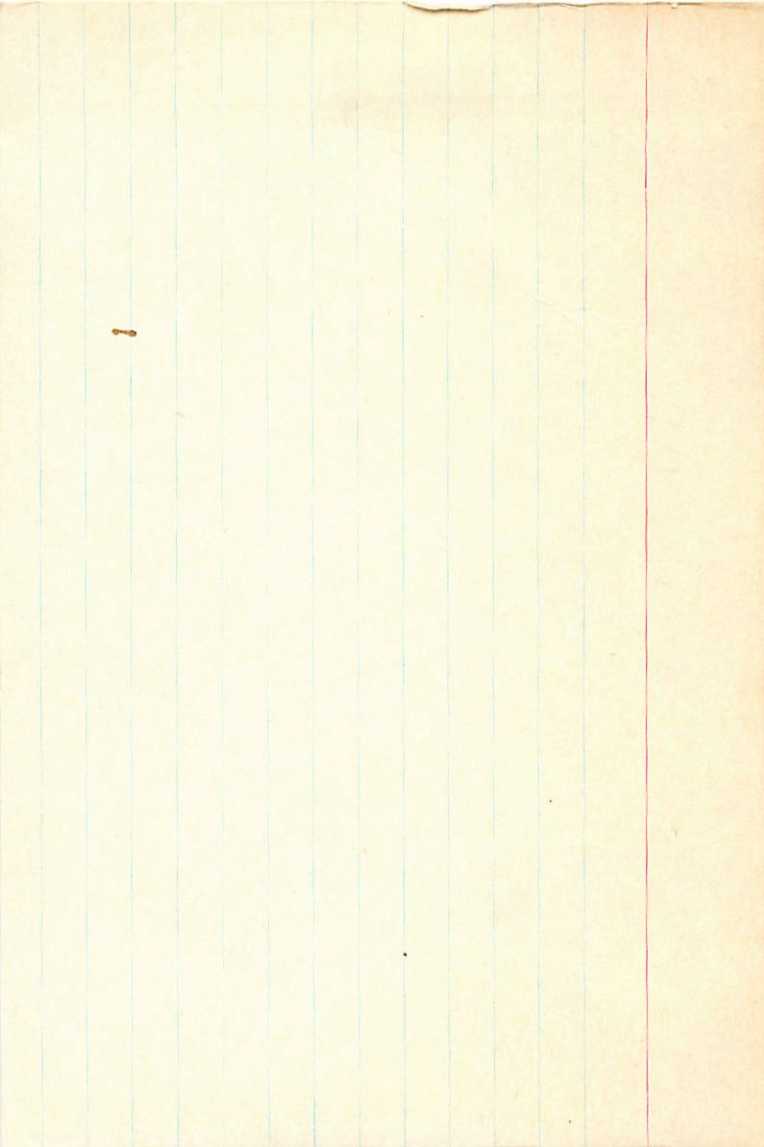
188

6c7956 6 11.4 +17 55 Am

ATUM -0003 -011 12650
+288 0002

934

1952.22	137	0.35	4V0
1959.15	139	0.47	3V0
1961.67	141	0.44	4B



406m

42633

6 11.2 +60 01 5.6 51R3 +12.16

+0050 ± 2.4 -021 ± 1.7
+0041 -021

3932

11.178 1897.5 +60 0 56.54 1894.3

7949

262
10,914
1.17
57.71

56.33
74.692
17.022
-0.07
24
031

78.17 1927.1

19.55
59.175
-2.45
56.33

38.6

152
24
031

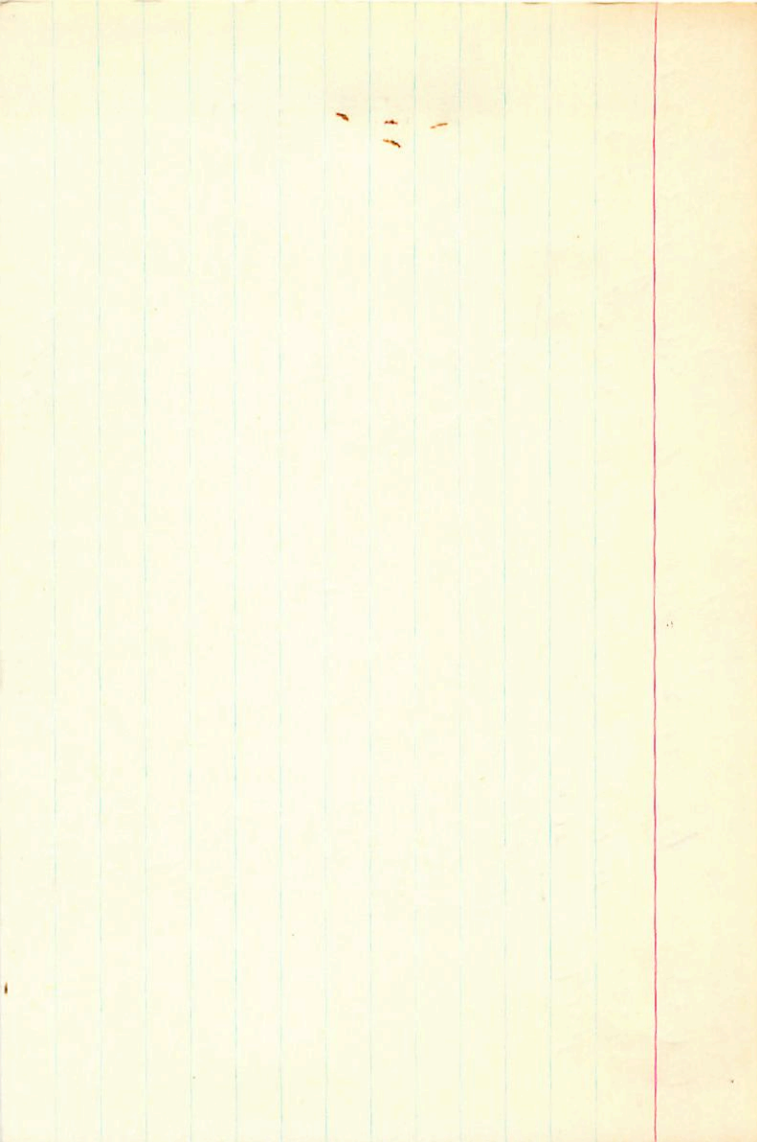
72.12
36.1
41.9

11.083
38
121

57.03 1945.02
56.73
-13
56.60

.076
+1.160

56.52
-0.89



18'
1870 (X)

2214 6 11.9 7 222 31 11211 113 114

7569 3.28 + 1.61 + 1.66 F
4255 0.2mg 3.25V + 1.58 + 1.61 8/E

2.17 + 1.00 J
2.11 + 1.06 E
2.14 + 1.06
1.76
1.74
1.74
0.25
5.75
5.75

58 58 20 85 20
m¹⁴

0.45
0.25
5.75
5.75
m₁₄ = -2.2 0.2W
= -1.4

±001
1007
280
150
-6048 -013

210 990
-066 -013

401 202
401 202
1001
3.75
+D

-60472 -013

-0650
-065 -013



6

10

2

2216.800*

6.000*

11.900*

22.000*

31.000*

-0.066*

-0.013*

4.650*

85.114

19.000

0.028

0.987

21.143

0.093

-0.154

4.993

-0.304

0.044

-25.011

6



2216.000*

6.000*

11.900*

22.000*

31.000*

-0.065*

-0.013*

4.600*

83.176

19.000

0.028

0.987

21.045

0.091

-0.151

6

42983 6 11.3 +02 50 dko -26.3 6 u(3)

GC7951

W3933 7.34 +0.975 +0.97 2555 18"

Y1442

020163

-54 -44 -14

~~138~~ 7000 44 .030

-45 -25 -10 .030

+057 -276 GC

757A(20)

+00385+10.0 -276.5
+0051 -252

15.510 1907.8

-160

350

15.464

50

+2

49 38.97 1907.3

11.79

5076

43.10 1937.05

18

4328

AD54849

43017 6 12.3 +36 10¹¹ (6.7 dFV +6.8 σ)

3947

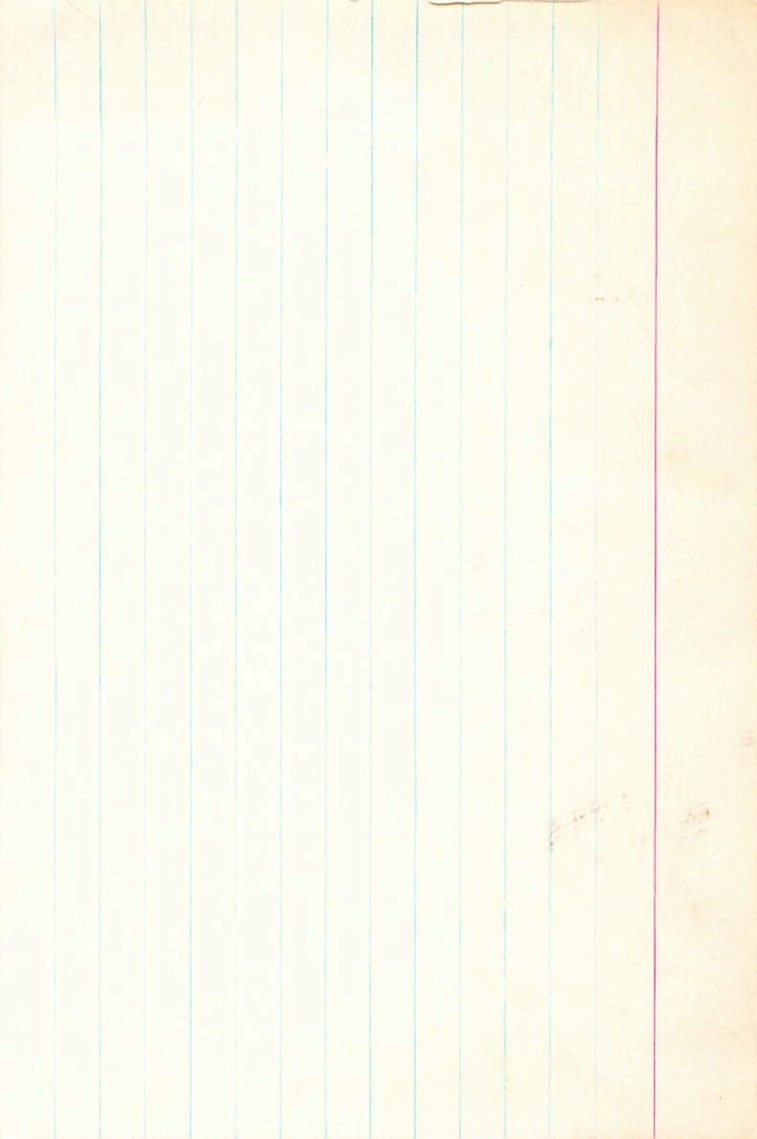
40 (7.5 dFV +9.2)

7983

-0052 +001 N30

HR2217

-0052 \pm 3.0 +004 \pm 1.9 GC \rightarrow N30

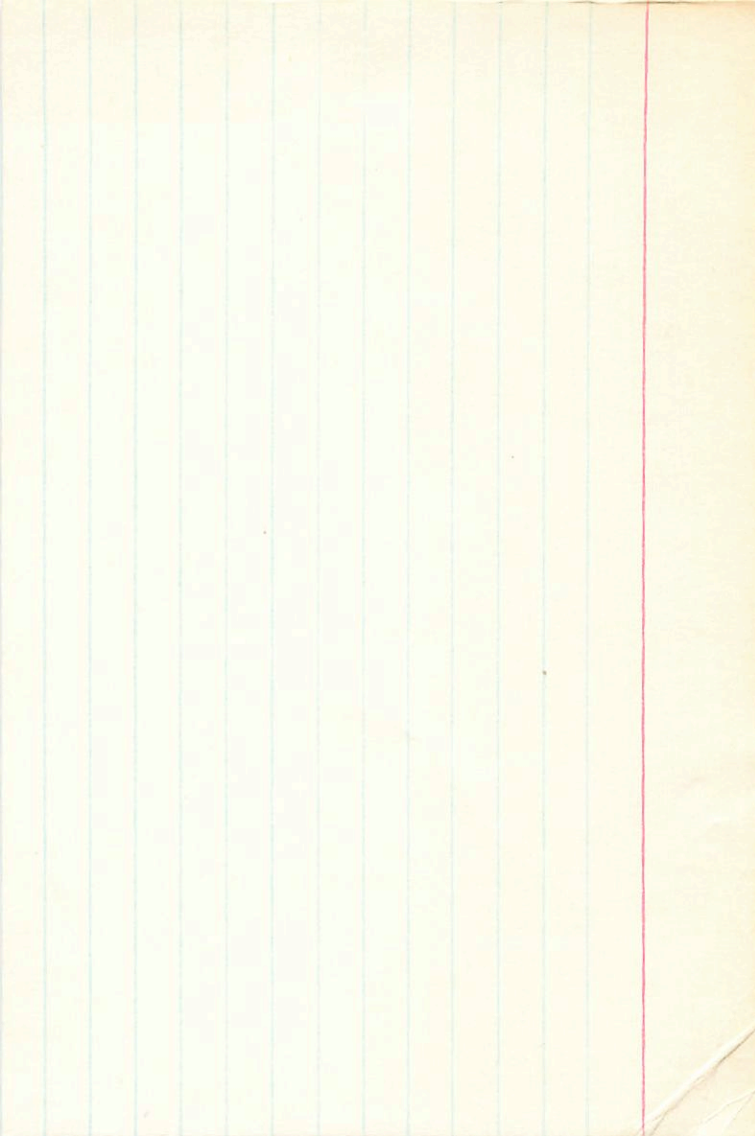


V Pic

6 12.6 - 59 54

f114 F-ent

Mo M



43185
+1501141

Van
and

6 12.8 718 18.5

⑤ 951 - 156(5)

+37 +12
000- 8100
000- 0218

0000- 0200
0000- 0100

0001- 0140

0307
0002
811-
0100
398
548 - 7636
8455
8089
6457

6000
0000-010
0000-010

-20.1336

360 ± 0.8
3000

← ~~factory~~ Exponential
6 13.0

+521 (2) Var 1.3-11
5.41 $\sqrt{1.325}$

2242

43896

+2.2
+59.6

DAS P
43.76

59317
+17
300

2.1

-0008
-0001
-0004
000

+000455

+024 ± 8.3

+024

+027
+027 20.06 4/7
-1.31
21.37

662997

(+75 to +66)

676

59.274
274

14.63
19.64

5-4.742

38.90

4.512

59256

-0002 +0271

-00058 +0253

260

+18

271

-0082
-0005 +026

53.61
2605
19.66

4526 - 4950

1.17 8917

8.700

20.83
+24
21.59

36050

6431

59.273
+221
201

14.63
+4
19.4

33.492

25.805

59308

301
-1/295

4168 4160

9.09
10.98

1907
+6
19.26 / 19.17

8
0
4
4
4.13

$$\chi = 0.43(17) + 0.4(15.5) - (10.2)$$

0.50

43299

6 132 +10 18

807x

~~147880~~

~~101890~~

77 7435

10.643 8.7

10.684

61.98

55.5

43358 6 13.3 +01 11 6.3 FS +2.68

3963

+480

8017

-0002 +023 N30

-0005 ± 4.5 +033 ± 3.9 GC 7N30

-010

+028

+6.7
+6.7
+1.0

6.4.6PA.

-114 468 875

+0054 +0621

+0675 +44 +2.3

-467 752 -463

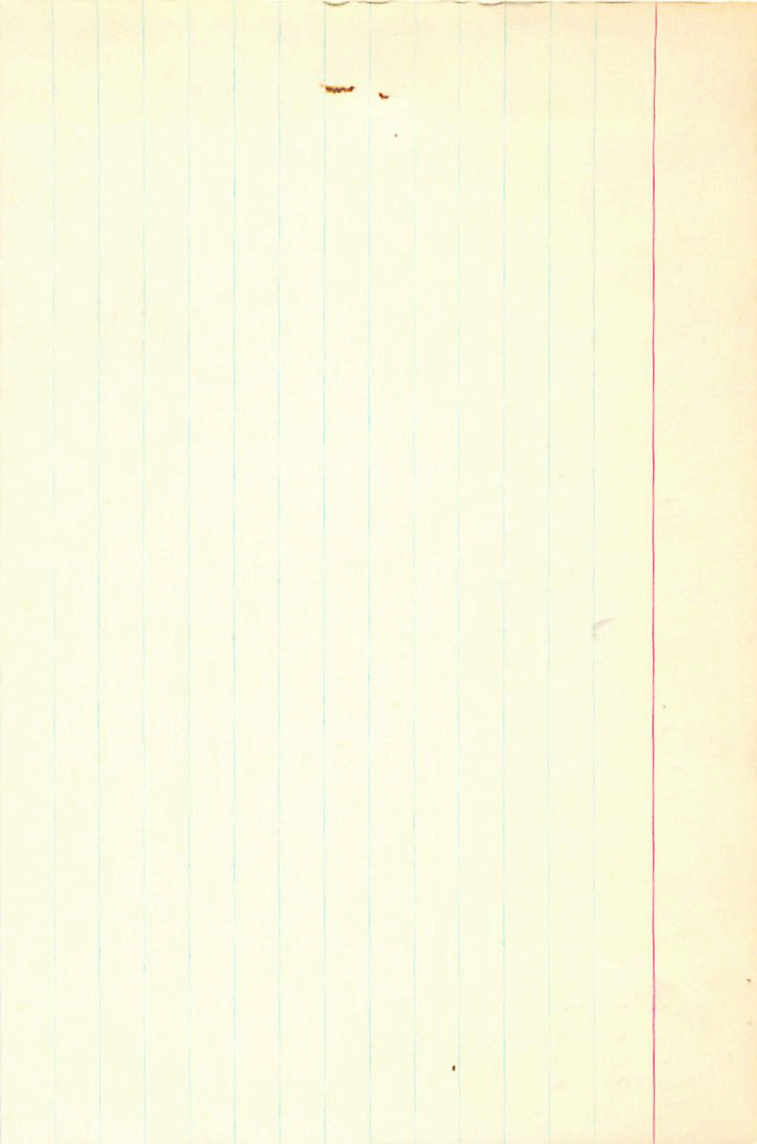
+0221 +0998

+1219 +17.9 -1.2

876 962 -132

-0415 +0613

+0198 +13 -0.3



+250118.8
254229

40026 ± 15.0
+ 37
6 13.6 +25 74

+26
+32
+10
-435
-432
-445
246 +446

8028
3960

9.8

+035 -435 GC
+048 -412 X

34.224 1912.9 +25 13 48.39 190.4 +041

-096
128

17.23
5162

188
1000
161

34.154
170
34.15
173

57.99 1928.04

290
18.6

57.27 1930.0

57.19
116

57.58
-8.0

958 -059 426 505 +041 -438 +44 -157 ¹⁹49 -1506
-041 187 -002 010 -242 ¹⁷977 +388 +2 +40 ³⁹

-3 +57 -18 05

-1 +51 -4 08

-1 +50 -2 09

7

6.200
25.200
60.000
-438.000
0.000
10
44.000

-0.113
0.068
0.991
-169.977
41.918

-0.460
0.876
-0.113
-1939.627
-24.378

0.876
0.477
0.067
-765.162
-4.712



14R 2225
42 Ann

17

157 192 804 2.747
²³⁹ ²²³
642

6 13.9 146 27 13.2 n -8 c

W 3970

6.52 +0.27 +0.09 -040 +014 GC

14043244

FOU

GC 8007
Jy 6/11/22 ✓

57.077 91.6
228
305

-008923 0
-0032

+014 ± 2.6
100 34.80 86.9
-55
33.92

+242 } NW
+20 }

51.067
+24
50.96

58.04

34.41
-11
34.31

-9.5

+3.4

-4.7 } AD

-20.4

-11.3

958 - 060 724 689 - 040 7014 - 8 010 - 6 047

040 010 002 - 001 144 - 038 - 5.5 0 - 5 025

+ 5 - 6 - 8

+ 12 - 8 - 3

015

$$+0009 \pm 2.0$$

$$-0002$$

$$-074 \pm 2.2$$

$$-074$$

$$12.789 \quad 19034$$

$$\begin{array}{r} -042 \\ \hline 747 \end{array}$$

$$38.755$$

$$33915$$

$$12.670$$

$$\begin{array}{r} 668 \\ 39 \\ \hline 707 \end{array}$$

$$12.752$$

$$\begin{array}{r} 24 \\ \hline 776 \end{array}$$

$$\begin{array}{r} 83 \\ \hline 742 \\ \hline -005 \end{array}$$

30.0

+27

$$13 \quad 53.10 \quad 1899.0$$

$$\begin{array}{r} 3.77 \\ \hline 56.85 \end{array}$$

$$25.87 \quad 1927.55$$

$$29.82$$

$$\begin{array}{r} 56.05 \\ -1.71 \\ \hline 54.34 \end{array}$$

$$\begin{array}{r} 54.34 \\ 21 \\ \hline 54.55 \end{array}$$

$$54.55$$

$$54.04 \quad 1939.22$$

$$\begin{array}{r} 1 \\ \hline 54.07 \end{array}$$

$$\begin{array}{r} 54.31 \\ -2.54 \\ \hline 51.77 \end{array}$$

$$46.77$$

$$33.4$$

$$\textcircled{34.4}$$

hb
680

2235 2 days

6 15.2 159 02

-3.68

4.35" 0.00"

\sqrt{A}

-005 1022-66

-005 1024 630

-010 1020 180

-007 1022

998 -066 857 515 -007 +022 -3.6 019 -3.2 052
007 -019 0 033 -050 -15. 0.1 -1.8 029

+2 -6 -1

$\boxed{-5+3-1}$

+2.3 -7.5 +0.2

015

$\boxed{-6.6 +4.8 -0.6}$

028

+1.3 -5.0 -1.4

-4.9 +1.7 -0.9



42637.000*

6.000*

9.600*

15.000*

22.000*

0.017*

-0.032*

7.400*

301.995

-12.500

-0.044

0.966

-25.403

-0.166

-0.256

-46.915

-0.003

-0.025

-0.578

4

(102158)

6 098 451 11 151 860 7

+10.88
92014
6.03 10.11

-003 -069 DC
-1 0
-004

|||
/

|||

6