

148241 2 6:21 P.M. 22

[107-110]

148241
✓ 11-
107



16



VEL.	28.880
MODULUS	288
STANICE	9.350
DEC.	-14.888
R.A.	17.888
DEC.	-14.488
R.A.	2.350

p1 (U)	0.888
p2 (U)	0.988
p3 (U)	0.483
p4	13.732
p5	21.812

p1 (V)	-0.448
p2 (V)	0.201
p3 (V)	-0.031
p4	-101.881
p5	-53.410

p1 (W)	0.332
p2 (W)	0.248
p3 (W)	-0.612
p4	0.448
p5	-18.818

10

R.A. : 2.250
DEC. : -14.400
R.A. : 17.000
DEC. : -14.000
DISTANCE : 9.250
MODULUS : 708
D. VEL. : 28.000

q1 (U) : 0.688
q2 (U) : 0.603
q3 (U) : 0.403
dU : 13.732
U : 21.015

q1 (V) : -0.648
q2 (V) : 0.761
q3 (V) : -0.031
dV : -101.081
V : -72.419

q1 (W) : 0.325
q2 (W) : 0.240
q3 (W) : -0.915
dW : 9.448
W : -18.918

14284

-140423

1255

2 15.7

41-

22

ee

1.8

9MB

1.0

3W

+0004 1022

-1

-3

+0023 1019

+004 1016

^s
-0005 1031 1000h

-1

-3

-6
+28



11



14284.000*

2.000*

15.700*

-14.000*

-22.000*

0.000*

0.019*

9.000*

634.957

3

671 2 160 246 15 442

5.5

~~524 00 07 6.05~~

100 156 1085 2.882

045 172 1074

-1456 44

444

-1016 -0172

+0.15
5.8
5.655

-0165
rec-610
-017-021

671.000*

2.000*

16.000*

46.000*

15.000*

-0.017*

-0.021*

5.650*

134.896

-14.500

-0.049

0.725

52

-17.190

0.012

0.646

23 Am

-0015 ± 2.8
-0021

-117 ± 2.0

14305 2 16.4 + 19 28 6.8 dF8 + 2.26

1297

2790 21.606 1904.8 + 19 27 35.70 1798.6
 $\frac{068}{.676}$

21.634
+ 1
642

58.195

23.335

21.530

$\frac{596}{.512}$
+ $\frac{12}{398}$
-.056

29.43

31.6

26.8

$\frac{620}{.620}$
-.056

44

37.27

+9

37.36

20 41.84

6 56.70

28 38.84

- 87

37.24

37.24

37.9

37.9

37.64

- 4.07

37.27 1933.8
627

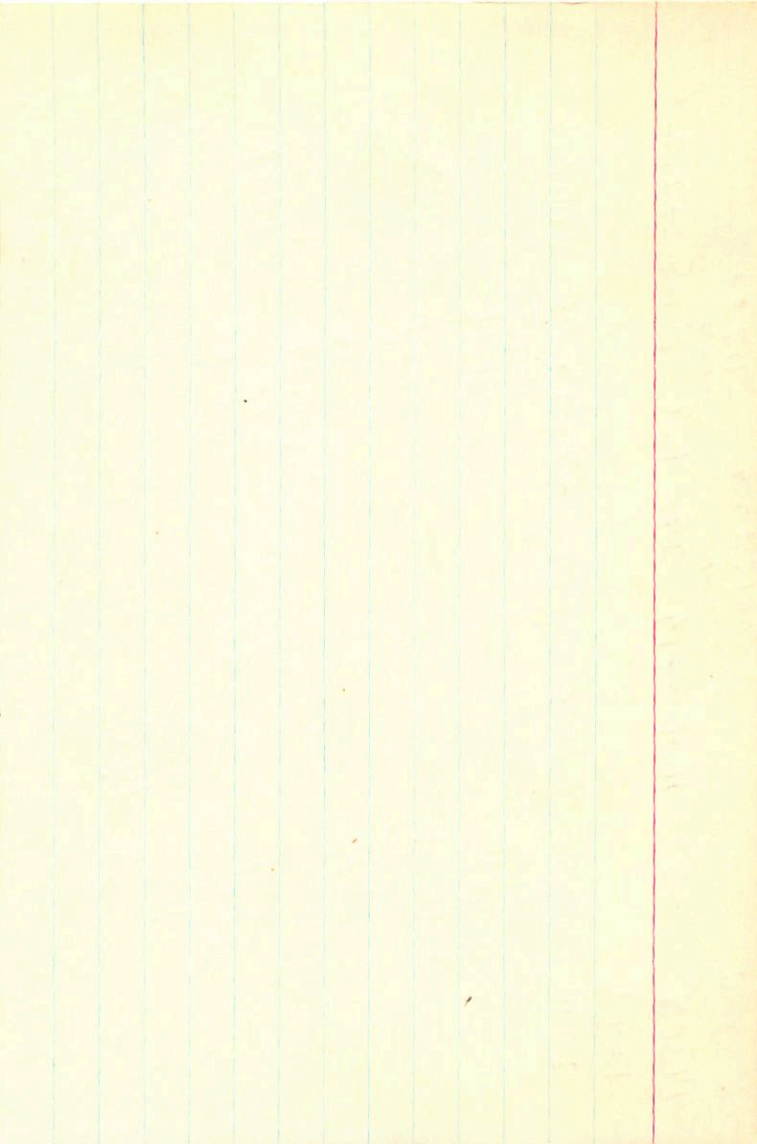
1628.91

31.4

32.8

37.64

- 4.07

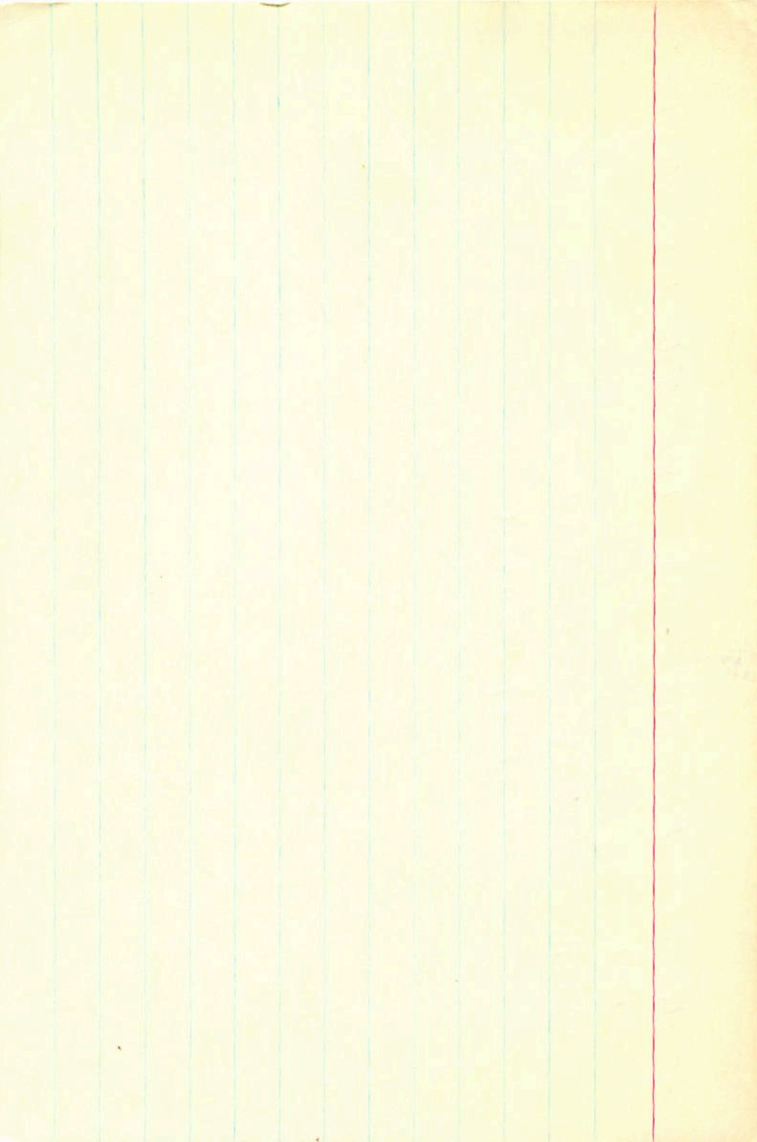


14641 7 18.3 -56 10 5.6 125 +49.18

1317

2821 +0035 +019 N30

+0033 ±4.7 +027 ±3.3



+700169 2 18.5 +70 57 w(+6.6) -1549

GC 2826

+475
1321
8.90 +0.86 +0.64 112E P
S = -0.8

+89 -100 +14 .620

+62 -86 +8 .027 ✓

+57 -81 +6 .030

+36 -66 +4 .040

+574 -146 GC

+535 -176 GC

-25.76w(3)

30A(20)
34A(10) 3425
41G(10)

+1171 F12.2 -146715.0
1098 -157

29.554 1409.4 +20 57 2.11 1510.4

-4754

5728

12.89

24.800

27.01

9.9 1930.0

54

9.82

'061

+1093 +535 -170 GP

+1098 -157 new

+1171 F12 -146715 - Gc

$$+0165 \pm 7.5$$

$$+0142$$

$$-005 \pm 11.3$$

$$14402 \rightarrow 18.7 + 6.8 \pm 3.2 \rightarrow 201 + 11.5 \pm 6$$

2950

$$\begin{array}{r} 366 \\ 102 \\ \hline 732 \\ 1465194^2 \\ \hline 13665194^2 \end{array}$$

$$7.2$$

$$48$$

$$+091 -005 \pm 6.6$$

$$+083 -013 \pm 6.4 \pm$$

$$\hline +087 -009$$

$$+6.8 \pm 3.2$$

$$+7.50$$

$$+1509.0$$

$$+2.0$$

$$+4.70$$

$$40041$$

$$19053$$

$$\begin{array}{r} -737 \\ 3 \\ \hline 29.3 \end{array}$$

$$39.856$$

(32.5)

$$4.70$$

$$1945.76$$

$$\begin{array}{r} 756 \\ \hline 37.8 \\ \hline 28.8 \end{array}$$

$$1532$$

$$+462$$

$$+088 -0.13$$

$$\hline +083 -005$$

$$4.9$$

$$1929.8$$

$$-1.2$$

$$\hline 4.0$$

$$-0.7$$

$$\hline 4.3$$

$$+076 +002$$

$$+091 -005$$

$$\hline +083 -005$$

$$39.56$$

$$50$$

$$50$$

$$475$$

$$\hline 4.05$$

$$4.83$$

568822 930 367 +087-009 11.5 -008 11 -13.7

-050 005 072 -007 -204 365 +4.2 +3 +2

-31 +63 -12 006

10/140 0

-20 +45 -4 005

200

-17 +38 -3 01

+679	-336	+653	+2482	+46.6	+7.5	= 57.1
-651	+135	+747	-2309	-47.6	+5.6	-39.0
+340	+932	+126	+1243	+24.8	+1.4	+26.2

14610

+15°33'

1330

445B

2 15.3 +15 46 8.1 dF1 -216

-210

8.14 ⁶⁹323 136 427 2.625 (4) dlc

+059±5 -112±6

-3 +F

B-V 0.50

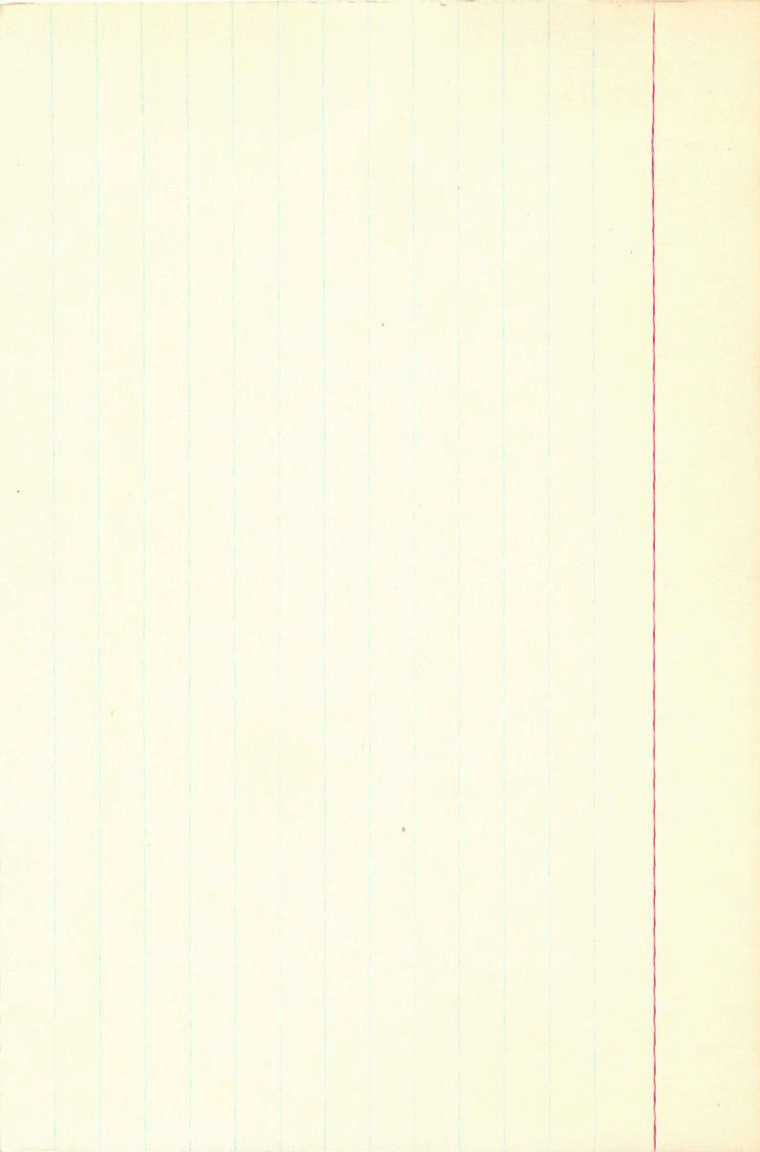
f0037-002 land 054 =104

053-052

next

9702	5354	0976
4555	-216	6909
4446	-2424	1009

449



+0006±9.7 -034±8.0

14692 2 19.4 -14 31 7.4 dA8m +6.06

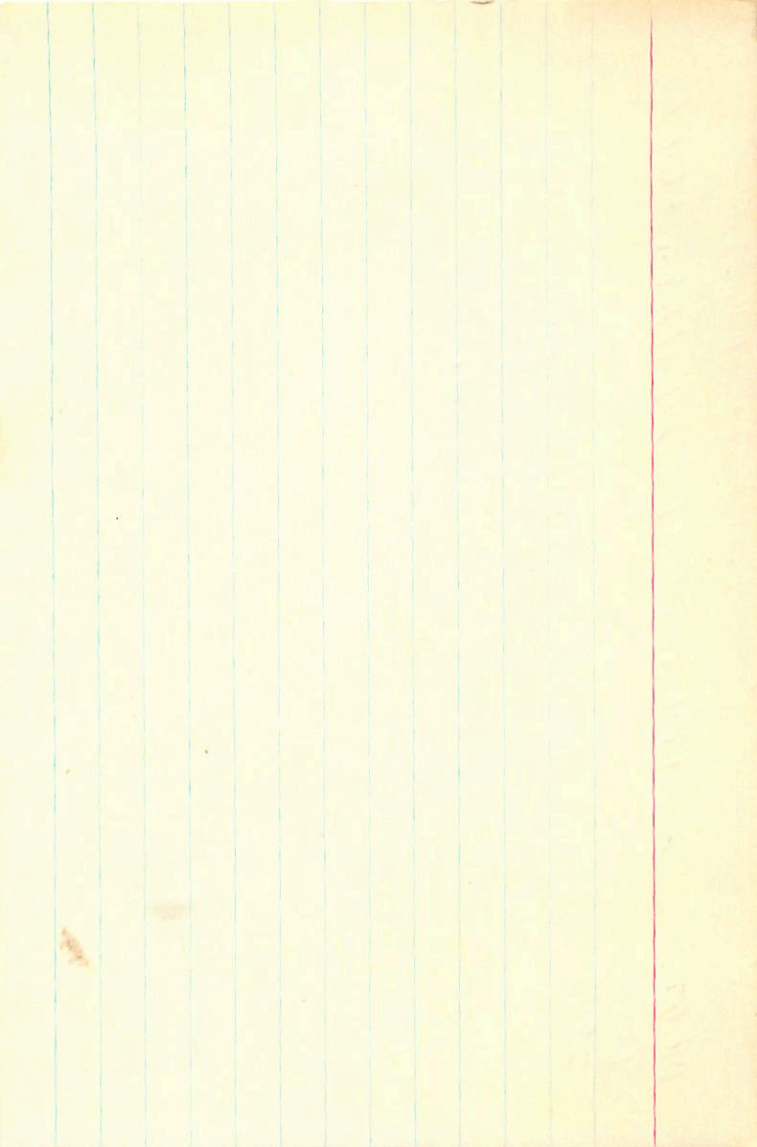
1335

2847

22.915 1897.8 -14 30 42.02-1895.3

$\frac{-031}{.884}$

$\frac{+1.52}{40.50}$



Plumb

13761 2 14.6 -11 00 A 8m

HR652

GL2849

[en] 222-6

[C] 501 ~~234~~

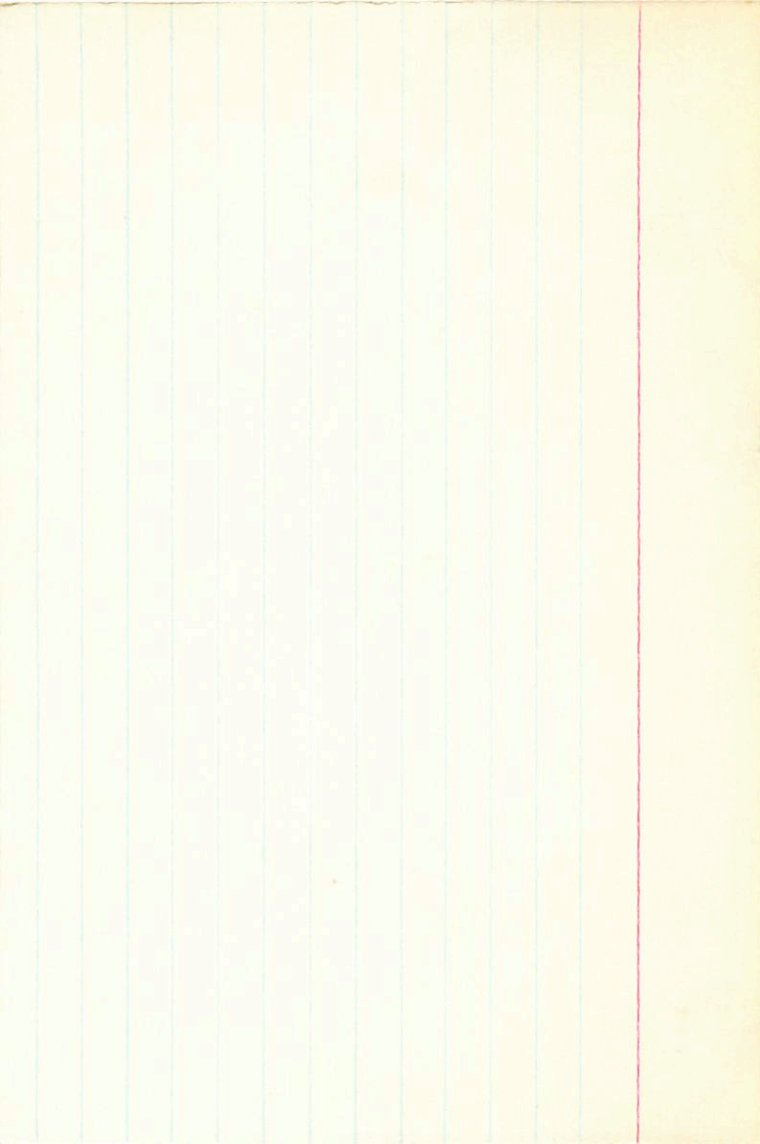
5.44 242.178 544 R.709 ② 35,1,18,4

+116-217-7.5

+207-719 4105

2.88 413-27-7

42-7 +1



-0078 ± 3.0
 -0072
 -0067

-102 ± 2.3
 -095
 -098

14622 2 19.7 +41 10 5.9 d/f 2 -3458

2851

1340

42.911 1894.6 +41 10 13.80 1893.1

-0073
 -0.100

$\frac{5.80}{19.60}$

$\frac{432}{43}$
43.343

9.69 223 -007

33320

$\frac{43010}{130}$
43120

$\frac{110}{120}$
405

$\frac{24.2}{52.78}$ 1928.0

$\frac{16.96}{94}$

$\frac{15.99}{30}$

$\frac{10.29}{10.29}$

42.558 595

$\frac{20}{934}$

13.74 1952.59

$\frac{7009}{1383}$

4x4

A1 ref L.02 C

2220220

058449

43094

A 8.30 + 0.61 + 0.10 ③ ✓

B 15.83 + 0.07 - 0.75 ③

66 7869

HO 14284

F14 +

059 ①

0520	8050
0520	8050 - 0520
0520	5008
0520	4922

$P_M = 0.159i \quad 714.3$

1354

2 21.1

449 ✓

-13.39

694

$$\begin{array}{r} 474 \\ 24 \\ \hline 1896 \\ 948 \\ \hline 11376 \end{array}$$

$$\begin{array}{r} 474 \\ 379 \\ \hline 33179 \\ 33179 \\ \hline 14228 \\ 1753 \end{array}$$

13.0 (2)

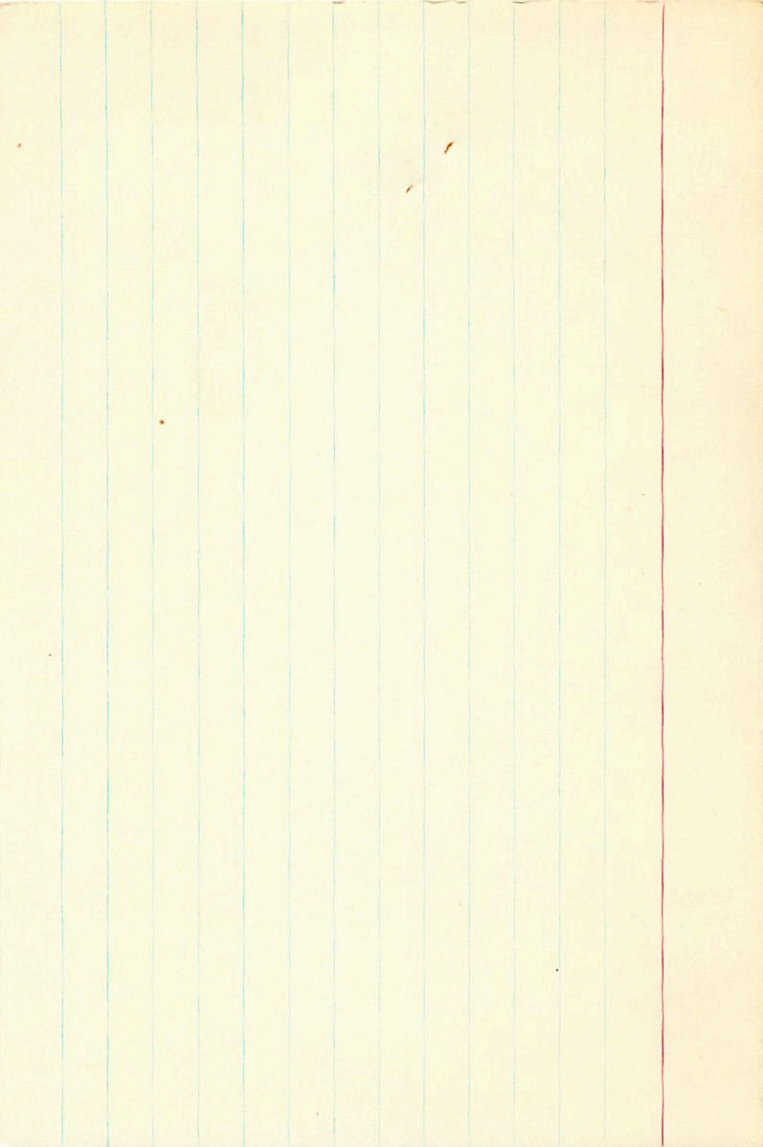
+024 -036 60 →

10000 1080 484

676 -115 728
 -652 367 664
 343 923 -174

+0770 +0202
 -0741 -0644
 +0390 -1620

796 79.5
 +0972 +7.8 -9.7
 -1385 -11.0 -8.8
 -1230 -9.8 +2.3



18915

12/3/40

1000 1000

1000 1000

1000 1000

1000 1000

1000 1000

1000 1000

1000 1000

R.A. : 2.400
DEC. : 25.250
PM. R.A. : -4.000
PM. DEC. : 9.000
DISTANCE : 6.800
MODULUS : 229
RAD. VEL. : -9.500

B
q1 (U) : 0.667
q2 (U) : 0.195
q3 (U) : 0.719
dU : -3.097
U : -7.543

13
q1 (V) : -0.654
q2 (V) : 0.616
q3 (V) : 0.439
dV : 37.507
V : 4.424

q1 (W) : 0.358
q2 (W) : 0.763
q3 (W) : -0.539
dW : 26.413
W : 11.168

65 Ann
14872

AR 699

2

22.3

+50

03

7.9

9125

-4.52

+0024 ± 2.2
+0028

-013 ± 1.8
-014

1364

2902

16.474
-124

15.350

1898.2

+50

3

12.92

1893.7

+73

15.65

4.60

+1.31

36.56
39.695

16.255
169

1424

420

56 24.3
6 49.72

3 14.02

1.06

12.96
+33.9

13.2

1926.1

71.3

37.4

454

+1.04

16.500

127

48

13.13

1945.20

-29

12.8

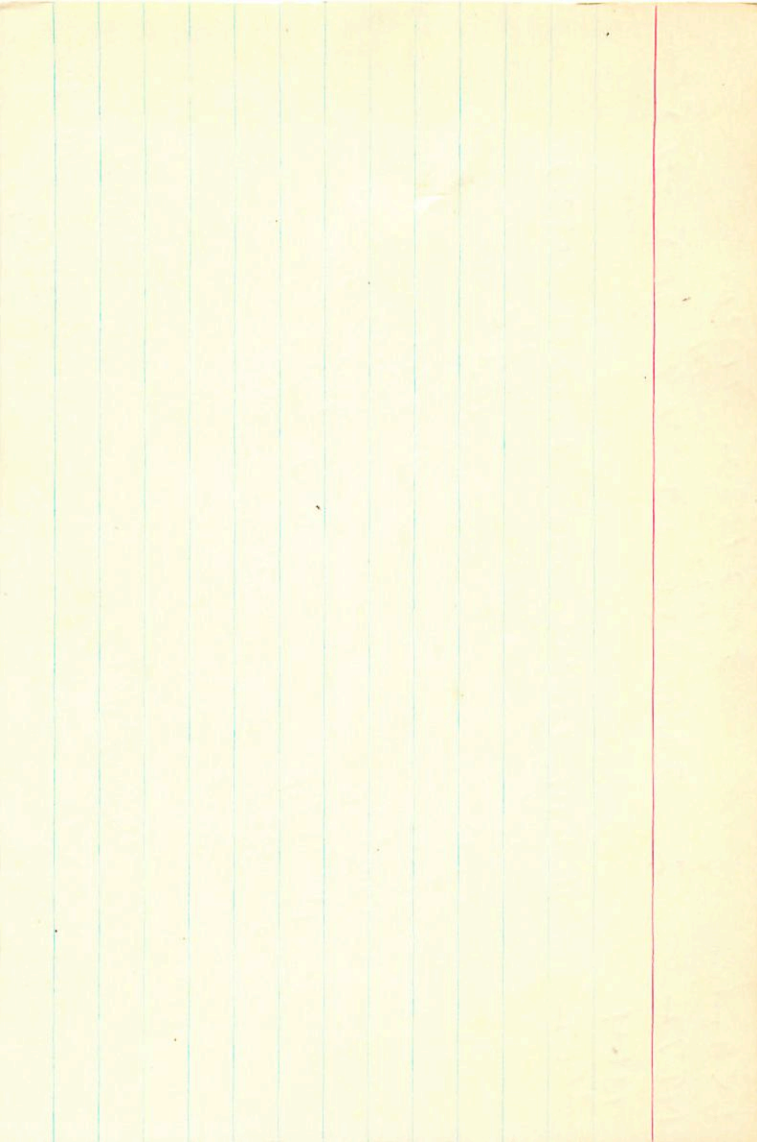
35.6

13.06

41.9

-1.59

500



USA and

HR 699

2 22.3 450 03 NY VII

4.50 4.60 4.70

4.60⁺ +1.316

-4.50

+023 -013 6C

+024 -013 F123

+024 -013

no 1/7

027.4 -010.3
FR 5 3000

37.4

40.3

45

4.6

54

R.A. :	2.400
DEC. :	50.050
R.A. :	37.400
DEC. :	-10.300
ANCE :	4.500
LUS :	79
VEL. :	-4.500

+550616

WIBLS

2 22.4 +55 53

-32 C

Dmte .574

4871

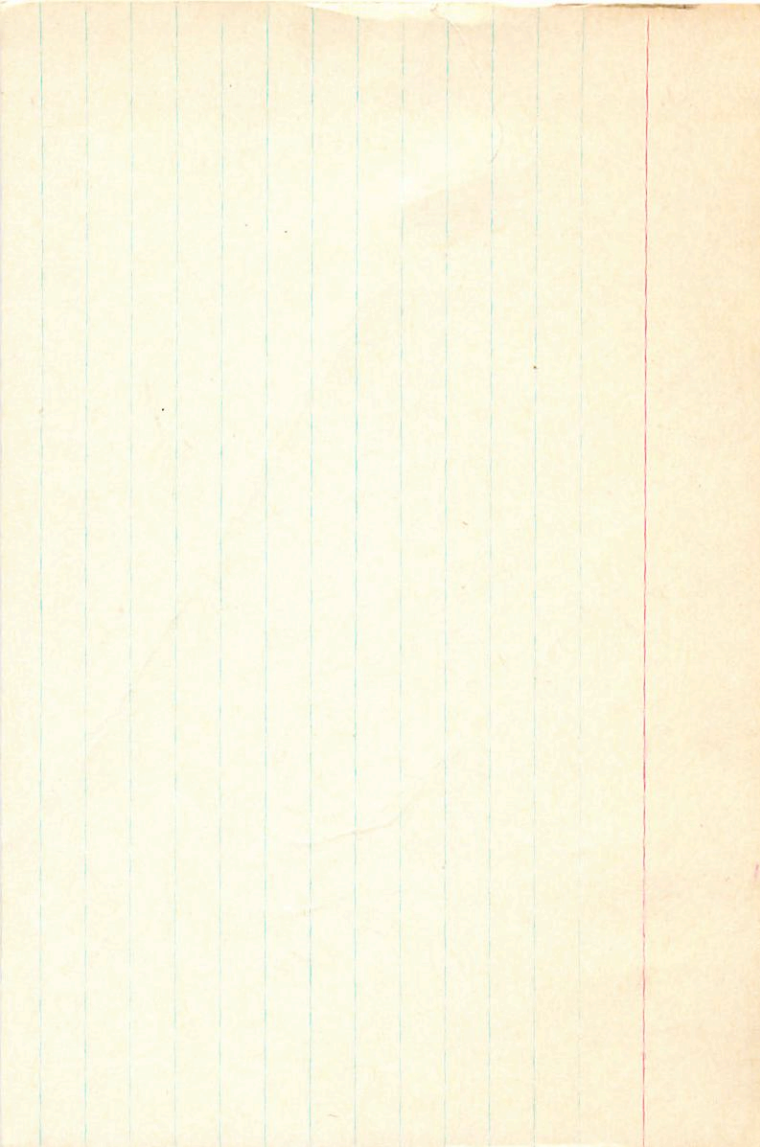
70 250^{ms}

13.2 Orbit

+0.0008	+0.001
-8	+7
+0.0004	+0.0044

→ 1/100 of 1000.04

+670	-194	+715	+0109	+0027	+0146	+3.5	19	-22.9
-653	+301	+694	-0106	-0057	-0163	-4.1	26	-22.2
+352	+933	-074	+0057	-0177	-0120	-3.0	0	+2.4



391) V_{fix}

02

22.7

+25

32

-146 (4)

abs. P⁷ 15⁴ $\frac{1}{1000000}$

+280412

V_V

9.07

+0.56

+0.73 (1)

+0.40 (1)

082

Var Varf

170 -079

24-6

2.4

+288

194

-79

-31.9

2.3

-14

+0.294 -087 ml -AV

51



Year	Month	Day	Time	Location	Notes
1900	Jan	1	10:00
1900	Jan	2	11:00
1900	Jan	3	12:00
1900	Jan	4	13:00
1900	Jan	5	14:00
1900	Jan	6	15:00
1900	Jan	7	16:00
1900	Jan	8	17:00
1900	Jan	9	18:00
1900	Jan	10	19:00
1900	Jan	11	20:00
1900	Jan	12	21:00
1900	Jan	13	22:00
1900	Jan	14	23:00
1900	Jan	15	24:00
1900	Jan	16	25:00
1900	Jan	17	26:00
1900	Jan	18	27:00
1900	Jan	19	28:00
1900	Jan	20	29:00
1900	Jan	21	30:00
1900	Jan	22	31:00

R.A. : 2.400
DEC. : 28.550
R.A. : 194.000
DEC. : -79.000
ANCE : 2.300
ULUS : 29
VEL. : 1.000

(U) : 0.667
2 (U) : 0.154
3 (U) : 0.729
dU : 480.981
U : 14.601

1 (V) : -0.654
2 (V) : 0.590
3 (V) : 0.473
dV : -749.172
V : -21.133

1 (W) : 0.358
2 (W) : 0.793
3 (W) : -0.494
dW : -7.987
W : -0.724

51

ADS 1865

85 (18)

644 (20)

545 (12)

675 (40)

$\Delta m = 0.10$

25.2 4 12 " +1148 +.222 VH

2 22.5 +3 59 1900

8.74 + 1.44 + 1.11 ② $92 + 5.5$

7.74 + 0.67 ⑤

$\frac{782}{724} \approx 73$ $\times 10^6$

Comparison in Ann Rev Arch Bridge 5, 1967 p. 92

25.22 467.63 0.21 +218 -0.65 +451 0.545 74 2540

.04 0.18 0.02 0.10 0.11 0.08 0.11 0.010 1 200

m v w

π 073 $m_{1,m_2} \times 0.65$ +17 +6 +8

067 0.85 +16 +5 +6

440

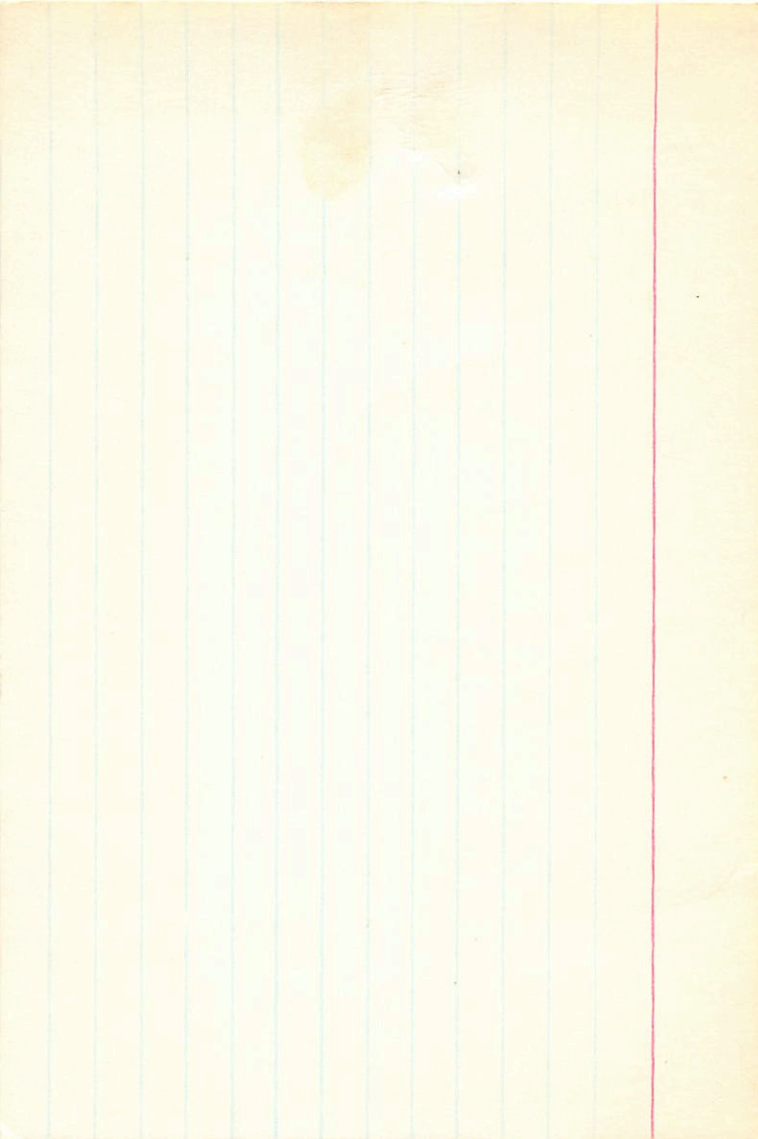
$\frac{6}{7.07}$

$\frac{782}{7.21}$

7.34

64.15

72



15120

7 233

-24 12

302 ①

$-18-37$

$-2-1.8$

-3.7

54





16



D. VEL. : 0.000
 MODULUS : 0.000
 ISTANCE : 0.000
 M. DEC. : -37.000
 M. R.A. : -21.000
 DEC. : -24.000
 R.A. : 2.400

U : -172.820
 UB : -180.920
 P3 (U) : 0.010
 P2 (U) : 0.074
 P1 (U) : 0.007

U : -94.000
 UB : -97.100
 P3 (V) : -0.100
 P2 (V) : 0.704
 P1 (V) : -0.024

W : -40.000
 WB : -40.000
 P3 (W) : -0.000
 P2 (W) : 0.000
 P1 (W) : 0.000

21

R.A. : 2.400
DEC. : -24.200
PM. R.A. : -21.800
PM. DEC. : -37.000
DISTANCE : 9.900
MODULUS : 955
RAD. VEL. : 0.000

q1 (U) : 0.667
q2 (U) : 0.674
q3 (U) : 0.319
dU : -180.965
U : -172.820

q1 (V) : -0.654
q2 (V) : 0.734
q3 (V) : -0.183
dV : -67.103
V : -64.083

q1 (W) : 0.358
q2 (W) : 0.087
q3 (W) : -0.930
dW : -48.896
W : -46.695

16

15165 / PN 2 241 +10 20

A 6.7 42

+3774 del ① +321 2875

B 8.3

+28 ② +2889

+081 -0304

8.71 184 115 825 2.706 +103

-5 +6

+34

8.33 143 165 656 2734

+0029 0.15

+205

+60286 -0076 2-0

+058 -003 4003

+00291 -0070 -0c

+00281 -0055 →

+0415

+042-008

3.06

+0025 324 -012 ± 2.3

4487

1792.0

28.82 18587

21

Check



1851

[Faint handwritten notes]

1852

[Faint handwritten mark]

1853

[Faint handwritten mark]

[Large handwritten mark, possibly 'X']

1854

[Faint handwritten mark]

59
5135

6.05
163.5

2.400
10.300
43.000
-8.000
6.000
150
34.000

5.6
4 131.8

0.667
0.373
0.645
119.503
40.871

+41

37.7

-0.654
0.708
0.266
-157.965
-15.996

-16.8

-11.7

0.350
0.599
-0.716
40.968
-16.597

17

-16

-19

1564/5^g

2 241 +10 20

+340

VW PM

+0286 -0076 ZL

~~+~~ +

+0091 -0069

+00281 -0054

+0915

[+073-009]

Am 7 862

M 0439

~~9508~~

8608 9547

8050 0259

2.4

+10.33

+44

-9
6.35

+34.0

+10223 -009

+00229 -0076

0335

[0350 -011]

460

443 + 12 = 4

453 - 2 = 0

+ 10025 324

- 112533

- 2016
- 010

4481 970 + 10022

0223

28.32

13.7

$\frac{-132}{349}$

$\frac{68}{2900}$

4482 - 59.23

457

28.21

$\frac{-11}{28.10}$

4442 - 39.26

457

28.42

$\frac{+8}{28.50}$

~~scribble~~

15/11

2 241 + 25 49 - 34.9 Net

6157 + 58 709

2010 - 034 *handing*
- 014 - 034

75
- 39

20
34.9

18



R.A.	2.400
DEC.	25.600
R.A.	-15.000
DEC.	-39.000
ANCE	2.000
	25
	-34.900

+0014 ± 63 -040 ± 54
+0014 -042
+16 25 7.3 FO

15227 2 24.8

1387

2949 46.478 1901.6 +16 25 13.24 1899.6

$$\frac{-068}{410}$$

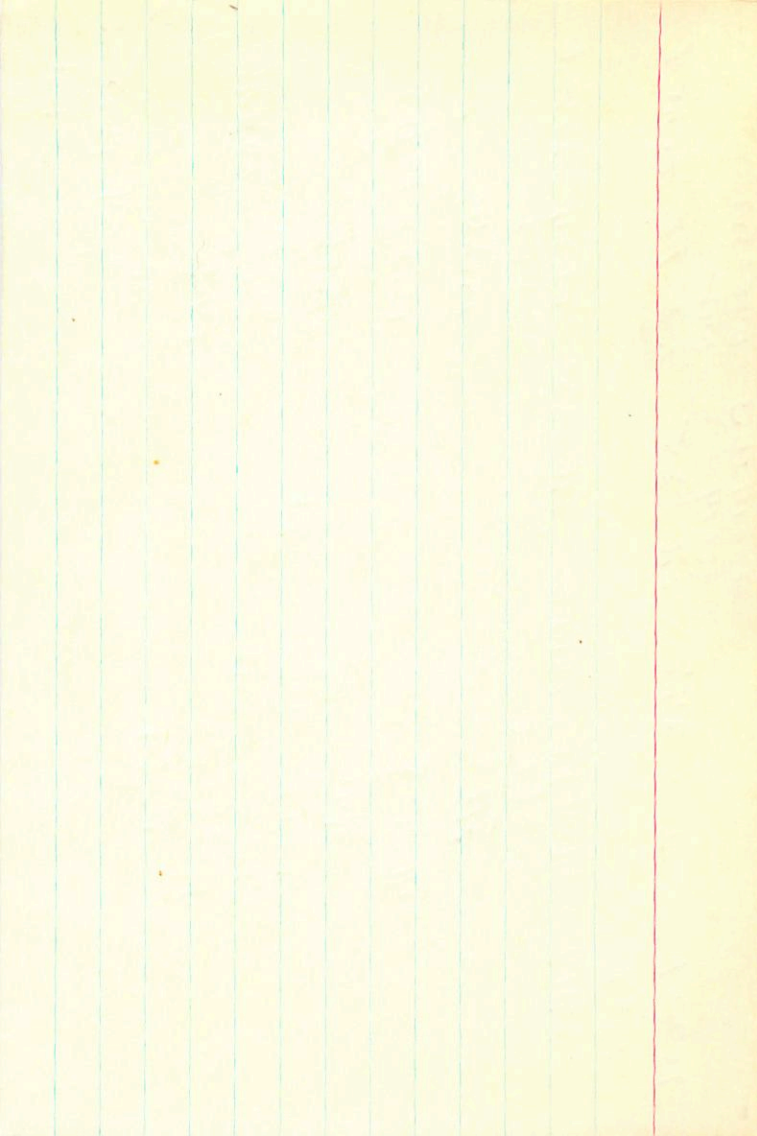
$$\frac{46.438}{446}$$

$$\frac{23.847}{22.542} + \frac{450}{040}$$
$$\frac{46.052}{1442}$$
$$\frac{1412}{454}$$

(29.1)

$$13.77 + 4 \quad 1934.9$$
$$\frac{13.86}{22}$$

$$\frac{28.52}{46.15} \quad 192726$$
$$\frac{14170}{-90} \quad 30.7$$
$$\frac{13122}{1404} \quad (31.1)$$
$$\frac{1395}{131}$$



15138

2 24.5 + 50 21

HR709

GC2544

66And

1278 147.476 ② SPC 2.640 ④ C+

6.82
7.87

96
KCT 651

[M]

420
~~6.82~~
6.82
7.87
+3.2

[N]

694 -131 735

-84 372 659

361 915 -1100

1070 +0540 +1610

-1054 -1534 -2588

0582 3350 4938

-2.9

2.6

+0.6

638

-yd SEC(150)

+0034

-084

W50

+0038

-037

CV ~~7~~

+0036

-087

+034-087

6 Cas

2 24.9 +67 11

Van 41.9 (10)
45p +1.2 T

4.53 +0.13

-013 +016 N30

-013 +016 60
023

7^m Bnd at
also 8.7 7^m

591 806 922 388 -0.13 +0.6 +1.2 -0.15 +1.1025

008 -009 -010 012 -019 -020 +0.7 +0.6 +0.4 0.25

$$-0.2 -3.2 + 2.2$$

$$\boxed{-1.8 + 3.0 + 1.7}$$

$$-1 -4 + 2 \quad 0.28$$

$$-0.4 -3.7 + 2.4 \quad 0.22$$

$$\boxed{+2.2 + 3.3 + 2.1}$$

$+0002 \neq 113$ $+006 \pm 9.0$
 $+0018$ $+010$
 H015339 2 24.9 246 13 -1.6 \pm 0.5 C_2 (14)

2950

2.14 + 1.11 100 III

+020 + 008 Capap
 +002 + 006 GC

52.551 1901.4 -46 13 26.13 -31 1898.8

26.44

39.1

54.370
 56.252
 52.610
 6.12
 130
 5.92

10.99

1926.95

8096

25.49

26.03

41.7

613

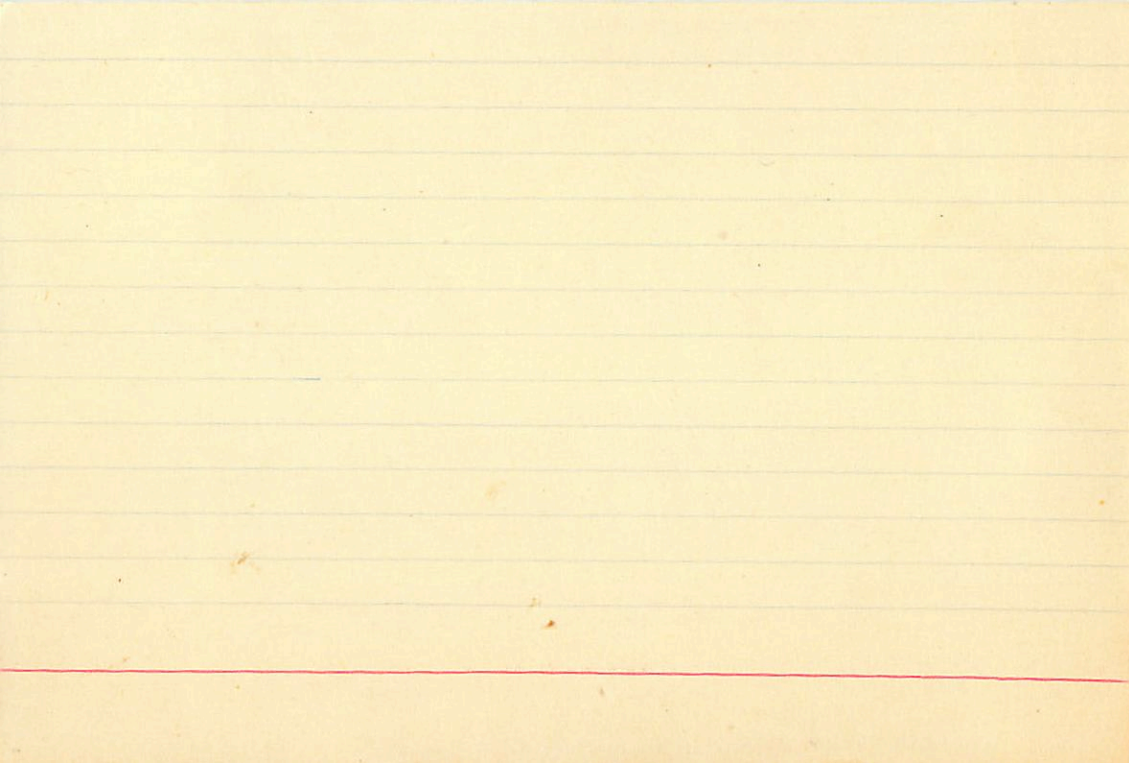
+41

52.685
 -40
 645

25.98

1954.07

26.07



PRR

2 25.1 + 51 03 7.52 gML e

+500557

+9C 24

HD 15180

~~W-20224~~

722

2 247 16 43

MS IV + 2

(27)

1240 ✓

~~11-88~~

25 Ari

2 24.7 +09 59 dF4 -40.86W(4)

48.2 74

15228

6.49 +0.46 -0.08 RFS

GC2946

S = .09

W1386

+5 +7

-40 (6)
-38.5 (11)

4 498

-01981 1945 20

+40323

-01976 1991

-01983 1978

± 2 ± 2
-288 -201 GC
-293 -200 Z
-290 -200

-2929

-89 -1 -26 .020

-292-201

-77 -7 -17 .025

4453
-7842 } 3537
-6206 } 0286
-0362 } 1.2
0.98 2 0.1

23M(8)
19M(7)

21 ± 8

550 907 174 985 -290 -200 -40.5

-035 -7 -933, 171 021 -234 -028 943 -1009 -40.2 -32 -24

+9-69-48

0225

[-93 -1 -15]

+6-64-44

.025

[-76 -1 -16]

0

REI

2 25.2 -47 56 +2838

HR721

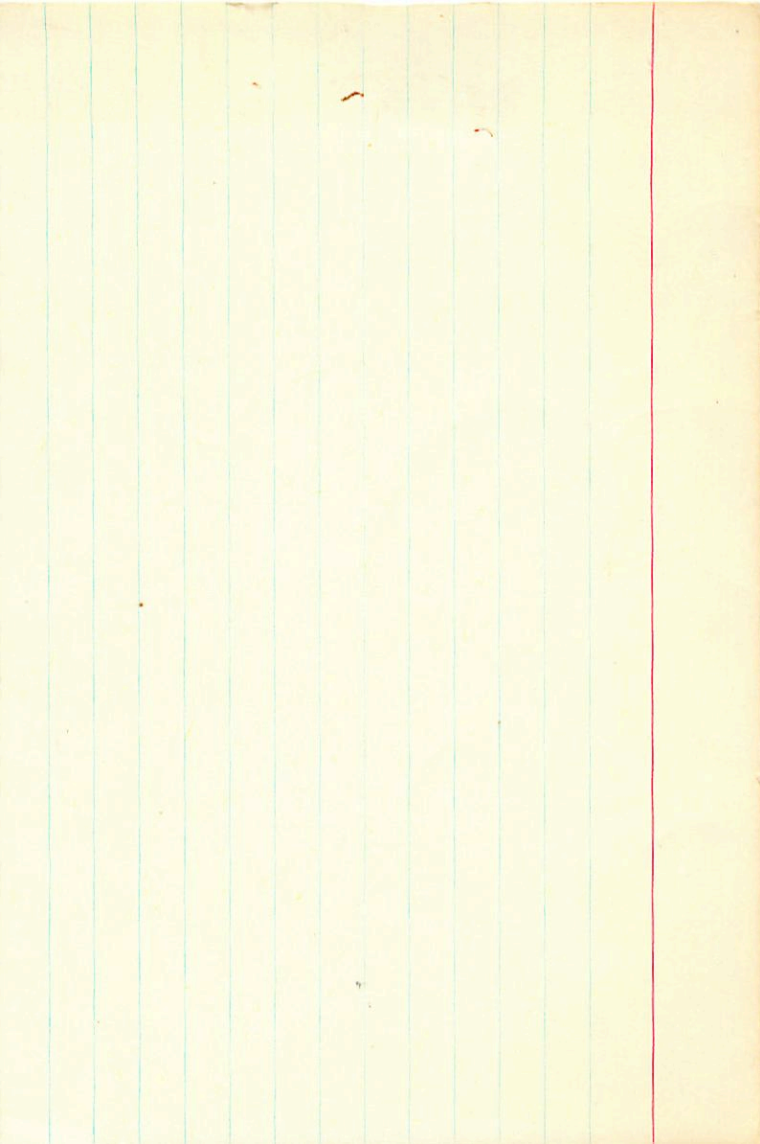
4.22 -0.13 -0.43 BF $\overline{101}$

+029 -004/01

+028 -003/030

+024 -013/123

+023 -009



of 200

724 2 25.9 - 34.63

15427
2967

5.10 +10 - C
(+13)

Sta ?

New?

6.13 033 150 1016 2912 13,84,60
360
137
142

+1010 +012
+ 3 +1
1013 1013
1016

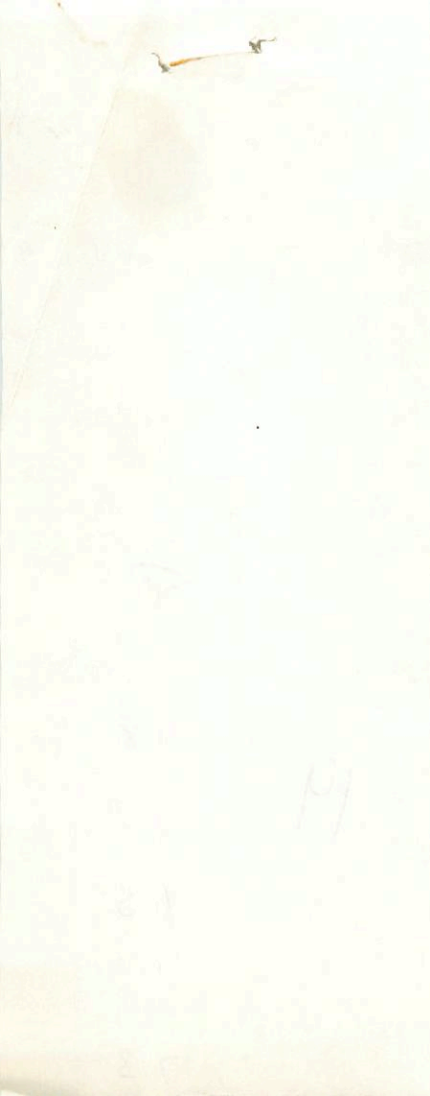
+25 VarSta
+16 Var? 186 372
1609
1.381
1.441
081

288
a = +1088 ✓

a = +1000 ✓
+1.775

3.480

19



724. 000 *

2. 000 *

25. 900 *

-34. 000 *

-3. 000 *

0. 016 *

0. 013 *

3. 500 *

50. 119

100. 000

20

0. 095

0. 204

8. 804

-0. 007

-0. 910

-6. 529

0. 023

-0. 928

372

-17. 394

19

+00322 ± 17.0
-089 ± 12.2
-074
41)

+0030
+45 49

2 26.5

15365
2978
1404

6.8 + 34.08

445 48 3775 15067

30.594 1907.5

-136

458

3.85
41.60

20.9

53.33
37.050
30.312
5.227
5.15

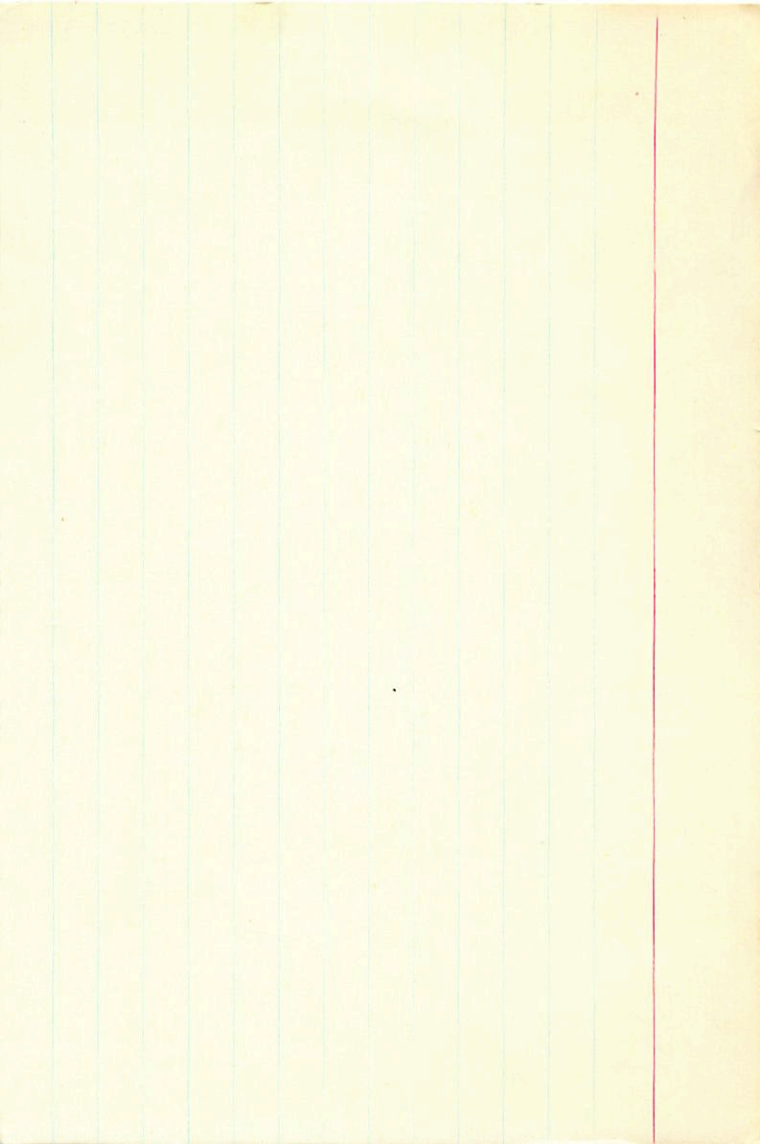
520
7062

54.5 1926.9
94.28
40.78
1.07

39.31
40.02
40.1 1929.8 (21.7)

30.526
526

-14
39.96



+0262 ±9.0 +029 ±8.3
+0257 +045

1555 2 27.3 -24 20 7.5 110 +28.97

1408

2992 17.138 1400.1 -24 19 36.46 1898.5

Answers +0260 +038

358 036

37.95

91
246

526
1826
388
2114
3

8.875
7.782
16.657

694
+20
674
35

16.647
+15
17.2

9093
9161

9391
3436

78.40 1433.68

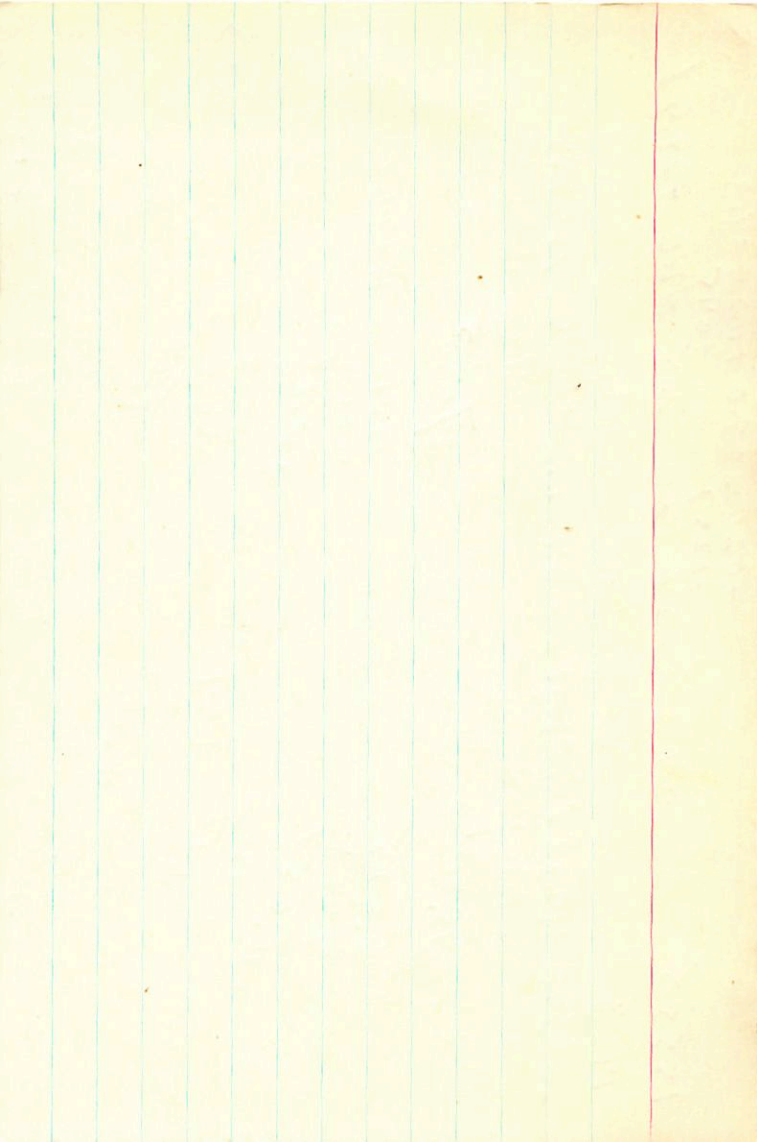
42.62
35.78
-72

33.7
35.2

36.53
36.14
3

36.64 1933.78
36.27

36.36
1.59



$+0056 \pm 9.5$
 $+1032$
 -060
 40
 15464 2 27.3 +33 37 6.2 141 III +7.44

2991

1407

15.664 1907.9 +33 36 46.53 1907.4

$$\begin{array}{r} -234 \\ \hline 42 \end{array}$$

$$\begin{array}{r} 2.43 \\ \hline 48.96 \end{array}$$

202

$$\begin{array}{r} 45.44 \\ 29.955 \\ \hline 15.485 \\ 50.12 \\ \hline 15.12 \\ 4 \end{array}$$

$$\begin{array}{r} 4.92 \\ \hline 404 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 19263 \end{array}$$

$$\begin{array}{r} 43.15 \\ \hline 48.18 \end{array}$$

$$\begin{array}{r} 47.17 \\ \hline 47.22 \\ \hline 47.17 \end{array}$$

$$\begin{array}{r} 2 \\ \hline 281 \end{array}$$

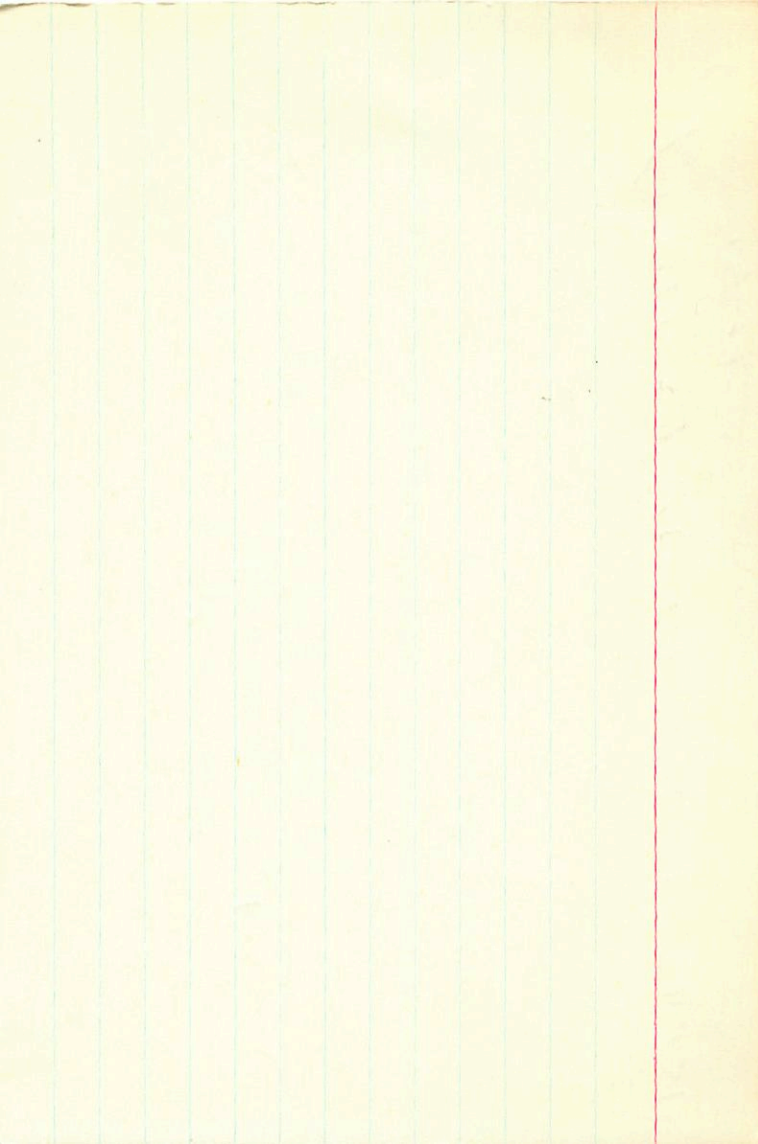
20.7

$$\begin{array}{r} 15.46 \\ \hline 49 \end{array}$$

$$\begin{array}{r} 47.1 \\ \hline 47.3 \end{array}$$

1929.9

$$\begin{array}{r} 47.19 \\ \hline 47.19 \end{array}$$



836 2 27.6 -2254 Quadrant +13.0 (4) C5
 15851 # 82 m 11 +0056 -0025 9057 9426
 600209 4204 3334

6.76 +0.19 (1.60) A5E

+0054±39 +010±32
 +0053 -005

38.309 1904.9
 2.11
 805

17.29 1901.0

+0053 +002
 0
 0

38.261

18.06 1938.55

240
 230
 240

+3
 1803 224

29.842
 8.350
 38.200

59.53 1933.64

+0052
 0
 0

20
 20
 20

42.18
 1736 361

18.162

HD 15588

2 27.6 -22 54.

+13.04C

CC 3000

q20

6.70 + 0.19 (1.60)

+0054 ± 39
0058

+010 ± 32
00

+13.2 144
-12.0 -23
+7.2 -120

38.309 1904.9
244
065

17.29 1906.0
-50
77.79

+0056 +003

38.261
-1
38.260

18.06 1938.55
26
17.80

+176
-143

29 848 | 658 670 342
28.352 | -655 733 -176
38.200 | 369 108 -922
20
220

+2410 +0095
-2400 +0104
+1352 +over
+ 47.80

+2505 -25
-2246
+1867

+4.4
-2.3
-12.0

17.93
20
17.53

36

44
382

15524

2 27.7 +25 01

RF4

(HR728)

30016C

85000

NO.4 +16
-11

52

[m] 206 +14

.264 1158

559 (4) SPC 2.6748

[C.2] 505 +84
98

275

GC #2.0

+100465 -0785
2827 -0745
6435

+2.6 (8.15)

1063 1064-080

" +060
-077

658 194 727

1871-0708

1163

-7.8

-655 622 426

-1863-2270

-4133

-76

369 758 -537

1044-2766

-1717

+5.8

-10.86

-1086

906

$+0046$
 $+0046 \pm 2.3$
 -075
 -078 ± 1.6
 $+0045$
 $5-2-25$
 1858.8

$\frac{215}{176}$

$+0045 - 074$
 $-1 + 2$

$\frac{3.59}{56.24}$

39.487

$\frac{+0044 - 077}{6.521}$

51.83

1960.53

$\frac{5}{432}$

2947

5143

$\frac{-16}{51.37}$

+256

$\frac{46}{46}$

$\frac{-14}{51.2}$

$\frac{-4.87}{51.37}$

20

195

180

170

160

150

140

130

120

110

100

90

80

70

60

50

40

30

20

10

0

723.000*

2.000*

27.700*

25.000*

1.000*

0.064*

-3.000*

3.150*

42.650

-10.000

4754

0.126

0.728

-1.8

-2.491

20

-0.435

0.427

25.4

-23.160

-0.175

-0.536

-26

-1.674

1544g
3002
200g
202 257 85 15

1544g
3002
200g
202 257 85 15

1544g
3002
200g
202 257 85 15

1544g
3002
200g
202 257 85 15

1544g
3002
200g
202 257 85 15

2015

15579

2 28.6 +46 22 f=2 +23.28

7.1

+083 -020 0

83
581
29
57

37.084

-330
36.754

37.092

18
.110
+356

19092 +083

+082 -024
+1 +1

+087

+0081 ± 12.2 -020 ± 9.5
-027

55.38

87
56.25

55.15

-12

55.03

19067

1952.15

604 757 724 680 +083-020 +23.2-014 +17 -066 ✓

-050 008 066-011 -155 351 +16.0 +13 +10

-5 +45 +10 01

$\boxed{+45 - 14 + 2}$

+1 +33 +13

015

$\boxed{+35 - 40}$

02

+4 +28 +14

+32 +10

27.3 49 49

15801 2 28.4 -49 36 +162.9 15k.

-490699

"-030 -064 CA"

40 A0

9.5

↓

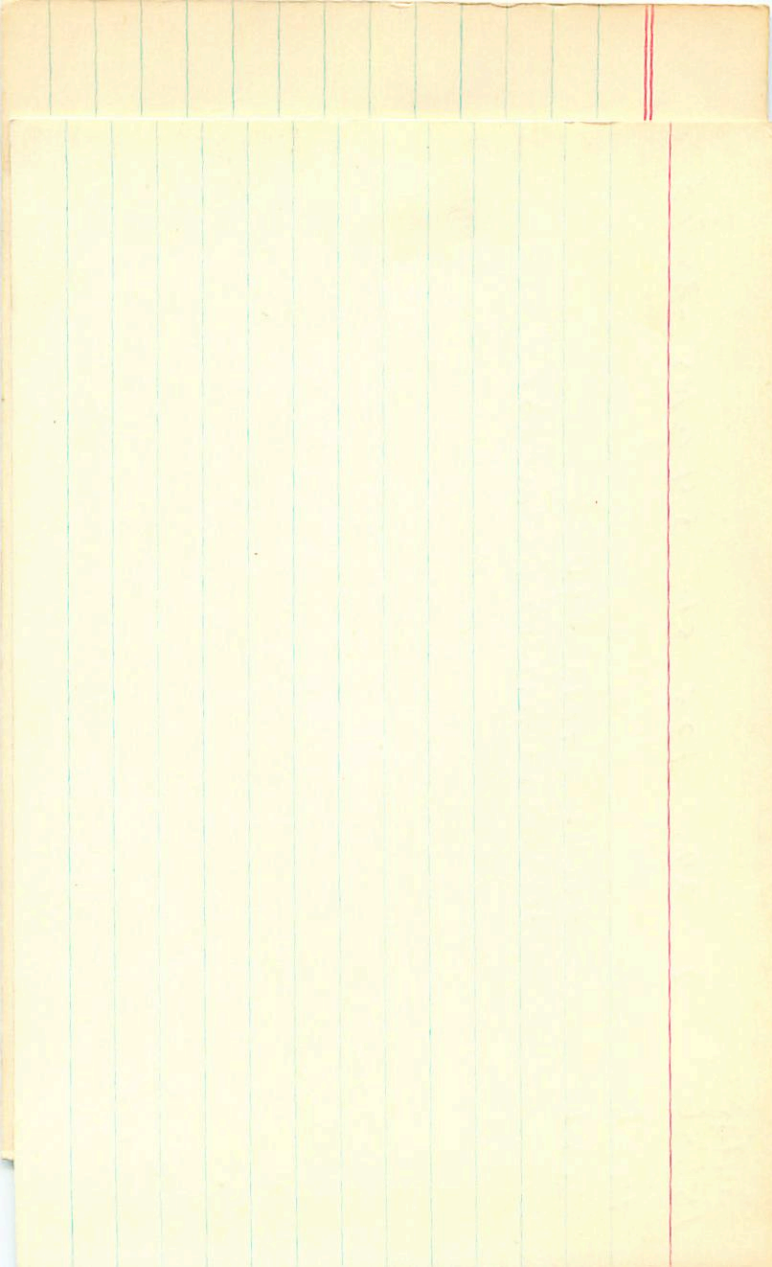
p. Kennedy

for

14
150

14
30

*



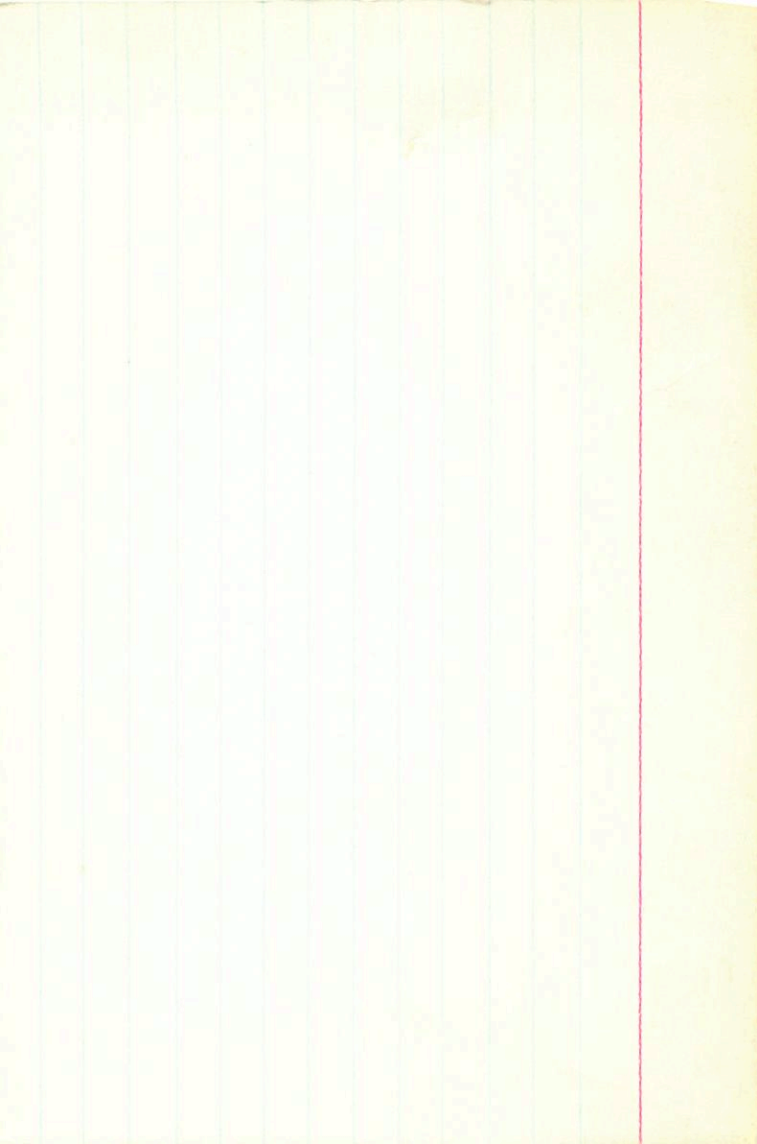
HTB 229.9 +34 19 -2.2

-067 -012 66

0 +1

-067 -011

652 074 755 -2071
-657 552 5B
379 831 -404



420550

3W

15830 2 30.9 442 34 7.6 d64 +15.76

CC172

1443

D 752 (4)

7.42 -1.14 cm

10874 -42 Scrubbing

413 -142

8884	9535	47516
4550	3013	0817

30.0 4945

25.6 4900

28.6 0817

1.26

25

more

10/11

10/11

(11)

0.000
0.000
0.000
0.000
0.000
0.000

AD. VE.
MODULES :
DISTANCE :
PM. DEE.
PM. R.A.
DEC.

0.000
0.000
0.000
0.000
0.000

IP
SP
SP
IP
U

0.000
0.000
0.000
0.000

IP
SP
SP
U

R.A. :	2.500
DEC. :	42.550
PM. R.A. :	0.000
PM. DEC. :	0.000
DISTANCE :	0.000
MODULUS :	0.000
AD. VEL. :	10
	0.000

q1 (U) :	0.652
q2 (U) :	-0.039
q3 (U) :	0.758
dU :	0.000
U :	0.000

q1 (V) :	-0.657
q2 (V) :	0.470
q3 (V) :	0.590
dV :	0.000
V :	0.000

21

10076

-32.907

2 31 5.06

-31 56

22.9

-1006 -101

-21.1028

2 32 10.9

-30 47

008.9

-0171 -105

2.82

3.29

4.41

5.12

8.58

5.04

1.87

5.42

8.20

0.303

10.8

3.02

2.20

3.70

2.026

7.41

9.67

1.0

F_{20/k} - 0.22

256 / 020

~~MV 5.76~~

147m

15656

2 29.0 +35 56 5.49 125 -35.98

1427

49

-3827

3032

+0042 +013 N30

+00382.2 +01731.7 6-26m 5 N30

RR 93p

