

+37.30242

13

11.4

+37 06

44

13 15 45.8 +36 35.99

0.350 196

-0.83 -2.88

+23: 2400

MLL-AL +08: -32:

-103

196

1.05

+23

10.5 012

69

M : 58.333
 QM : -102.682
 d3 (M) : 0.283
 d5 (M) : -0.122
 d1 (M) : -0.100

8

^ : 12.025
 qn : 204.323
 d3 (N) : 0.182
 d5 (N) : 0.220
 d1 (N) : 0.282

N : 18.608
 qn : 842.427
 d3 (N) : 0.015
 d5 (N) : -0.302
 d1 (N) : :

RAD. NET : 53.000
 51
 DIWAPNCE : 1.220
 BM. DEC : 129.000
 BM. R.A. : -103.000
 DEC : 39.400
 R.A. : 13.520

R.A. : 13.250
DEC. : 36.600
PM. R.A. : -103.000
PM. DEC. : 196.000
DISTANCE : 1.650
MODULUS : 21
RAD. VEL. : 23.000

q1 (U) :
q2 (U) : -0.805
q3 (U) : 0.593
dU : 0.012
U : 866.667
U : 18.808

q1 (V) :
q2 (V) : 0.585
q3 (V) : 0.790
dV : 0.186
V : 504.393
V : 15.052

q1 (W) :
q2 (W) : -0.100
q3 (W) : -0.156
dW : 0.983
W : -105.985
W : 20.333



7915

13

16.8

+85

01

dF7

+11.3

18022

FMS system

-139.9 + 17.9

7.28

$\frac{41.0}{3}$

+0.1

2 E

-1133 - 096

-1018 ± 1.7

-1253

46.512

$\frac{5.02}{51.512}$

+85

5.18

59.40

0

54.22

1896.0

9956

0589

-9734

1403

2293

9147

53.50

18

53.68

45.578

$\frac{41}{41}$

46.023

-489

→ 51

-5.72

+35.2436

Y3047

A058861 A0

9 } 17.5" binary
10 }

126 M(4)
45 K(6)
116 S(7)

Yerkes-Sproul meas.
Middel - McCombs
rel. parallax is mean for
2 components.

W7918

BV18029

Cam 18-1719

+383 -797

364 ~ 798 AGR3

1896.51 12.0 17.30 3A

81

13 12.8 +35.57⁴⁰

+35

13 17.2 19.6

+35 24.05 -9.5

-7.9

-2.9 of 3W

DMI

A 9.52 +1.47 +1.18 (3)

8.41 +0.815 (2)

B 12.09 +1.59 +1.08 (3)

10.50 +1.05 (2)

9.5 MR2

+0.391 = 0.770

+0.311804

383 - 797

-7.0

6e
mud
↓

416

70

ANSWER 17"

18029 13 17.2

7918

$+0331 \pm 6.0$
 $+0310$
 $+03735$ 23 9.8 dmi - 2.98
 -756
 -790 ± 5.5
 -792

14.165 1599.3 +35 22 58.75 1896.6

-1.678
 $\hline 12.487$

42.19
 $\hline 40.94$

4.36
 9.050
 $\hline 13.418$
 9.8
 $\hline 3.618$
 3

70.0
 53.78
 $\hline 16.22$
 16.43
 $\hline 16.6$
 16.6
 $\hline 16.6$

25.4

580
 $\hline 2.55$
 $\hline 2.55$
 788

4.22
 9.0568
 $\hline 13.2788$
 12.6
 $\hline 0.6788$

19.325
 $\hline 16.4$
 2.925

52.42
 -33
 $\hline 19.02$

58.24

16.8
 15.4
 $\hline 16.6$
 16.6
 $\hline 16.6$

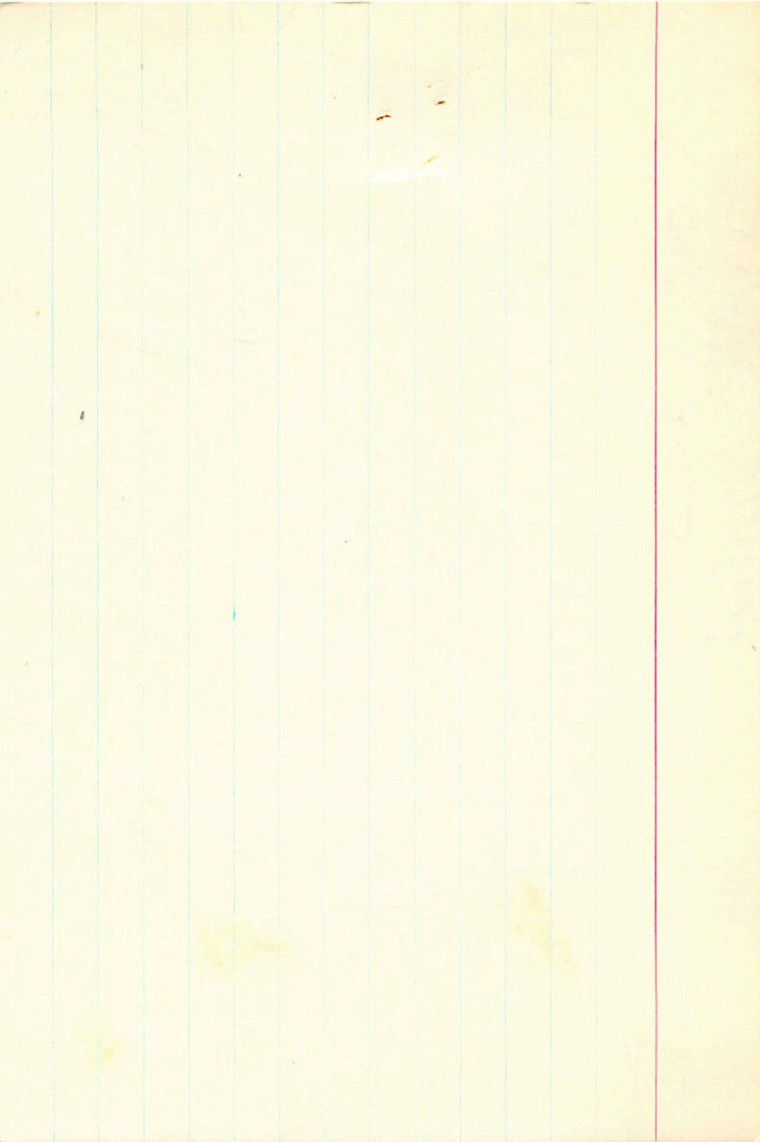
94
 247
 $\hline 28.1$

13.2788
 12.6
 $\hline 0.6788$

58.88
 $\hline 16.6$
 42.28

16.4
 19.24
 $\hline 35.64$

19.02
 1.12
 $\hline 20.14$



48.2108

13

13.5

+48

33

142

AD58862 $P=50\%$
 $13m=0.5$

¹³
13

^{15.5}
17.65.8

⁺⁴⁸
+48

¹⁸
3.08

(4.5)

W7920 H0115953

43048.1

Boiz, 5032, 52

82M(8)

1.0 100W

+130.2W

dm2

69

+140 -26 AC113

2nd km 25

+141 -0.15

⁵³
-20

8.7112+94

+168 -0.12

+143

MR

155

-12

+8.0

P24885

a=1.465

B=0.5

+0.156 -0.018

+140 -2

826
789
110
98
6
710
22



71





142.000*

10.000*

+29°.2405

W 509 13 16.8
13 18.9
13 21.3 15.4

8.90 13.3
8.75 13.6
+2.9 5
+2.9 2
+2.9 2

38.7 (16) Wagon

W 7953 AB: 7.5, 9.7 binary (4.0) -38.7

ADS 8887, d=0.7, A.M. = 0.2
(3M/7)

G-C 18119

HD 11495

Y 3061

Ci 18.1730 -0.476 +0.244

-0.454 +0.2

9.5
6.5
7.3
2A
5A

234

* Spectrum is comparable. M. lib. observed
give MO for brighter + K6 for fainter comp.

1887.36	299	0.62	2 HD	1918	30	0.65	3 VB
1894.88	312	0.64	5 HD	1920	48	0.66	8 VB
1896.46	315	0.80	3 A	1945.33	48	0.77	3 B
1900.35	321	0.74	8 Doo	1956.99			
1905			3 A	1956.27			

-0.611
0.124

4.585

1
58

27

+502767

13 270
13 29 4
31.8475

3094.1 (18)
53 M (18)

set

77.0 ± 1.5

Way 1487

+1.13

-1.16

net

+0.144

+0.141

-0.117

-5
+5

2336 (22) (20)
2336 (22) (20)

0.143
+0.136
-0.1184

99.1 @ 100

9.97 ± 1.38 +121 ①

9.06 ± 0.68 ③

436-125 / +50

19.055
~~22.000~~

387

FB

48.000*

13.000*

31.800*

4.000*

56.000*

0.136*

-0.125*

1.150*

16.982

9.000

-0.807

-0.359

-16.938

-0.063

-0.213

-2.979

-0.333

0.909

2.515

73

-3169

-65

-342 ± 11

-66 ± 5

CR

-32055 121

-7068

-33887

65574

CR

-3435 105

-6108

-33728

65602

Y

-345 ± 12

-66 ± 2

Y

-351

-678

361

355

21/9

330

-327

-063

CR

33513548

-9288

9627

-063

-327

4588

-3705

9627

-063

-327

4588

-3705

9627

-063

-327

9627

-327

116558 13 23.9 -24 02 divo -10.8 (w/13)

-23011071 V65794 8.9 8.78 +925 +2.07 2 24'' 18 -5.0

W79669 2nd floor A 8.9 8.72 +915 +2.05 2 24'' -dl

Y3067 344 B 8.72 +915 8 -30 -06

(-23011076 13ⁿ 24.0 -24.0 02ⁿ A -374 512 -050.524

Y3068 8.540 M2 -346.512 -066.512 -345 12 -066.512 M

(H0116420) 71 = 5112 C (1) -351 -078

9549 -1.000 358 0388
-288B -0887 +10 2467

+30 -15 -9 .054
+37 -24 +2 .044

54513 C (1) (Amplitude)

355-0644 H grade

-340-643

5.1
16.2
54.2
9.85
7.54
7.54
7.54
7.54

PL512

13 25.8

-2 06

-424

9"

2.4

11.30 1.57

173-450

~~13.75~~ 1.70

10.05 1.12

13.4

12.21 1.34

-2.1

173

-450

0.0

9776

7688

-426

-2106

6355

74

5M0-01 -01071 +0371 P1K5 -0106 +037 A1
5085 13 26.6 +6.0 13

9894-9515
-0359 2405

117376

18226

0180
-0078
-4.0

1
15
20

000 164
002 158
001 161

1019
1.027
1.023

2.894
2.913
2.906

5.40-01-03 2.594

2.894 - total

5.19

168
322

-001 = 4
015 = 2

-100.6
87.1
44.0

1023
1343
1347

-001 = 4
015 = 2

-0798 +0371

11
44.0

+1.2
4.2

9956 - 9403
3403 - 0000

13.4
+10.2
-16.5

607
0744
0877
0880

9956 - 9403
3403 - 0000

-01124
+0371
+9

-0744
-082 +033

13.4
+10.2
-16.5

607
0744
0877
0880

9956 - 9403
3403 - 0000

-01124
+0371
+9

-0744
-082 +033

13.4
+10.2
-16.5

607
0744
0877
0880

9956 - 9403
3403 - 0000

-01124
+0371
+9

-0744
-082 +033

13.4
+10.2
-16.5

607
0744
0877
0880

9956 - 9403
3403 - 0000

75

+133

+1102576

13 27.5 +10 39

+172

W8008

+19W(7)

+12M(12)

9.02 +1.49 - Mum

M 3079

9.04 +1.91 +1.26 MIV M+5

R000490

9.09 +1.54 - Egg (1.2") +1.02 -1.09 km

+1.120 -1.080 Tst.

L004

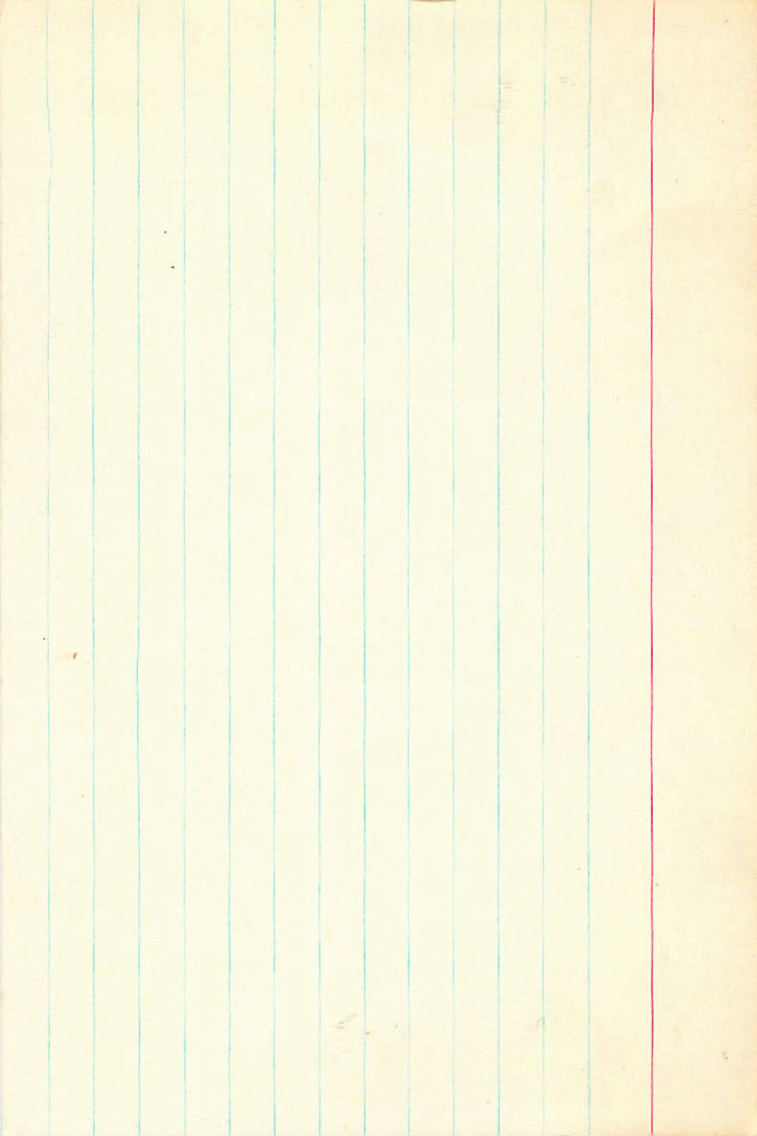
-56 -10 -2 .121

+1.177

MCR

-72 -11 -10 .100

.121 ± (1 ml)



2nd

+750510 13 319 +75 16 10.4 dx5-35c

8038

+750510 -418 +039 GP
-421.5 +046.6 GR

+750511 -427 -013 GP
-428.2 -046.1 GR

+0.3077

12 28.0 +0 19

42

30.4 +0 3

32.9 51.9

-0 12.42

N

13

+0.029 4182

SA105

+10 Dupon

844

803

6045

MCC-AC +018 +191

9.7 MD

+0.018 +0.191

10.26 +1.45 +1.02 (1)

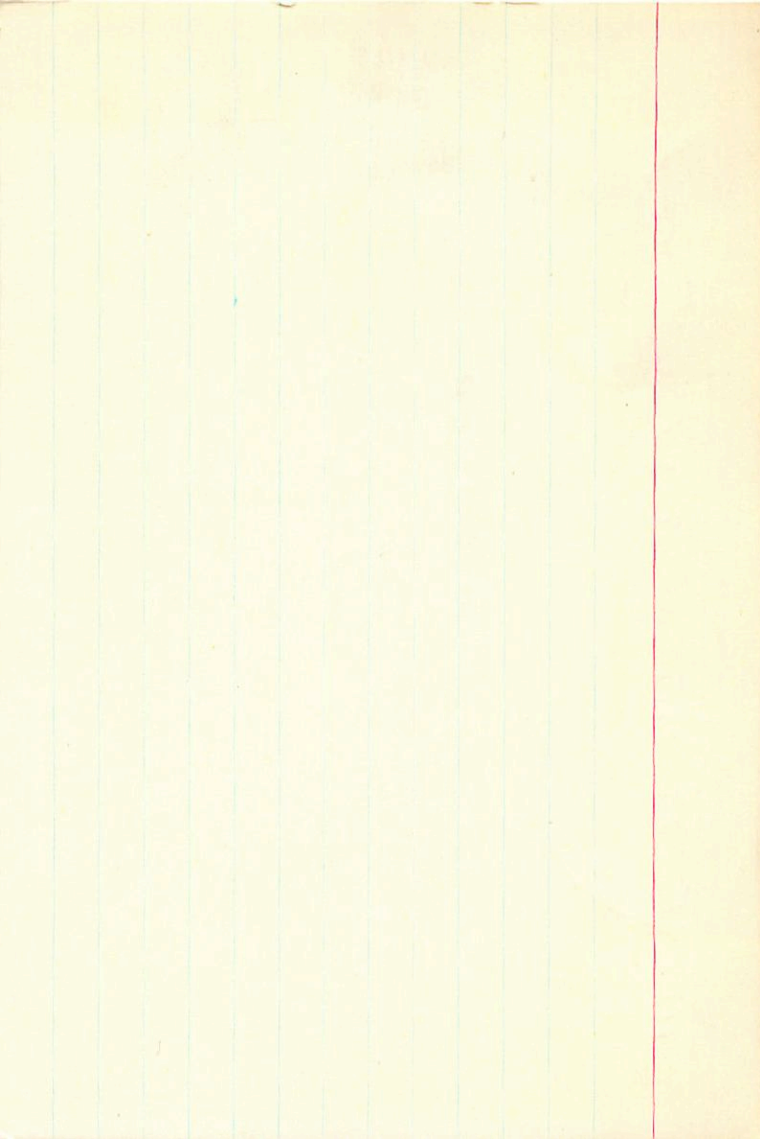
9.32 +0.68 (2)

$C_3(5)$

118258 13 33.7 -55 54 6-60 -390 to 8
7.97+85-1.85

~~10.83'~~
10.83'

S	-0.107	-0.020	-0.559	±7 CP
	-2		-1	
	<u>-0.109</u>		-0.00	
	+13		+11	
	<u>-0.096</u>		<u>-0.49</u>	
				-0.81



721

 $13^{\text{h}} 33^{\text{m}} .7$ $-55^{\circ} 54'$

HD 118258

+7.97

+0.85

+1.85

G6V

- .774	- .067	- .629
+ .609	+ .191	- .770
- .172	+ .979	+ 1.07

13 358 +48 23
+48.848

617-46 AD-AD5850 6 m=10 2.5
6-77-45 6 2m-44-9
DE 2 py

9102 883 0205 ✓
9102 883 0205

11-11
149 149 129 129 (2) 421 33.21 27.1 5441

211-1111-

4111-4589
4111-4589
4111-4589

+46° 1889

13 33.4

+45 56

305

13 37 23.3

+45 27.11

-0.43 + 409 ALR3

-65.2 (19)
-65.2 (21)

M0

E.B. Ser. -0.04 +0.39

10.5 M2 +11.1

-57

+390

50

171

76

13,200 : A

~~5,400~~ : C

1,200 : A

3,200 : C

1,000 : CE

10 : US

1,100 : L

1,700 : U

1,300 : U

1,000 : U

1,310 : BU

1,300 : U

1,000 : U

1,700 : U

1,300 : U

1,140 : VE

1,100 : U

Handwritten initials

1,100 : U

1,100 : U

1,300 : U

1,440 : WE

1,100 : W

A. : 13.600
C. : 46.450
A. : -57.000
C. : 390.000
CE : 0.000
US : 10
L. : -67.100

U) : -0.770
U) : 0.635
U) : 0.064
dU : 1316.820
U : 8.893

V) : 0.612
V) : 0.706
V) : 0.356
dV : 1192.145
V : -11.948

W) : -0.181
W) : -0.313
W) : 0.932
dW : -544.792
W : -68.013

76

13 35.7 +35 558.7 M2
(32)

9.14 8.18 +0.64 26 June 460"
8.95 8.04 +0.65 July 460"

9.08 +1.40 +1.15 29 June 460"
9.07 +1.40 +1.14 30 " "

9.05 +1.40 +1.18 31 March 60"

9.07 +1.40 1.14 ③

221-311

6-51-12

15-031

151

611-05-

91112

111-112-

-3.3508
 13
 13
 32.6
 38.0
 37.53
 -3
 -3
 28
 42
 56.91
 146
 49.0

HD 118926

205211 JWG
 Jul

$94M(18)$
 $94M(17)$
 $42/45$

376.100
 3929.400
 24
 23

22326
 22326

$C20-794 -0.36 +.46$

835
 76

$9.740 + 7.7$

-0.348 MR

$-345 + 445$

$+220$
 125

$-0.343 + 0.484 C$

$-0.345 + 0.480$
 $-350 + 500 (62)$

72



AND OF

THE

STATE

OF

NEW

JERSEY

IN

THE

YEAR

1880

BY

THE

LEGISLATURE

OF

THE

STATE

OF

NEW

JERSEY

IN

THE

YEAR

1880

BY

THE

~~XX~~

27/10/80

1880

146,000*

13,000*

37,500*

-3,000*

-57,000*

-0.345*

0.485*

1.250*

17.783

~~27,000~~

+7.0

2.297

-0.454

+390 28,603

0.663

-0.314

+10.5 3.317

1.498

0.834

+300 49,161

+36.2393

13

30.9

+36.28

49

33.0

13

35.29

+35.58.97

+16.80

+3116.1

319.53

58.56

+16.04

91.72

+16.53

90.4

+1.40

+11.6

+

dy + R

8.11

+0.65

(2)

8549

8994

3110

3010

519

4954

0916

43.7

773

785

65

65

EB du +340 -0.61

8.7112

+0.313

MR

F300 - 0.75

6W2

0.3

73283

+330

-75

-13.0

088

+0.332 -0.060

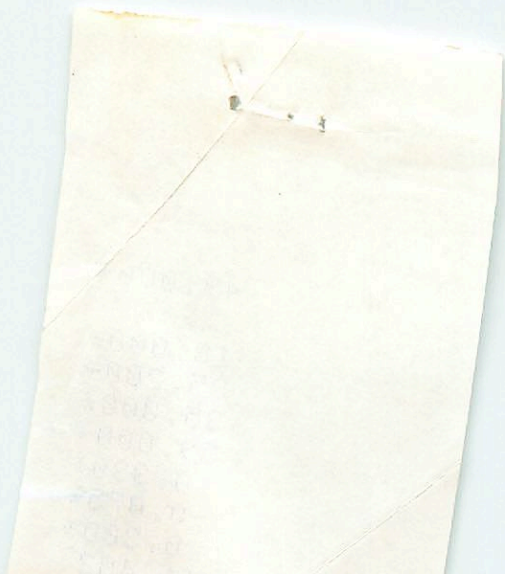
+331 -0.72

+335 -0.90

6.61

335 -0.83

78



49.000*

13.000*

35.200*

35.000*

59.000*

0.330*

-0.075*

0.300*

1.482

521.2MB

497KB

HR574F

119129

017

12 13 384 + 50 46

-0133 + 059 (Amberg)

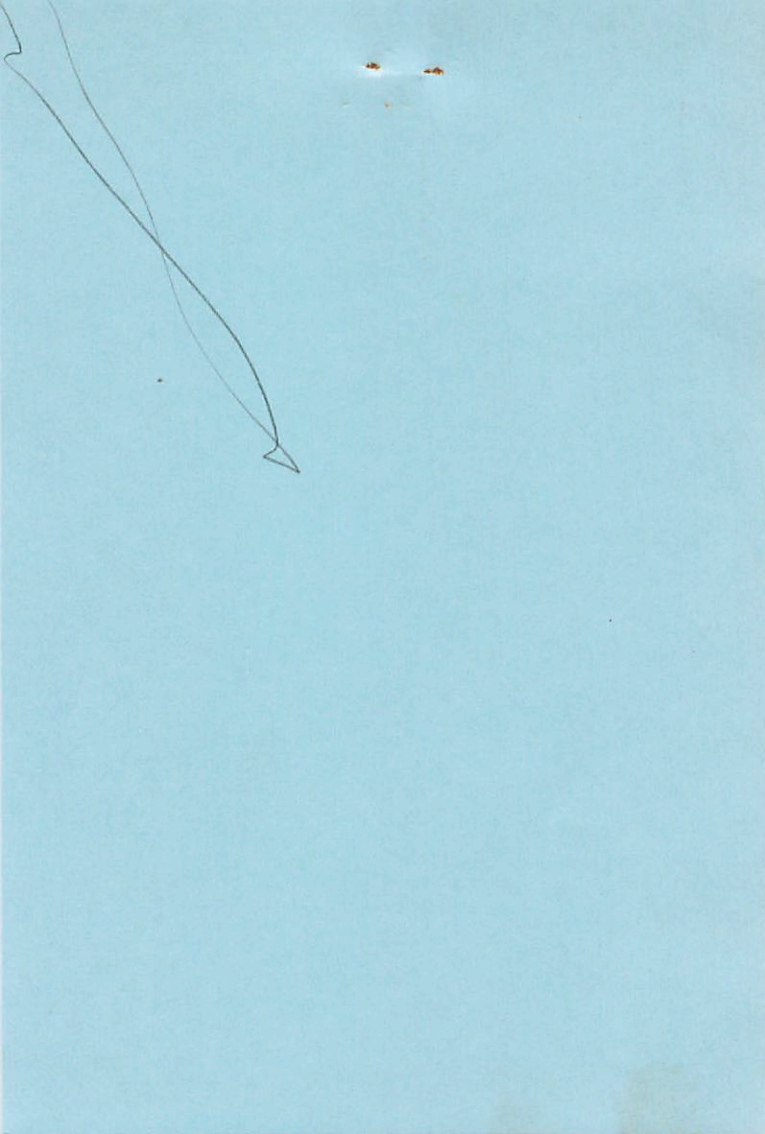
4504 471

4.910
-1881
1445

4246

1411

017E



$T15^{\circ} 2620$ $13^{\circ} 38.4$ $+15 41$ 308

$Y 3135$ $13 40.7$ $+15 26$

$W 8123$ $13 43.0 \rightarrow 0$ $+15 12.42$

$H 119850$ $156 205$ $8.97 + 1.44 + 1.11 MGR R$ $+15.26 SW$ DMZ

~~S 2024~~ $225 M/S$ $152 YK (5)$ $198 ST (3)$ $188 A (20)$ 2024

$B.C. 18602 +1.778$ -1.457 $8.5 M2 + 11.1$ $+0.193$

1201 -1444 (random) $11763 - 1450$ Ge new V

1765 1406 $1764 - 1441$ $7.41 + 85 N$ 1840 1444 -1445 $+15.2$

308

13 43.2 415 10

4502620

8.46 41.44 41.10

408533

hsit

5713

3760
096
1125
3720

+ 1228 24.8
+ 1210
+ 1.5
- 1.457 24.5
- 1.456
10 8.5 dm2 715.28

18602

5123

450262

13 43.2

11.825 1860.2 + 15 9 42.35 1888.6

~~7.345~~

~~4.1482~~

10.591

~~606~~

9.34

~~56.85
12.885
8.981
9.89~~

~~19482
9.741
11.894
5.259~~

45.5

43.3

15303

10.9

~~34~~

~~10.54~~

3.44

68.37

~~17.81~~

29.40

56.31 1940.25

~~56.33~~

~~47.1 1926.7~~

~~32.08~~

~~19.68~~

~~20.09~~

~~38.21~~

3.1

~~20.09~~

~~44.9~~

44.5

47.1

35.2

205

3.1

19.2

10.9

3.6.51

3.1

79



1.3.200 : R.A.
 1.4.200 : DEC.
 1.5.200 : M. R.A.
 N-1444.000 : M. DEC.
 -1.4.20 : DISTANCE
 1.3.200 : MODULES
 1.3.200 : D. VEL.

-0.750 : 01 (M)
 0.200 : 02 (M)
 -0.200 : 03 (M)
 N-10307.010 : 04 (M)
 -0.200 : 05 (M)

0.200 : 06 (M)
 0.700 : 07 (M)
 0.200 : 08 (M)
 -1.0.441 : 09 (M)
 -1.200 : 10 (M)

-0.200 : 01 (M)
 0.210 : 02 (M)
 0.200 : 03 (M)
 N-3170.870 : 04 (M)
 -1.700 : 05 (M)

M

R.A. : 13.700
DEC. : 15.450
M. R.A. : 1840.000
M. DEC. : % -1444.000
DISTANCE : -1.450
MODULUS : 5
RAD. VEL. : 15.200

q1 (U) : -0.759
q2 (U) : 0.582
q3 (U) : -0.292
dU : % -10365.010
U : -57.591

q1 (V) : 0.619
q2 (V) : 0.785
q3 (V) : -0.043
dV : -169.441
V : -1.529

q1 (W) : -0.203
q2 (W) : 0.213
q3 (W) : 0.956
dW : % -3170.872
W : -1.738

-20.1
7.5 div 6 -20.58
8.2 div 6 -21.76
-20.58

-0329±3.5
-0331
13 46.8 +27 14

A055031

120476
18670
815516

DM=0.44
0811

-440-095 H

47.43 / 1892.7 +27 13 43.60 1888.5-

1.885
49.316

5.78
49.38

7.04

44.72 1938.4

47.797

(411.6)

45.5 1930.2
-26

48.07

68.6
34.3

144
15861

45.22
9 9.4
44.97
4.41

45.22
9 9.4
44.97
4.41

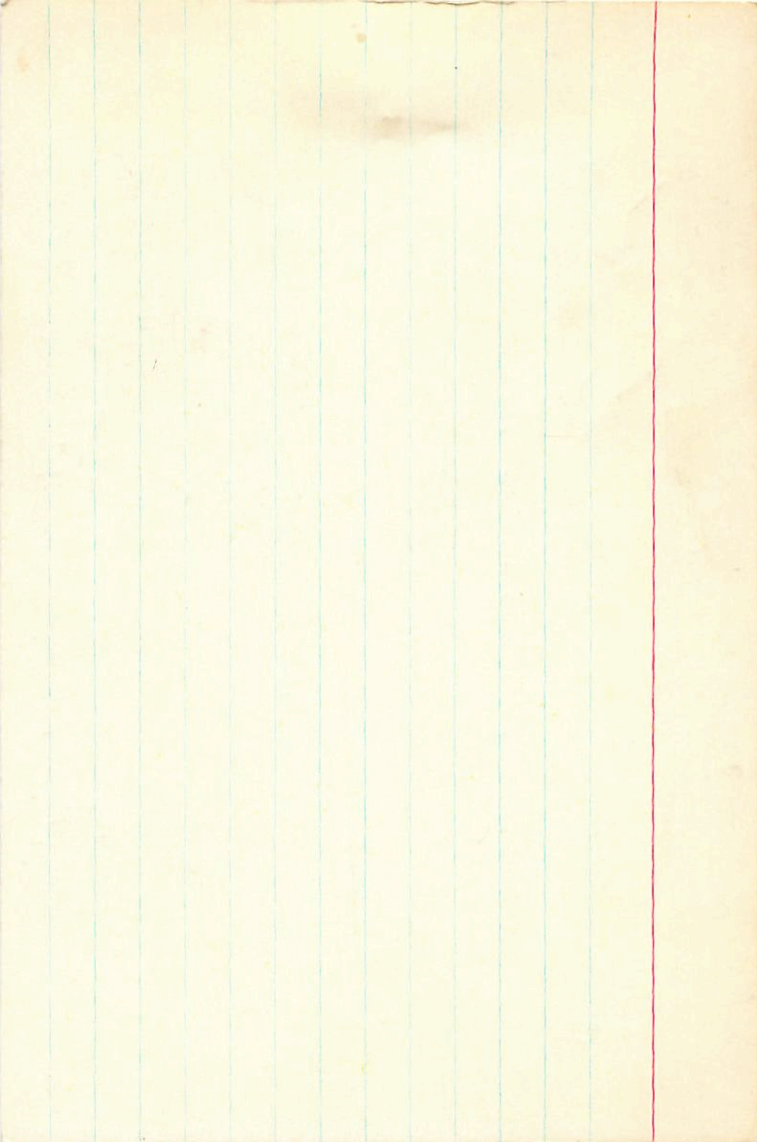
15861
47.940

47.940
11.376

44.97
4.41

45.6
34.3
45.6

-11.376



40 120476
6618670
109031

13 46.8 + 27 29 1500
14 46.8 + 30 - 6 - 9
- 207
- 20.5 (6)

205 + 1.12 + 1.04 (1) 079
205 + 1.12 + 1.04 (1) 079
205 + 1.12 + 1.04 (1) 079
205 + 1.12 + 1.04 (1) 079

6.41 + 0.425 (3) $\rho = 0.87$

Strand R.S. 60, 42, 1555

P as w.

155.71 2.422
155.0 2.423

Rube A.N. 281, 12, 1527
Strand 4560, 42, 1555

$\rho^2 = 2.4133 \times 10^4$
 $\rho^3 = 14.2252$
 $\rho^3 = 1.6587 \times 10^{-3}$

$\rho^3 / \rho^2 = 5.894 \times 10^{-4}$
 $\rho^3 / \rho^2 = 6.587 \times 10^{-4}$
1.16

$m_1 = m_2 = 0.45$
0.60

$\rho = -2.11$

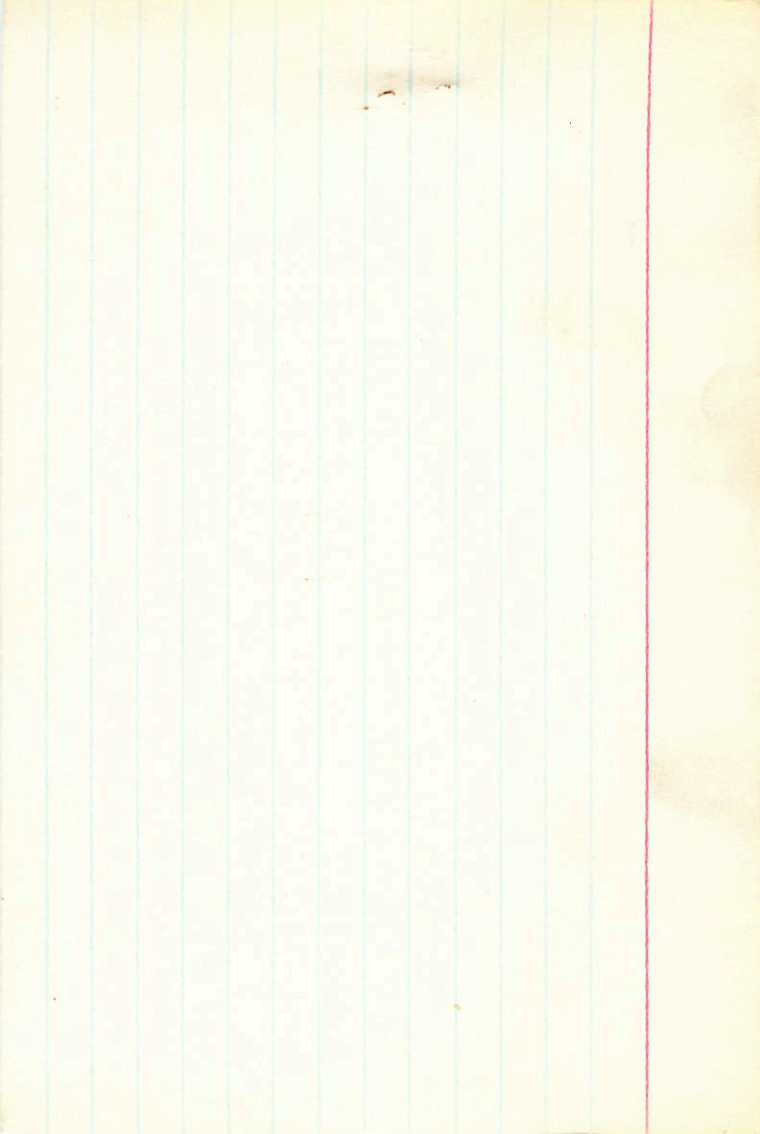
$m_2 = 6m_1$ (Yehus Sunde, D. A. 560 44 1455)
80 M (7)
69 Y (6) (16)
Vim. Bellamp. Apr. 7424 985 (20)
Warren 1569

92 (43)

Photo

long

-1.35



+5° 2767

13 270 +5 25

13 31.8 47.5

10 55.77

43099.1
33 M(8)

25 Jux

7.0 ± 15.0 cm

88
76
76

Way 1487 t.13 -.16

9.2 110

+0.144 m.r

+0.141 -0.117 Y

① 9.97 + 1.38 + 121

-5 -6 +5

+238 -127 (W)

③ 9.06 + 0.68

+0.193
+0.136 -0.118 Y

+136 -125 1.15

48

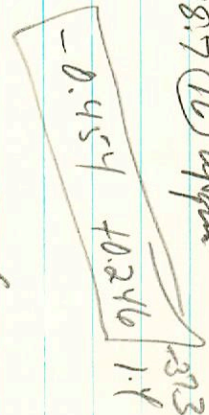
73

+29° 2405 W 509 13 16.8 8.90 12.5 1.24
 13 18.9 8.85 13.6 8.04
 13 21.3 15.4 +29 5.9 BOT 0.59 (16)
 +29 29.24 48.9 301 West 301

W745-3 AB: 7.5, 9.7 binary (Yale)
 HD 8887, $d=0.7$, $\Delta m=0.2$
 -38.7 (16) Wrgum 3.73 -38.7 8.5W
 -38.7 (16) dmd -38.7 (16)

GC 18119 (3M(7))

HD 114455
 Y 3061 W 801 AB



Li 18.1730 -0.476 +0.244 2.34
 8.5 MO 7.9.8
 +0.665

* Spectrum is comparable: M. Hill structure
 give MO for tripletter + K6 for fainter comp.

1887.36 299 0.62 2HO 1418 1418 24

1844.88 312 0.64 5HO 1920 5.4

1846.48 315 0.80 3H 1945.33 30 0.65 3.13

1900.35 321 0.74 8 DOO

1905 3.4 1956.99 48 0.66 8 VB
 1958.27 48 0.77 3B

72