



2.151

5.2

524  
-0002

-035  
F7.4

49.59 60

136

9  
140

0000

0003

-051

-094

1.67  
51.21

100003

49.72 - 33.1

2.164  
-1  
14

~~49.82~~

2.150

-5  
15

49.65

40.52

~~49.70~~ 49.66



136

7390.000\*

19.000\*

24.000\*

20.000\*

9.000\*

-0.000\*

-0.036\*

4.500\*

79.433

-20.600

-0.129

-0.570

1.652

-0.089

0.016

-23.856

-0.069

0.030

-6.125



136

~~15.400~~  
20.000  
0.000  
-43.000  
4.500  
79  
-35.600

0.375  
0.725  
-0.578  
-147.738  
8.831

0.299  
0.495  
0.816  
-100.992  
-37.060

-0.877  
0.479  
0.030  
556

190407  
182955

19243

1947

17.352 5.8

<sup>±2.5</sup> 5000 -0.87

26.84 32

17357

27.47 36

0451 F14

-00030

136

7395

19 244 +86 13

Ar

183056

26876

510-12 -47

593

104

W50  
PAY  
161  
SM

+10003

+10003

-057 121 602.717

171 104  
308  
822

Varied

$m_1 = -1.05$

+10036

10 5.0  
6.05

-22;

1008 +116



137

137

7395.000\*

19.000\*

24.400\*

36.000\*

13.000\*

0.008\*

0.016\*

6.050\*

162.1811254

~~22.000~~

-11.0

0.079

-0.352

20.596 DV

14

0.030

0.922

-15.408 -11.6

0.001

0.162

-3.393 24

Yup

19 24.3 + 34.3

-22C

140183056

-0002 +013 N30

~~-0004~~ +047 GC → N30

-0002 +015

+378	+855	-354		
+244	+251	+922		
-877	+454	+154		
0	+0608		126 m <sup>2</sup>	+15.3
0	+0178	+7.5	+17.8	-18.1
0	+0323	+2.2	-20.3	+0.5
		+4.0	-3.5	

-201  
44

4 byq Si 14 24.4 +84.13 35.02 of

7295 5.14 -0.11 -0.41 317 -11.0 757

183054 W<sup>50</sup> -058 119 603 2710 A  
+1000 109 615 2822

!

14 ± 2.5 833

-00015 +012 N804

+00005 +0136

+00006 89  
16 6.8

1004 1012

-52 119 614 80000

-50 127 664 2729 262

-58 119 603 2710 62

-54 122 608 2715

111 619 2825

224 110

3443

138



1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

138

7395.000\*

19.000\*

24.400\*

36.000\*

13.000\*

0.004\*

0.012\*

6.800\*

5.5 5.45  
144 154.5

229.087

-11.000

0.056

-0.352

42 42

16.672

0.020

0.922

7 7

-5.622

0.009

0.162

0

0.300

Plinky

Thelma West

-22c

7401

19 24.9 +57 56

183339

6.2

-050

880

476

2706 W

+35  
+10

074

486

2774

148  
334

F104

-050 148 +0 113000

6.45

-14

-0118

7.55

-1.2

6.55

-1007 +010

Pub

8912

+02 41516

6577

7533



129



100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

139

7401.000\*

19.000\*

24.900\*

57.000\*

56.000\*

-0.007\*

0.010\*

7.550\*

7.2  
278.5

323.594

-22.000

0.031

-0.009

+9

10.338

-0.015

0.949

-25

-25.761

0.046

0.316

+6

8.001

7401 19 24.9 457 56 187 15

193339

6.62 -14 -54 403 09

-050 088 476 2706

074 486  
158  
644

6.55

55  
-1.25  
9.8

-22.0

~~6014 1014 1130~~  
F-124

-6014 1013  
-6014 1010  
-0116  
-6014 1010

140



140

7401.000\*

19.000\*

24.900\*

57.000\*

56.000\*

-0.007\*

0.010\*

7.800\*

363.078

-22.000

21

0.031

-0.009

11.583

-0.015

0.949

-26.412

0.046

0.316

410

9.542

HRP352  
 HD 183007

Atadris Group  
 19 25.8 -43 33

$\beta = 164.62$   
 $\delta = -30.9$

4 planets  
 $-17$   
 $-42$  }  $-32(4)$

FC2685

574 024 1.215

$$5.69 + 0.22 - 0.01 \text{ BS} = 5.70 + 0.22 + 0.01$$

$$5.71 + 0.22 + 1.55 = 7.48$$

50.801 1507.5 + 10084

$$\frac{357}{.444}$$

$$\begin{array}{r} 10084 \\ + 8 \\ \hline 10092 \end{array}$$

50.735

50.710

$$+ 266$$

121  
 52.23 15080  
 4700

$$\frac{6.26}{45.97}$$

50.02

$$\frac{50.04}{-09}$$

12.20 Hypothesis  
 $M = +44$

$M - M = -17$   
 $3.50 - 13$

81105

130  
 $-324$   
 $398$

309

6337 37 4058  
 8504  
 7731 - 9140

+1796 + 1119  
 +1403 - 5550  
 -4157 - 1397

+2915  
 -4147  
 -5544

+29.2 + 24.0 = +58.2  
 -41.5 + 2.5 = -39.0  
 -55.4 + 13.3 = -41.1

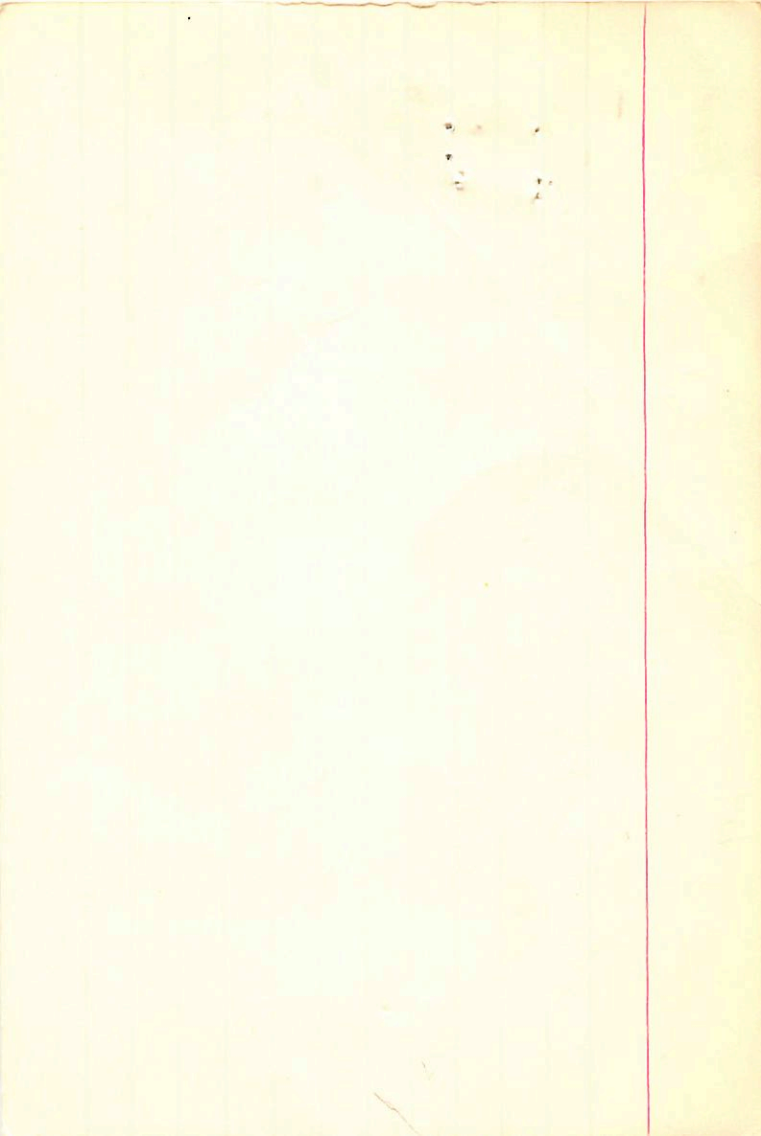
141

100000

70

546  
 -27  
 -25





7392 -31030 5868 -1091 -117 ~~1091~~ 33  
 19 258 -43 33 40 A30  
 A30

18007 -122 sking 5.70 +22 -01 130  
 81 - put 141 160 881 2803

+150 199 817 398 2801 Skim  
 715-3  
 147

NE Sking

FRY 10097-129 1215

+100835-019  $M_V = +2.2$   $q = -30.9$

$n-m = 3.1$

+10907 +1091 120

87-124

$M_V = -0.15$

124  $\delta$  50 145  
 6337 4058 1899  
 7736 9140 0366

Ln 252 +20 161 45.50

-2741

-1356.0

27 -1213

S27 604

+0084

-123 52.23

52)

4471-2001  
621 -784

50.801 022

+0084  
+0074

626  
4597

608/ sin ..

357  
477

+0084

4091.5 -112

-911 MP

50.735  
-22

50.02 34.24

60811

70883 -0120

50.11

490-122

14.4  
-43.55

710  
-2064  
621  
70883  
60620  
70930

-0116

56.77

1460  
0301  
4441

6368 4336  
-7711-9059

+126  
-43.55  
-117.5  
712

1091.4  
91.5-117.5

52.1

1460  
0301  
4441

6368 4336  
-7711-9059

+126  
-43.55  
-117.5  
712

W

60.47X

-11

5335

69.62

6244  
-9103

1461

1441

967

5344

1444

1345

3.05

7397

19 25.8 + 2 49

86111

193227

5.84 + 01 - 40 6

+17 51

11m  
9 m

+059 051 600

2.641

2.118

067 588

4120

138  
92.8

5.36

-13.5

Shoof -0105

6.95  
-1.65

Shoof 108

117-810  
11

10087

SD.120

1913.1 + 0009

0001 ± 3.5

-007 ± 3.4

-014  
37.39 15100

257

37.67

+00045

50.132

37.17 1533.6

+6

+18

181

37.35

1018

-32

475  
+054

-004=0  
-030=0

324  
1624  
1350

614  
47  
82-  
131-  
rest  
194

012-008

620-003  
+1.9  
15pm

2893 56  
1030 167  
2905 157  
2594 162  
2594 1026

17 312  
1024

with  
15pm  
2688  
18324  
748

19 26.2  
+52 13  
40

2688  
18324  
748

241

142

19,400

52,200

-19,500

-28,000

4,700

87.10

91.20

1,900

0,375

0,921

-0,103

-143,524

-12,695

13

0,299

-0,015

0,954

-14,078

0

0,517

-0,077

0,389

0,281

-1,087

0

0,369



7699  
183534

19 26.2 + 52 13 5.7 A0 + 1.9 a

26893

11903 -0020<sup>20</sup> -624<sup>20</sup> N30

-6023<sup>±2.0</sup> -023<sup>±1.8</sup> G6 7N30

Buy C  
8146

7418 15 282 31 15 207 51

183514

Party

W50

(104)

515-50-34

+5000  
+2000  
+2000

Field

+5000  
-2000  
-2000

2737

526

030

9006

126  
Q91

~~1200-6000~~

0010  
+1004-002

2000

126

800-100

Q105=01

290+111+80.8

55.2.95

515

(-2.90)

96.5

1

183806 19 24.8 -45 23 5.8 Ap -8 45h

-0008 -031 N30  
-0007 -025 00  
-0008 -028

