

664

12 31.4 -14 21

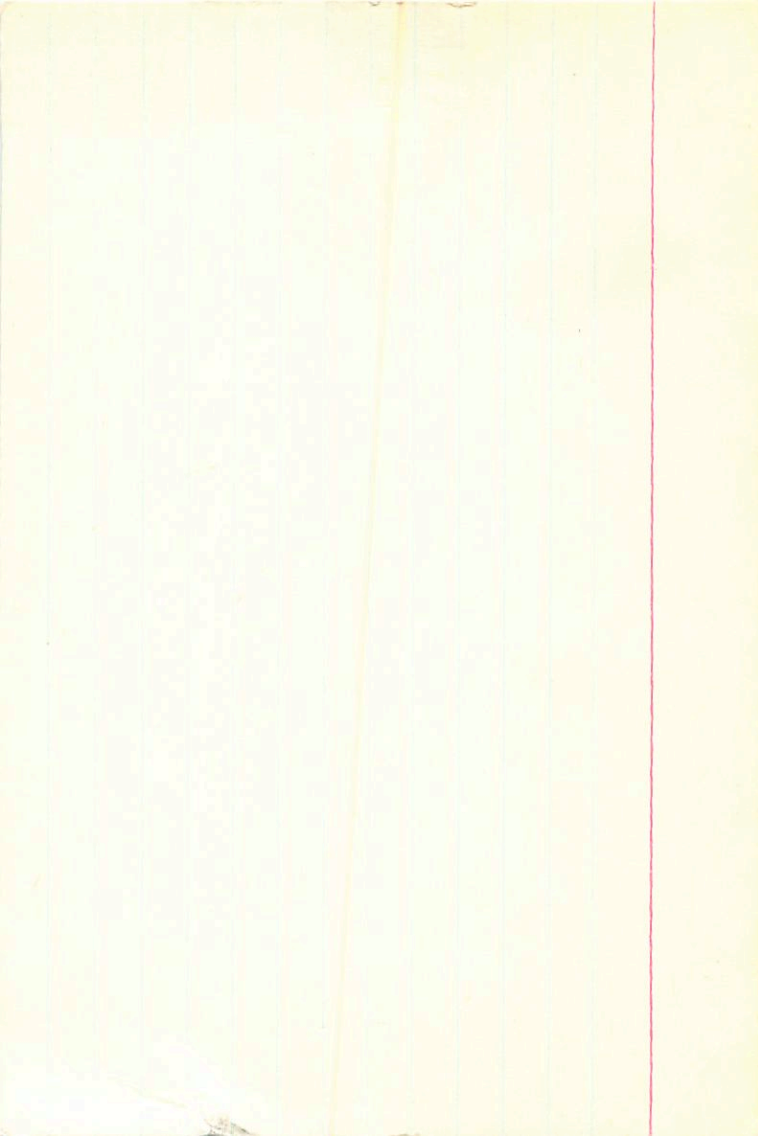
-1303557

9.05 +1.12 +1.01 $\text{\textcircled{D}}$ +0.4157

=21300

See 664-

+10.0



+12° 2497

12 30.6 +12 43

882

12 35 23.9 +12 11.64

$\text{IncC} - \text{AC} - 0.137 - 0.248$

10.3:K8-

+45° 2055

12 31.0

+45 32

667

12

35

33.3

+45

0.64

BDS 6226; $d = 10''.3$

$\sigma_m = 0.0 \text{ mag.}$

—

10.6 Mo + 8.5

~~1830 + 240.5~~

1880.31 78.4 10.28 1 B.ij

*

668

+50 47

12 32.0

12 36 28.9 +50 15.66

871

10.6 MO + 8.4

+55° 37374

12 32.5 +55 14

669

12 36 54.6 +54 42.67

McC-AC +.010 -.013

11.1 K8 +8.0

+27° 2163

12 35.0
~~12 37.3~~
12 39.7

+27 9
~~+26 9⁵³~~
+26 37.73

671 *

ADS 8635; $d = 0.4$
 $\Delta m = 0.4 \text{ mag.}$

47
23
23 = 8 VV

830
905
8.5

-6.1 3 kg
-4.3 2000
5.2

Yale Zone +.021 +.081
0 -8
+4

8.9 K8 + 7.4

+0.021 +0.077

+0.81 +0.87 VV

+8 +16 -4
+1 +4 0

3.0
+25 +90 -43

880
905
532
838
045
55

828
75
604
010
67
2

671

12 89.7 +24.88

+2702163

AD59635

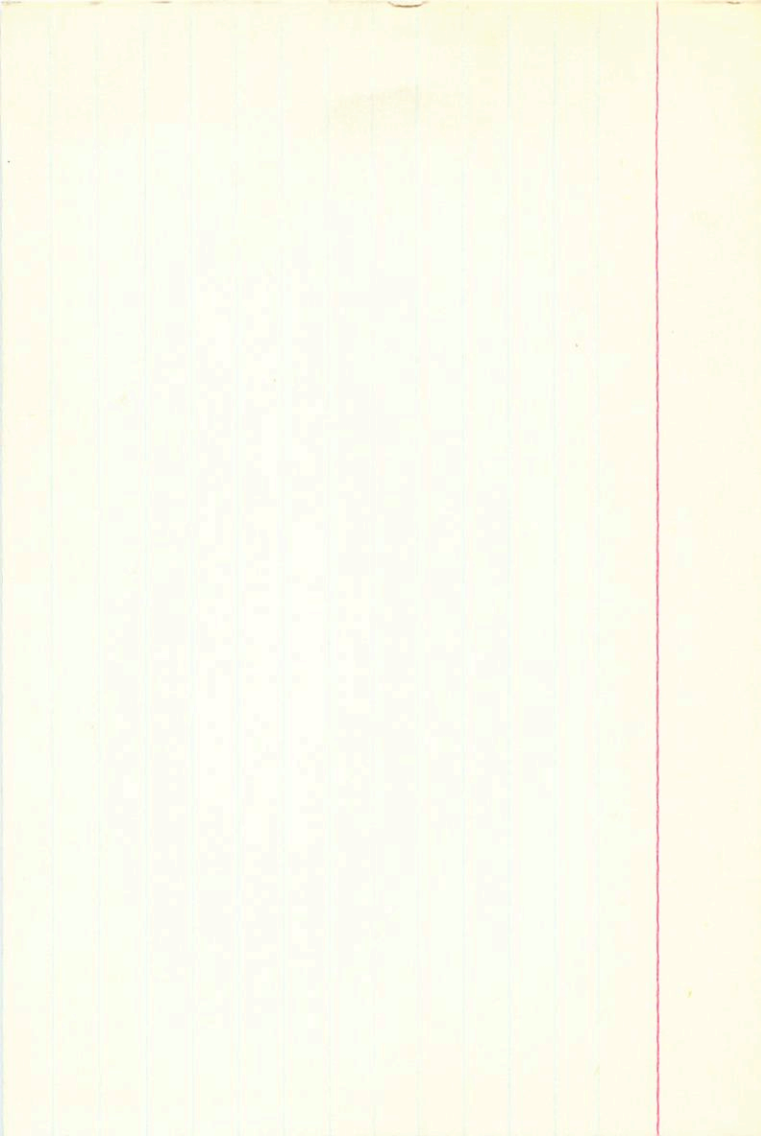
AB 9.27 +1.05 +1.01 ①

+0.405 ②

"
DM 6m²0.4

v/mer

-4.3



-2° 3569

12 36.9

-2 13

672

12 41 46.8

-2 44.22

McC-AC +.085 -.158

11.1 K8 +7.7

+44° 2223

12 38.1

+44 13

673*

12 42 36.4

+43 41.81

ADS 8655; $d = 1''.6$

$\Delta m = 0.1 \text{ mag.}$

MCC-AC -0.061 ± 0.038

9.6 KS ± 6.9

673

12

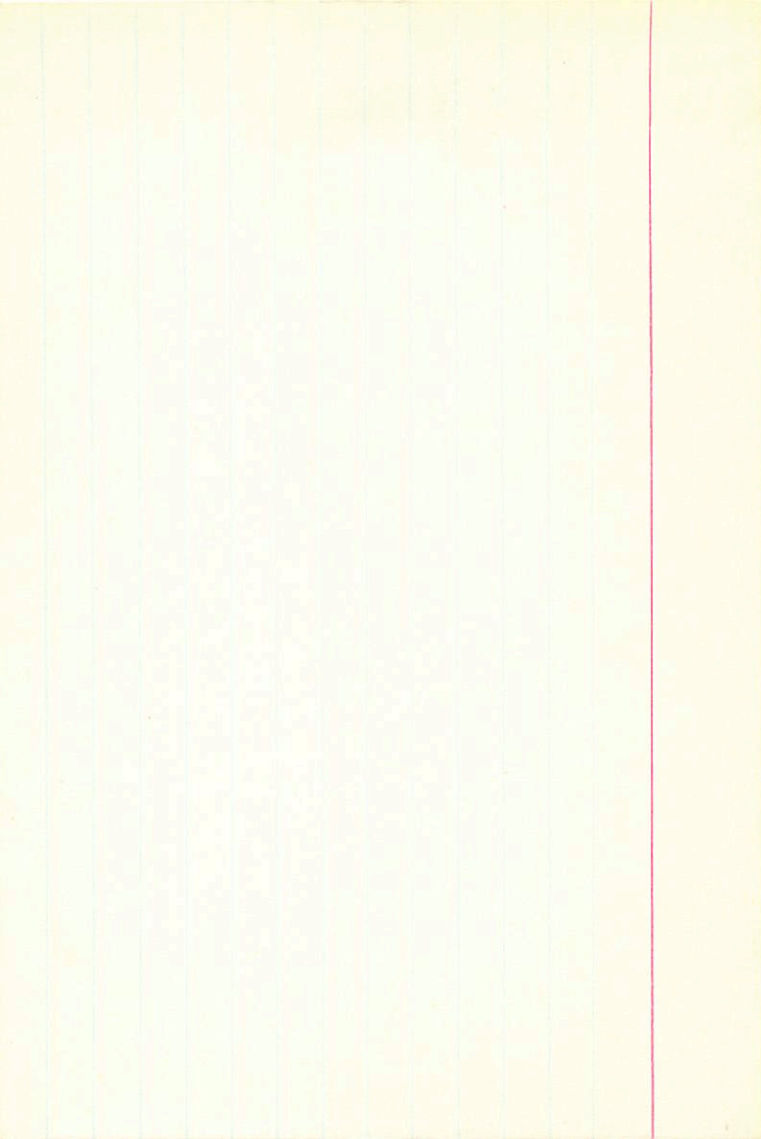
31

עעעעע

ADSS655

1.6 6m.p.t

1/2
1/2



+23° 1189.27

12 40.9

+23 43

674

12

45 35.5

+23 11.89

MC-AC -0.050 -0.095

11.4 170 +8.7

+41° 537-54

12 43.6

+41 7

677

12 48 6.1

+40 35.96

M_C-AC -0.57 +2.56

11.2: M_O +8.3

30" $\delta m \Rightarrow m$

+272181. 12 44.8 +27 34 678

12 49 26.5 +27 3.00

McC-AC +.036 +.048

11.2 K8 +7.8

+60° 23' 28.4

12 45.4 +60 36

679

12 49 30.0 +60 5.01

McC-AC -0.074 -0.084

10.7: 190 + 8.2

+17 2554

12 45.9

+17 37

680

12 50 37.6

+17 6.03

McC-AC -0.079 +0.096

10.3 K8 +8.0

H0109011

12 28.9 +55 24

-12.4 6

+5501534

8.09 +0.93 +0.64 112.5

104
+122 -004

+102 - 5 40R
+105 + 3 4 →

6-15

+0122 -004

+7 +1

0124 -000

0122 -001

104

+103 -001

6711

-7414

9998
-078
1030
0008
+010
0404

1.47
-13.3

-176-552 823 568 +104-004 -12.4-003 -10.2-009
013 0-104 003 047 -493 -7.0 +7.0 +0.9 045

+8.0 -10.1 -10.2

$\boxed{-117 + 12 - 97}$
-12.5 -10.2

04

+8.2 -11.4 -10.2

$\boxed{-171 + 13 - 97}$

-6.3
-5.8
-7.5 - 10

12 395 +56 00
8.27 + 0.95 + 0.76 K30

H0110463
+5601618
W7430

+122 -008 Y
+132 -007 G(2)
+130 -008

H21 +3 APR 6th Y →
+120 -4

6859
SEC
1310
~~5050~~
-048

-13.0

5-1414
+ r

1200
-0071
10.75 00956 171

1048 -006
H21

100-1

-172 955 829 559 +130-008 -6.8-007 -9.2-021

022-001-128⁴007 074 -671 -3.5 +3.4 +0.6 05

+4.8 -11.6 -5.6
-12.4 +3.3 -4.1

04

+5.2 -14.7 -5.9
-15.1 +4.6 -4.6

045

+9.0 -13.0 -5.6
-14 +4 -8.7

12449-0318

518-215

1-419

000 334-

~~104~~ 605-

~~610-055~~ ~~000 334-~~

9953	- 9957	5010 445
-0923	1088	0545 053
		5145 + 415

0518

1.93

$734 \text{ } ^{\circ} 2366$ 12 45.9 $+34$ 31 681
 $\begin{array}{r} 12 \\ 12 \end{array}$ $\begin{array}{r} 48.2 \\ 50.5 \end{array}$ $\begin{array}{r} +34 \\ +34 \end{array}$ $\begin{array}{r} 16 \\ 0.03 \end{array}$

$+11.32 \text{ up}$
 $\begin{array}{r} +10.3 \\ +10.5 \\ \hline +10.4 \end{array}$

$9.6 \text{ } 158 \text{ } 77.4$
 $\begin{array}{r} 871 \\ 755 \end{array}$

$C: 18.1641 - .21 - .02$

$\begin{array}{r} 23 \\ -0.210 \\ -0.020 \\ \hline 10.3 \end{array}$

$\begin{array}{r} 5444 \\ -9872 \\ \hline 185 \end{array}$ $\begin{array}{r} 185 \\ 014 \\ +335 \\ \hline 014 \end{array}$ (NO)

$-185 + 16 \pi$



1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

1000000

681.000*

12.000*

50.500*

34.000*

0.000*

-0.210*

-0.020*

2.300*

28.840

10.800

0.782

0.058

23. ¹⁶~~15~~

-0.623

0.099

-16. ⁹⁰~~85~~

0.017

0.993

11.21
10.112

687

12 50.5 + 34 00

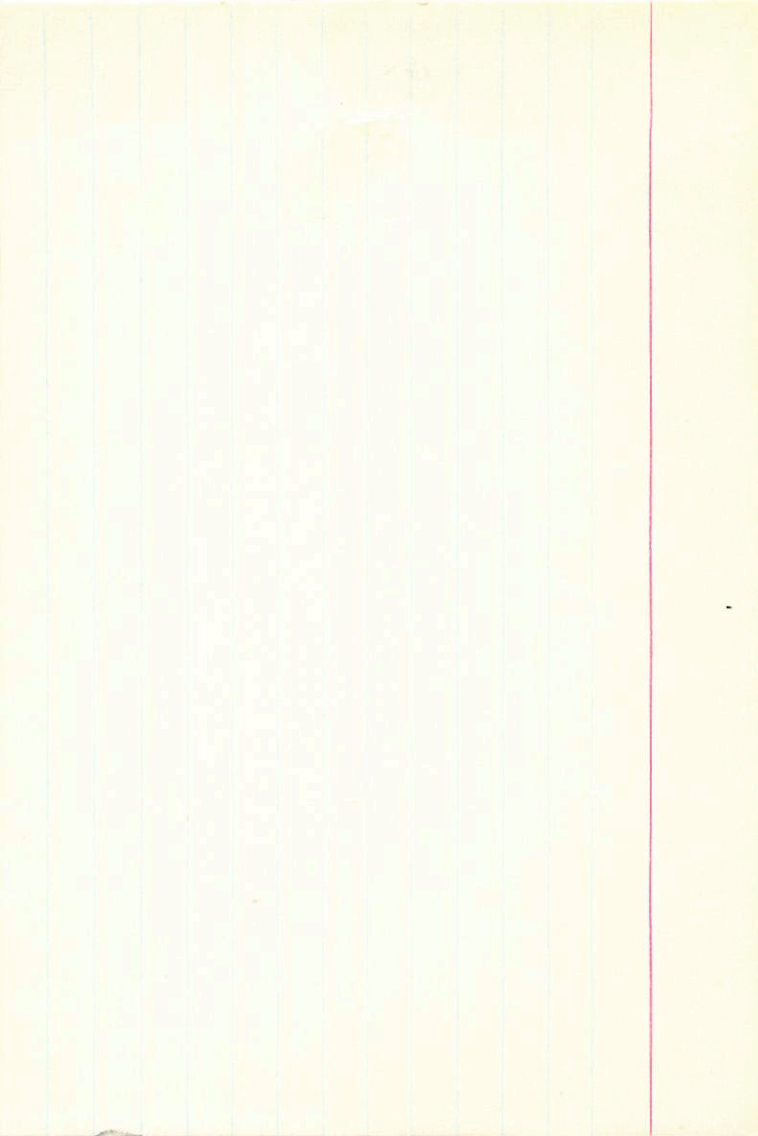
+ 3402366

+ 0.413

9.42 + 108 + 0.840

- 0.21 - 0.12 in

+ 10.3



-21° 56' 27

13 57.8

-20 17

683

13 2 52.3

-20 47.56

McC-AC +.109 -.152

10.2; 158 + 7.2

883

12 57.3 +42 15

+4202361

8.64 +0.54 +0.72 ② +0.35 ②

① 6.14 ①



+56°45927

12 58.7

+56 41

684

13 2,743.8

+56, 10.46

McC-AC -.160 +.038

NO

10.4: MO +9.1

WOR 23

$5m = 0.9$

1940.41 130.8 0.94 2 WOR

1941.37 139.1 0.84 3 WOR

1643

-0048

-1.3

0171

383

+35°, 2406

13

0.8

+35

10

299

3.0

+34

58

39.54

5.315.8

+34

39.54

11.0 @ 0600

80°

76

E.B. Lex. -0.127 -0.005

9.6 K8 +7.8

19
-0.127 -0.005 11.0

299

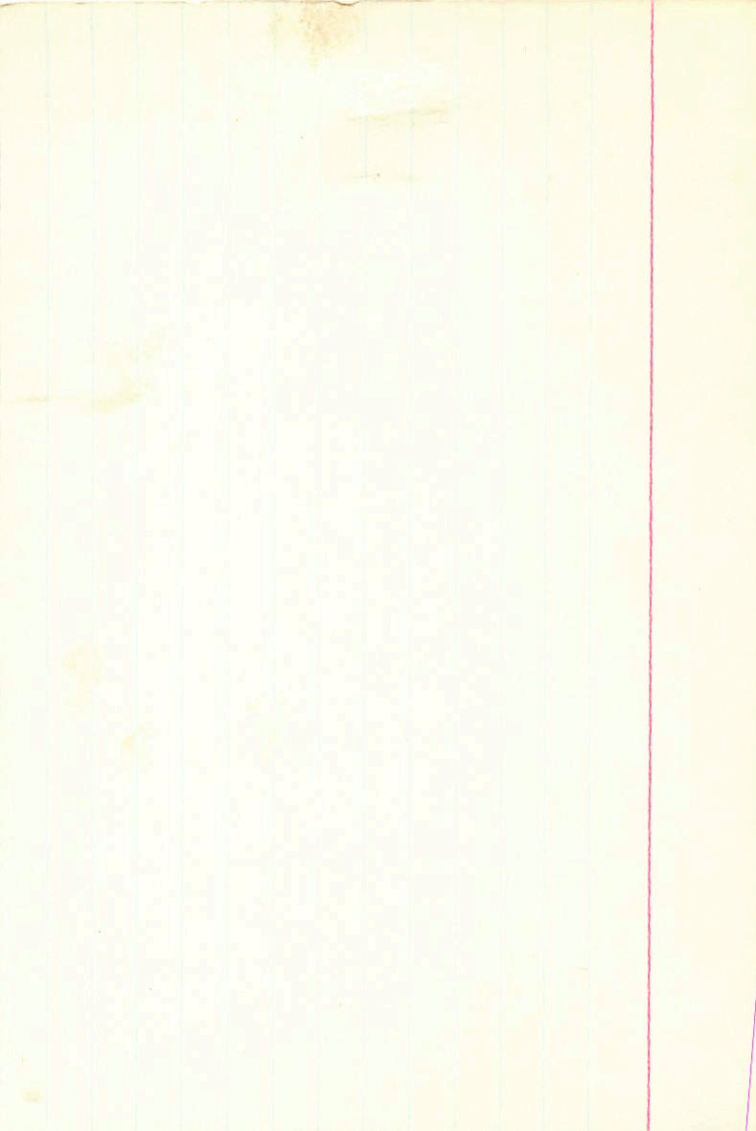
'13 05.3 734 46

+3502406

9.34 +1.18 +1.10 (2)

+0.455 (2)

-1.0



G14-32

13 05.9 07 02

Sample
+74.2

114095

8.34 0.945⁷ 5.8 (2)

7.82 + 0.395

π_{18} 0.045

0.793 2540

744
5

205 119

1.75

-270

169

1.75

+74.2

Handwritten text on a piece of paper, possibly a receipt or note, with a metal fastener visible. The text is partially obscured and difficult to read due to the angle and lighting. Some legible fragments include:

Handwritten text (partially obscured):

- Handwritten text (partially obscured):



13.100
1.950
200

+17° 478-60 13 1.4 +17 45 686
13 6 4.9 +17 14.57

M₁C-AC -0.82 -0.003

11.2: M₁O +9.4

G-164-47 2051865 #13 07.2 +29 15

Gradin
45 235°

B 13 07.3 +29 18

393 -275

43

240 0.374

-328 -190



Road
57414

9042 - 8557 } 374

479

Agua

-4270 -5174 } -007

032

-075

+2.75

0487

0.552

1.80

1.24

Road 57-04

994B-9821

-1059 #1065

12 Mont - Street and Barnett

The Parable of the Sower
written in Manuscript.

13107 + 2027

18 10.7 + 20 27

G-6/1-41

-590 + 139 ~

(-600 149)

9899	-448	605
-1427	1740	-0322
		-245

0637

617

0458

-042

-30

0649

054

+21° 1201-60

13

10.5

+21

11

687

13

15

6.7

+20

40.95

McC-AC - .020 + .020

10.5: MO + 8.7

$+30^\circ 2400$

13

21.5

+30 48

690

13

25 55.1

+30 18.47

McC-AC $-164 - 195$

10.8: MO + 8.3

+75°510

13 30.4

+75 44

*
695

W8038

13 32.1 5.7

+75 14.87

-350 2nd
div5

Green. Ast. - .418 + .039

10.5 K8 + 7.8
+ 0.039

* Common motion with BD +75°511
(10.0 mag, K5).

-0.418 + 0.039

300 13 18.3 +10 11

+1002540

9.50 +1.14 +101 C

+0.42 (2)

+10.2 ✓



+10° 25' 40

13

13.6

+10 41

300

13

15.9

+10

26

13

18.3 ~~20.3~~

+10

11.10

687

Arc C-AC -0.24 -0.11

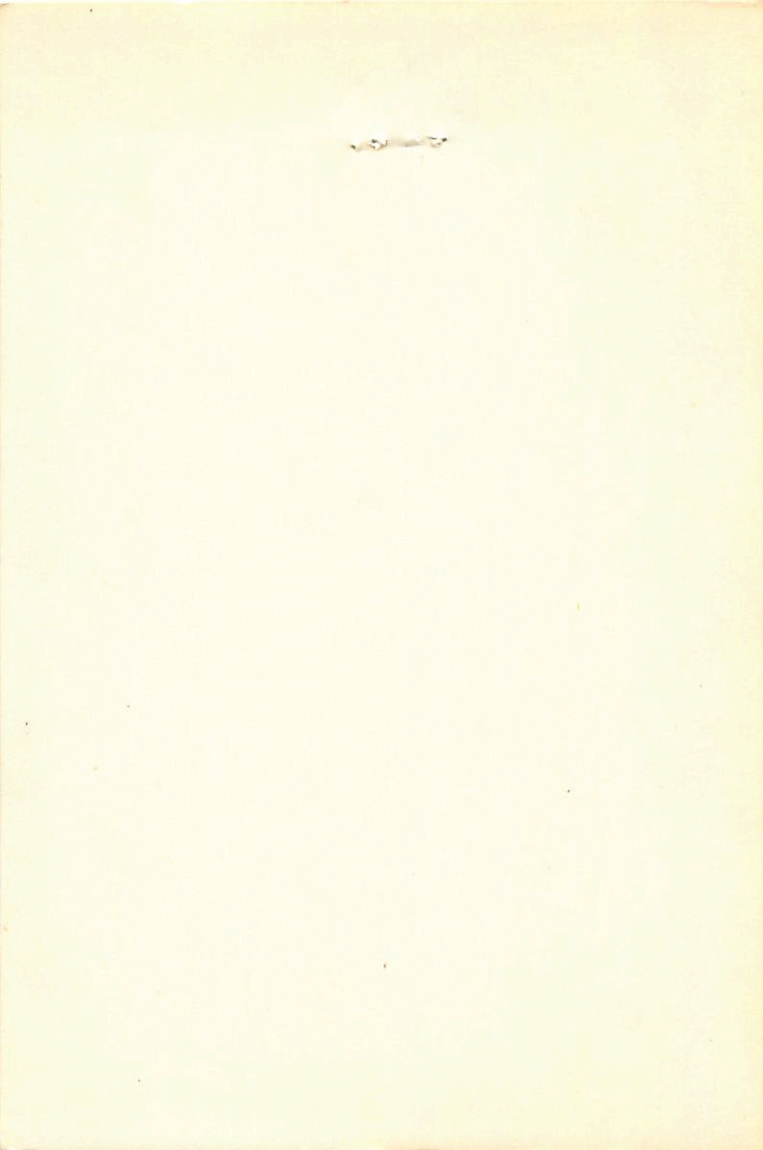
9.7 K8 + 7:

63

-0.240	-0.110
--------	--------

-275 -125 2.7
+10.0

-311 -135 (60)



177

180-180

181-181

182-182

183-183

184-184

300.000*

13.000*

18.300*

10.000*

11.000*

-0.275*

-0.125*

2.700*

1.674

1855

.13 18.7 139

302

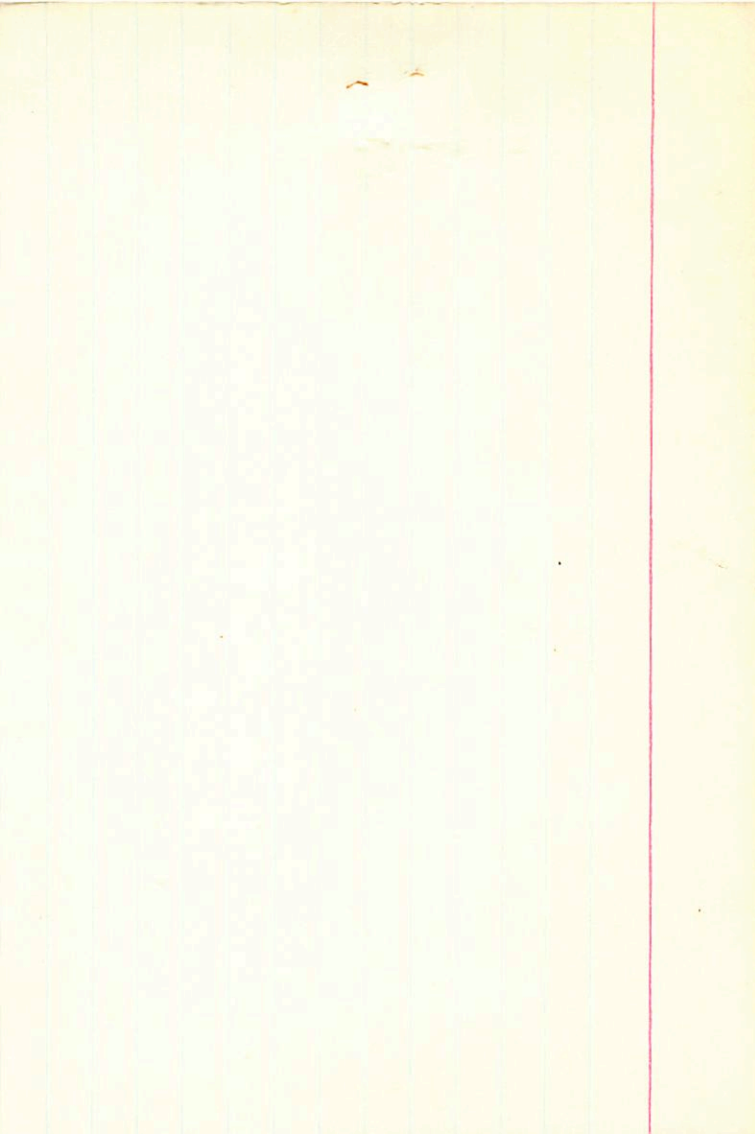
13902643

9.5

10.112 + 1.02 + 0.82

70.405

1



+39° 2643

13 18.7
¹³ 20.8
13 22 57.8
23.0

+39 41
⁺³⁹ 26
+39 11.33

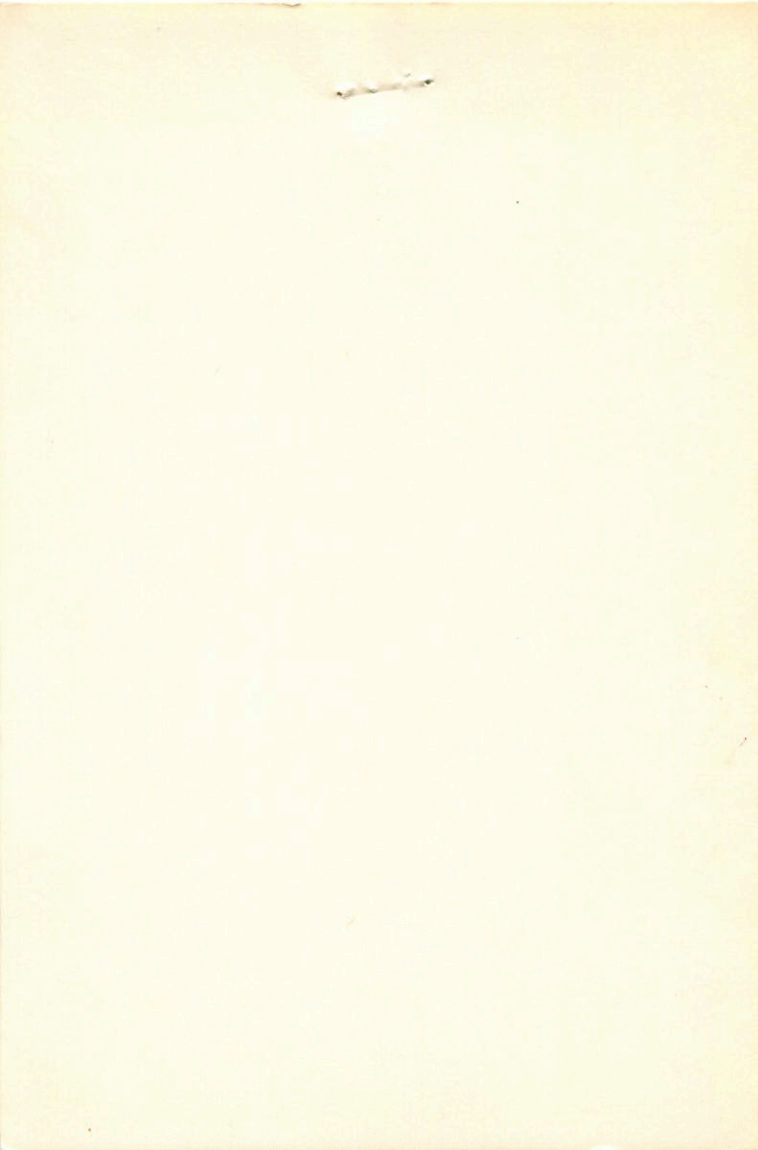
302

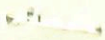
E.B. Lex. -0.08 -0.04

2.95
-0.080 -0.040
-7

902
846
55

9.5 K8 +7:





302.000*

13.000*

23.000*

39.000*

11.000*

-0.080*

-0.040*

2.950*

38.905

-7.000

0.185

0.017

7.072

-0.371

0.237

-16.108

0.087

0.971

-3.403

+31°2500

13 25.3

+31 54

691

13 29.740.7

+31 24.67

44
22

-144 +39 AB10} → 1442 -0021 -0.6 0.158 4.00

McC-AC -0.078 +.024

10

11.05
10.3 MO +8.7

WOR 24

$\Delta m = 0.2$

1940.32 352.8 0.36 4 WOR

1941.39 335.9 0.26 4 WOR